



GeoMat Testing Laboratories, Inc.

Soil Engineering, Environmental Engineering, Materials Testing, Geology

December 3, 2007

Project No. 6003-02

TO: Inland Communities Corp
1801 Avenue of the Stars, Suite 1107
Los Angeles, California 90067

ATTENTION: Mr. Mohamad Younes

SUBJECT: Geotechnical Review of Conceptual Grading Design, University Hills Specific Plan,
Badger Canyon Area, City of San Bernardino County, California

Per your request we have reviewed the subject 40 and 100-scale Conceptual Grading design for the University Hills Specific Plan from a soils standpoint. The plan was prepared by PBS&J of Riverside, California and dated August 31, 2007.

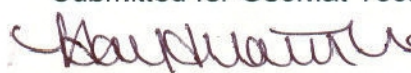
We have also reviewed the subject site preliminary geotechnical investigation report prepared by CHJ Incorporated with respect to the subject new University Hills Conceptual Development Plan. Project planning since the date of CHJ Incorporated preliminary geotechnical investigation report (May 18, 2006) has changed. The project now includes not only single family homes but also two and three stories attached and detached multi-family residential units in addition to recreation facilities.

The soils findings and soil laboratory testing presented in the referenced preliminary geotechnical investigation by CHJ Incorporated dated May 18, 2006 are summarized in this report. The recommendations in the report remain pertinent except as modified for the subject revised development plan and must be verified by observations and testing during actual grading of the site.

The subsurface investigation of faulting dated January 31, 2006 by CHJ Incorporated was also reviewed with respect to the subject University Hills Conceptual Development plan. This review is presented in Appendix "G" of this report.

Should you have any questions, please do not hesitate to call our office. We appreciate this opportunity to be of service.

Submitted for GeoMat Testing Laboratories, Inc.


Haytham Nabils, GE 2375
Project Engineer



Distribution: [3] Addressee

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Œ²» ¼±®²¹ ©¿¿- ¼®''»¼.² ¿¿.- °¿²².²¹ ¿¿¿¿¿ đÞŃē±đ Ā ¿» -±'..² ¿¿» ¼±®»¿¿±' ©¿¿- ¿¿-°±'±©-±

ÞŃē Œ¼ ß''ª.¿'°¿² Ū»°±±-¿- Ń ĩ ±Ń í ÷

Đ®±°±-»¼³ ¿¿- 1®¿¼.²¹ 0±®¿¿.- --»- .- °'' 1®¿¼.²¹đ Ő¿''..³ «³ °®±°±-»¼°'' 1®¿¼.²¹ -.. ±² ¿¿» ±®¼»®
±° ĩ đ ± ĩ đ »»»đ Ā ¿» ®½±³ ³ »²¼»¼ ±ª»®»'½¿ª¿¿±² 0±®¿¿.°'' °±®±² ±° ¿¿» --»- .- ĩ ĩ »»»đ »°®
ÝŸŸ x²½±®±®¿¿¿¿¼®°±®đ ß®»¿¿- °®±°±-»¼°±®³ ±®» ¿¿¿² ĩ ĩ »»»±° ½«¿ 1®¿¼.²¹ ³ ¿¿¿² ±¿¿¿»-«®»
±ª»®»'½¿ª¿¿±² ¼«²¹ ³ ¿¿- 1®¿¼.²¹đ ß®»¿¿- °®±°±-»¼°±®'-- ¿¿¿² ĩ ĩ »»»±° ½«¿ 1®¿¼.²¹ -.. ±«¼
¼» ±ª»®»'½¿ª¿¿¿¼ ±±¼-»ª» ¿¿» ĩ ĩ »»»½±³ ³ »²¼»¼®³ ±ª¿¿đ

Ā ¿» °¿²².²¹ ¿¿¿¿¿ 1®¿¼.²¹ .²½'«¼»- °''Ń±ª»®½«¿-±°»-đ Ā ¿»-» -'±°»- ¿¿» ¼»-..¹²»¼ ¿¿ ĩ Őđđ Ēđ
Ā ¿» -'±°»- ®¿²¹ »®±³ ĩ ē ± ĩ ĩ »»»¿.² ¿¿.¹ ±đ ĩ ±°»- ±ª»®'đ đ »»»¿¿¿® °®±ª.¼»¼ ©.¿¿ ¿¿ »»»©.¼»
¼»²½¿đ ¿¿- ¿¿±©² ±² ¿¿» ½±²½»°«¿¿ 1®¿¼.²¹ °¿²-đ

Đ'¿²².²¹ ß®»¿¿ è ŃŸ±±- èŃ éŃ ¿²¼ è±±

Ā ¿.- í òé ¿½®»- --»- .- °®±°±-»¼°±® -..²¹'»Ń³.Œ®»-¼¿²¿¿' «-»đ Ā ¿» --»- -'±°»- ±±©¿¿¼ ¿¿» -±«¿¿
¿¿²¼ -±«¿¿ ©»-¿¿¿² ¿¿°®±'..³ ¿¿»®¿¿» ĩ đ »»®½»²± Ā ©±¼¿¿¿¿²¿¹» ½±«®-» ½«¿¿¿±«¹ ¿¿¿¿¿-
.² ²±®¿¿¿¿¿-Ń-±«¿¿ ©»-¼¿®½¿±²đ Ā ¿» ¼¿¿¿¿²¿¹»- ¼¿-½¿²¼ -±«¿¿ ©»-»»Œ¿ ¿¿¿² ¿¿°®±'..³ ¿¿»®¿¿» ±°
ĩ đ »»®½»²± Ā ¿» -±'..² ¿¿» ¼¿¿¿¿²¿¹»- ©¿¿- ³ ¿¿°»¼.² ÝŸŸ x²½±®±®¿¿¿¿¼®°±®¿¿¿¿-ª»ŒŒŒ±«²¹
©¿¿- Ń ĩ ©±đ Ā ¿.- ³ ¿¿»®¿¿' - «²½±²-±'¼¿¿¿¼ ¿¿²¼ -«¼Œ»½¿± -»»³ »²± Ā ¿» ®³ ¿¿¿²¼»®±° ¿¿» ¿¿¿¿¿
©¿¿- ³ ¿¿°»¼ ¿¿- ±¼¿¿¿'«ª.¿'°¿² ¼¿°±±-¿- Ń ĩ ±Ń ¿¿²¼ Ā ±Ń í ÷đ

Ā ¿»» ¼±®²¹ ©¿¿- ¼®''»¼.² ¿¿.- °¿²².²¹ ¿¿¿¿¿ đÞŃí èđ ÞŃí çđ ¿²¼ ÞŃí í ÷đ Ā ¿» -±'..°®±°'» .² ¿¿»
¼±®»¿¿±' ©¿¿- ¿¿-°±'±©-±

ÞŃí è Œ¼ ß''ª.¿' Ū¿² Ū»°±±-¿- Ń ĩ ±Ń í ÷
ÞŃí ç Œ¼ ß''ª.¿' Ū¿² Ū»°±±-¿- Ń ĩ ±Ń í ÷
ÞŃí í Ē»ŒŒŒç±«²¹ Ē ¿¿- Ń ĩ ©±ª»® ß''ª.¿' Ū¿² Ń ĩ ±Ń í ÷

Đ®±°±-»¼³ ¿¿- 1®¿¼.²¹ 0±®¿¿.- --»- .- °'' ¿²¼ ½«¿-Ń±đ°''-®¿²-¿±² 1®¿¼.²¹đ Ő¿''..³ «³ °®±°±-»¼°''
1®¿¼.²¹ -.. ±² ¿¿» ±®¼»®®±° ĩ ç °»»±² Ő±± èđ Ő¿''..³ «³ ¼¿°¿¿ ±° °®±°±-»¼ ½«¿ 1®¿¼.²¹ -.. ĩ ĩ »»»±²
Ő±± èđ Ā ¿» ®½±³ ³ »²¼»¼ ±ª»®»'½¿ª¿¿±² 0±®¿¿.°'' °±®±² ±° ¿¿» --»- .- ĩ ĩ »»»đ »°® ÝŸŸ
x²½±®±®¿¿¿¿¼®°±®đ ß®»¿¿- °®±°±-»¼°±®³ ±®» ¿¿¿² ĩ ĩ »»»±° ½«¿ 1®¿¼.²¹ ³ ¿¿¿² ±¿¿¿»-«®»
±ª»®»'½¿ª¿¿±² ¼«²¹ ³ ¿¿- 1®¿¼.²¹đ ß®»¿¿- °®±°±-»¼°±®'-- ¿¿¿² ĩ ĩ »»»±° ½«¿ 1®¿¼.²¹ -.. ±«¼
¼» ±ª»®»'½¿ª¿¿¿¼ ±±¼-»ª» ¿¿» ĩ ĩ »»»½±³ ³ »²¼»¼®³ ±ª¿¿đ

Ā ¿» °¿²².²¹ ¿¿¿¿¿ 1®¿¼.²¹ .²½'«¼»- °''Ń±ª»®½«¿-±°»-đ Ā ¿»-» -'±°»- ¿¿» ¼»-..¹²»¼ ¿¿ ĩ Őđđ Ēđ
Ā ¿» -'±°»- ®¿²¹ »®±³ ĩ ē ± ĩ ĩ »»»¿.² ¿¿.¹ ±đ ĩ ±°»- ±ª»®'đ đ »»»¿¿¿® °®±ª.¼»¼ ©.¿¿ ¿¿ »»»©.¼»
¼»²½¿đ ¿¿- ¿¿±©² ±² ¿¿» ½±²½»°«¿¿ 1®¿¼.²¹ °¿²-đ

Ý±2½»°«¿ Đ'¿² Ĩ »ª.»©Ě².ª»°.-§ Ø.°- í »½º.½ Đ'¿²
Ý.-§ ±° í ¿² Þ»²¿²±0 Ý¿:º±²¿.

Đ±½»½- Ò±0 êððí òðí
Ú»½»³ ¼»° í ò ððé

Đ'¿²².21 ß»¿ è ò0±½ ¿±½

Ĩ .- í ò Ĩ ½»- -»» .- °±º±»¼ º±º .-21'»º¿³ .§ »-¼»²¿¿ «-»ð Ĩ » »'..-¿²1 -»» -'±º»- ±¿¿¿¼
¿ »-±¿¿¿ ¿²¼ -±¿¿¿ »-¿¿¿¿ ¿º±º±.³ ¿¿ »¿¿' í ð è °»½»²-ð Ĩ ±³ ¿½»¼¿.¿¿¿¹ ½±«-» ½«-
¿»±«¹ ¿¿¿¿ ¿»¿¿¿.2 2±¿¿¿¿¿-0-±¿¿¿¿ »-¼»½¿±²0 Ĩ » 2±¿¿¿¿² ¿²¼ -±¿¿¿¿² ¼¿¿¿.¿¿¿¹ »- ¼»-½»²¼
-±¿¿¿¿ »-»»²¿ ¿¿¿¿¿.² ¿º±º±.³ ¿¿¿¿ ¿¿¿± ° èð ¿²¼ è °»½»²-ð »-º»½¿ª» §ò Ĩ » -±.² ¿¿¿ ¼¿¿¿.¿¿¿¹ »-
©¿-3 ¿º±º±¼ .2 ÝØØ ×2½±º±¿¿¿¼ »º±¿¿¿¿-ª»§ §±«²¹ ©¿-¿. òí ©:ð Ĩ .-3 ¿¿¿¿¿.¿.
«²½±²-±:¼¿¿¼ ¿²¼ -«¼¿½¿½-»»³ »²-ð Ĩ » »³ ¿.²¼»º±º¿ »¿¿¿¿¿ ¿¿¿-3 ¿º±º±¼ ¿-±¼ ¿'«ª.¿'
º¿² ¼»º±-»- òí ±º í ð

Ĩ »» ¼±»²¹ ©¿-¼»'»¼ .2 ¿.- °¿²².21 ¿»¿ øPóí èð Póí Çò ¿²¼ Póí í ð Ĩ » -±.'º±º.' » .2 ¿ »
¼±»¿¿¿ ¿¿¿ ¿¿-¿-º±'±©-½

Póí ç Ñ¼ ß'«ª.¿' Ú¿² Ú»º±-»- òí ±º í ð
Póí è Ñ¼ ß'«ª.¿' Ú¿² Ú»º±-»- òí ±º í ð

Đ±º±»¼ 3 ¿-- 1º¿¼.21 º±º¿.- -»» .- °.¿²¼ ½«-0±0'º-º¿²-¿±² 1º¿¼.21ð Ó¿.¿³ «³ °±º±»¼ 0'º.
1º¿¼.21 .- ±² ¿ » ±¼»º±º í í »»-2 ¿ »-±¿¿¿»² ¼¿¿¿.¿¿¿¹ » ¿¿¿.0 Ó¿.¿³ «³ ¼»º±º±»¼ ½«-
1º¿¼.21 .- í è .2 ¿ » 3 ±-¿ 2±¿¿¿¿² °¿¿¿±º ¿ » ±ð Ĩ » »½±³ 3 »²¼»¼ ±ª»»'½¿ª¿±² º±º¿ » °.
º±º±² ±º ¿ »-»» .- í ð »»-2 ¿ » ¼¿¿¿.¿¿¿¹ »- ¿²¼ è »»»-»»»º »ºº »ºº ÝØØ ×2½±º±¿¿¿¼ »º±º±
ß»¿¿-º±º±»¼ º±º±³ »¿¿¿¿.² í í »»»±º ½«-1º¿¼.21 3 ¿§ 2±¿¿¿'«»±ª»»'½¿ª¿±² ¼«²¹ 3 ¿--
1º¿¼.21ð ß»¿¿-º±º±»¼ º±º'--¿¿¿.² í í »»»±º ½«-1º¿¼.21 -¿±«¼ ¼»±ª»»'½¿ª¿±² ¼±±¼-»²ª»
¿ » í í »»»»½±³ 3 »²¼»¼ »³ ±ª¿

Ĩ » »¿²².21 ¿»¿ 1º¿¼.21 .2½«¼»-º.'º±ª»º½«-±º»-ð Ĩ »-»- ±º»-¿» ¼»-1.2»¼ ¿¿¿ î Ø»î Èð
Ĩ » -±º»-º¿²¹ »º±³ èð ¿±²¹ ¿ »-±¿¿¿-¼»±º ¿ » ±¿±¿¿¿¿º¿¿¿.2 ¼»-©»² ¿ » °¿¼-ð í ±º»-
±ª»º í ð »»¿¿ »º±ª.¼»¼ ©.¿ ¿ è °»»©.¼» ¼»²½¿.0 ¿-¿.±©² ±² ¿ » ½±²½»º¿¿ ¿ 1º¿¼.21 °¿²-ð

Đ'¿²².21 ß»¿ è ò0±½ ð±½

Ĩ .- í ò Ĩ ½»- -»» .- °±º±»¼ º±º³ «-¿º¿³ .§ »-¼»²¿¿ «-»ð Ĩ » -»» -'±º»- ±¿¿¿¼ ¿ »-±¿¿¿¿ ¿
¿¿¿-º¿².21 º±³ ð è ± í í ð è °»½»²-ð ß ¼¿¿¿.¿¿¿¹ » ½±«-» ½«-¿¿¿¿±«¹ ¿¿¿¿ ¿»¿¿¿.2 2±¿¿¿¿-±¿¿¿
¼»½¿±²0 Ĩ » ¼¿¿¿.¿¿¿¹ » °¿¿¿ ¼»-½»²¼ -±¿¿¿¿² ¿¿¿¿¿.² ¿º±º±.³ ¿¿¿¿ ¿¿¿± ° èð è °»½»²-ð Ĩ » -±.
.2 ¿ » ¼¿¿¿.¿¿¿¹ » ©¿-3 ¿º±º±¼ .2 ÝØØ ×2½±º±¿¿¿¼ »º±¿¿¿¿-ª»§ §±«²¹ ©¿-¿. òí ©:ð Ĩ .-3 ¿¿¿¿¿.¿.
. «²½±²-±:¼¿¿¼ ¿²¼ -«¼¿½¿½-»»³ »²-ð

Ĩ »» ¼±»²¹ -©»» ¼»'»¼ .2 ¿.- °¿²².21 ¿»¿ øPóí ð Póí ò ¿²¼ ¼óí í ð Ĩ » -±.'- .2 ¿ »-» ¼±»¿¿¿¿¿-
©»»³ ¿º±º±¼ ¿-º±'±©-½

Póí Ñ¼ ß'«ª.¿' Ú¿² Ú»º±-»-
Póí Ñ¼ ß'«ª.¿' Ú¿² Ú»º±-»-
Póí í í »»»±º È»§ Ç±«²¹ È ¿-¿.±ª»»ß'«ª.¿' Ú¿² Ú»º±-»-

Đ±º±»¼ 3 ¿-- 1º¿¼.21 º±º¿.- -»» .- ¿.º¿²-¿±² ½«-0±0'º-º¿²-¿±² 1º¿¼.21ð Ó¿.¿³ «³ °±º±»¼ ½«-
1º¿¼.21 .- ±² ¿ » ±¼»º±º í í »»-2 ¿ »-±¿¿¿»² ¼¿¿¿.¿¿¿¹ » ¿¿¿.0 Ó¿.¿³ «³ ¼»º±º±»¼ ½«-
»½±³ 3 »²¼»¼ ±ª»»'½¿ª¿±² º±º¿ » °.º±º±² ±º ¿ »-»» .- í ð »»-º »ºº »ºº ÝØØ ×2½±º±¿¿¿¼ »º±º±
ß»¿¿-º±º±»¼ º±º±³ »¿¿¿¿.² í í »»»±º ½«-1º¿¼.21 3 ¿§ 2±¿¿¿'«»±ª»»'½¿ª¿±² ¼«²¹ 3 ¿--
1º¿¼.21ð ß»¿¿-º±º±»¼ º±º'--¿¿¿.² í í »»»±º ½«-1º¿¼.21 -¿±«¼ ¼»±ª»»'½¿ª¿±² ¼±±¼-»²ª»
¿ » í í »»»»½±³ 3 »²¼»¼ »³ ±ª¿

Y±2½»°~«¿' Đ'¿² Á »ª.»©Ń Ē2.ª»®.-§ Ø.~' - Í °»½º.½ Đ'¿²
Y.-§ ±º Í ¿² Þ»®¿¿²±±0 Y¿:º±®¿.¿

Đ®±¶»½- Ò±0 éđđđí óđđí
Ú»½»³ ¼»® í 0 í đđé

Ì ¿ » °¿²².21 ¿®¿¿ 1®¿½.21 .2½'«¼»- °.~' ¿²¼ °.~'±ª»®½¿«- ±±º»-0 Ì ¿ »-» - ±±º»- ¿®» ¼»- .1²»¼ ¿-
î Øđđí Èđ Ì ¿ » - ±±º»- ®¿²¹ »®±³ í ð ±± èðº»»¿.2 ¿.1 -0 Í ±º»- ±ª»® í ðº»»¿¿¿® »®±ª.¼»¼ ©.¿ ¿ è
º»»¿¿.¼» ¼»²½.0 ¿- - ¿.±©² ±² ¿.¿ ½±²½»°~«¿' 1®¿½.21 °¿²²-0

Đ'¿²².21 ß®»¿ è 00±¿íí÷

Ì ¿.- î òì ¿½®»- --¿. -- °®±º±-»¼ °±® ¿ °¿®µò Ì ¿ » °¿®µ .2½'«¼»- - °±®.- °.»¼- ¿²¼ ¿ ¼«¼.¼.21 ð Ì ¿ »
°¿²².21 ¿®»¿ - ±±º»- ±±©¿¼ ¿ ¿. - ±¿¿. ©»-¿ ¿² ¿ °®±~.3 ¿-»® ¿¿±º ì ð èº»®½¿²-0 Ñ²» ¼±®¿²¹
ðPóí é÷ ¿¿- ¼«~'¼ ©.¿.2 ¿.¿ »¿¿¿¿ Ì ¿ » -±¿.² ¿.¿ ¼±®¿.±¿' ©¿- 3 ¿º»¼ ØYØØ x2½±®±®¿¿¿¼÷
¿- ±¼ ¿'«ª.¿'¿² ¼»º±--¿- òí ±ºí ÷0

Đ®±º±-»¼ 3 ¿-- 1®¿½.21 °±®¿.~ --¿. -- ¿-¿¿²--¿±² ½¿«0±0.~' 1®¿½.21 Ò¿~.3 «3 °®±º±-»¼ ½¿«-
1®¿½.21 -- ±² ¿.¿ » ±¼»®±º ì èº»»¿¿¿¿¿¿²¼ 3 ¿~.3 «3 °.~' 1®¿½.21 -- ±² ¿.¿ » ±¼»®±º ì ðº»»¿-0 Ì ¿ »
®½±³ 3 »²¼»¼ ±ª»®»~'½¿ª¿¿±² °±®¿.¿ °.~' °±®±² ±º ¿.¿ » --¿. -- íº»»-0 »®YØØ x2½±®±®¿¿¿¼®»º±®
ß®¿¿- °®±º±-»¼ °±®±³ ±®» ¿¿² íº»»¿±º ½¿«- 1®¿½.21 3 ¿§ 2±¿®»~«®» ±ª»®»~'½¿ª¿¿±² ¼«®¿²¹ 3 ¿--
1®¿½.21 ð ß®¿¿- °®±º±-»¼ °±®' -- ¿.¿² íº»»¿±º ½¿«- 1®¿½.21 - ¿.±«¼ ¼¼» ±ª»®»~'½¿ª¿¿¿¼ ±±¼-»®ª
¿.¿ íº»»¿¿¿¿¿¿²¼ ¼»³ ±ª¿¿

Đ¿¿½' 1®¿½.21 .2½'«¼»- °.~'±ª»®½¿«- ±±º»-0 Ì ¿ »-» - ±±º»- ¿®» ¼»- .1²»¼ ¿-î Øđđí Èđ Ì ¿ » ³ ¿~.3 «3
¿.1 -¿ ±º °®±º±-»¼ - ±±º»- -- ±² ¿.¿ » ±¼»®±º ì èº»»¿-0 Í ±º»- ±ª»® í ðº»»¿- ¿.±«¼ ¼¼» °®±ª.¼»¼ ©.¿
¿ èº»»¿¿.¼» ¼»²½.0 ¿- - ¿.±©² ±² ¿.¿ ½±²½»°~«¿' 1®¿½.21 °¿²²-0

Đ'¿²².21 ß®»¿ è 00±¿íí÷

Ì ¿.- ì òì ¿½®»- --¿. -- °®±º±-»¼ °±® 3 «~0¿¿³.¿®»-¼¿²¿¿¿ «-»ð Ì ¿ » --» - ±±º»- ±±©¿¼ ¿ ¿. - ±¿¿. ¿-
®¿¿-®¿.21.21 °®±³ í ð è±± ì ð èº»®½¿²-0 ß¼®¿.¿¿¿¿ ½±«®»- ½¿«- ¿.¿±«¹ ¿.¿ » -±¿¿. ¿-¿-½±²²»®±º
¿.¿ » °¿½' » .2 2±®¿.¿ »¿-0-±¿¿. ©»-¿¼.®»¿¿±² Ì ¿ » ¼®¿.¿¿¿¿¹ » °¿.¿ ¼-½¿²¼- - ±¿¿. ©»-»®§ ¿ ¿¿²
¿º»®±~.3 ¿-»® ¿¿±º ì ð èº»®½¿²-0 Ì ¿ » -±¿.¿¿¿¿±º ¿.¿ ¼®¿.¿¿¿¿¹ » °¿.¿ ©¿- 3 ¿º»¼ .2 YØØ
x2½±®±®¿¿¿¼®»º±®¿¿- §¿«²¹ ¿'«ª.¿'¿² ¼»º±--¿- òí §ºí ÷0 ¿²¼ ©»-¿±º ¿.¿ ¼®¿.¿¿¿¿¹ » °¿.¿ ¿- ±¼
¿'«ª.¿'¿² ¼»º±--¿- òí ±ºí ÷0 Í «³ 3 ¿§ ±º ¿.¿ » -±¿. °®±º.~.2 ¿.¿ ¼±®»¿.±¿' -- ¿- °±±±©-#

Póí î éº»»¿±º Ç±«²¹ ß'«ª.¿' Ú¿² Ò»º±--¿- òí §ºí ÷ ±ª»® Ñ¼ ß'«ª.¿' Ú¿² Ò»º±--¿- òí ±ºí ÷
Póí è Ñ¼ ß'«ª.¿' Ú¿² Ò»º±--¿- òí ±ºí ÷

Ì ¿ » ³ ¿½®-§ ±º °®±º±-»¼ 3 ¿-- 1®¿½.21 °±®¿.~ --¿. -- ½¿«- 1®¿½.21 »'½»º-¿±®¿.¿ ¼®¿.¿¿¿¿¹ » °¿.¿
©»®» ¿º»®±~.3 ¿-»® §'í ðº»»¿±º °.~' -- °®±º±-»¼ ð Ì ¿ » ³ ¿~.3 «3 °®±º±-»¼ ½¿«- 1®¿½.21 ¿±²¹ ¿.¿ »
2±®¿.¿®² »²¼- ±º ¿.¿ » °¿½' » -- ±² ¿.¿ » ±¼»®±º ì ðº»»¿-0

Ì ¿ »®½±³ 3 »²¼»¼ ±ª»®»~'½¿ª¿¿±² °±®¿.¿ °.~' °±®±² ±º ¿.¿ » --¿. -- éº»»-0 »®YØØ x2½±®±®¿¿¿¼
®»º±® ß®¿¿- °®±º±-»¼ °±®±³ ±®» ¿¿² íº»»¿±º ½¿«- 1®¿½.21 3 ¿§ 2±¿®»~«®» ±ª»®»~'½¿ª¿¿±² ¼«®¿²¹
3 ¿-- 1®¿½.21 ð ß®¿¿- °®±º±-»¼ °±®' -- ¿.¿² íº»»¿±º ½¿«- 1®¿½.21 - ¿.±«¼ ¼¼» ±ª»®»~'½¿ª¿¿¿¼ ±±
±¼-»®ª ¿.¿ í ðº»»¿¿¿¿¿¿²¼ ¼»³ ±ª¿¿

Ì ¿ » °¿²².21 ¿®»¿ 1®¿½.21 .2½'«¼»- °.~'±ª»®½¿«- ±±º»-0 Ì ¿ »-» - ±±º»- ¿®» ¼»- .1²»¼ ¿-î Øđđí Èđ
Ì ¿ » - ±±º»- ®¿²¹ »®±³ í ð ±± èèº»»¿.2 ¿.1 -0 Í ±º»- ±ª»® í ðº»»¿¿¿® »®±ª.¼»¼ ©.¿ ¿ èº»»¿¿.¼»
¼»²½.0 ¿- - ¿.±©² ±² ¿.¿ ½±²½»°~«¿' 1®¿½.21 °¿²²-0

Y±2h»°-«z' D'z² Î »ª.»©Ù Ê2.ª»®.-§ Ø.'- Í °»½ª.½ D'z²
Y.-§ ±° Í z² P»®z¼.ª±²±0 Yz:°±®z.

D®±½»½- Ö±0 êððí òðí
Ù»½»³ ¾»® í ò ì ððê

D'z²2.21 B®»z Ç Ø0±rìí±#

Ì º.- í òì z½®- --» - . °®±°±-»¼ 0±®³ «'r0z³ .§ ®»-¼»²z' «-»ð Ì º» -r» -'±° -r±©z¼ r¸»
-±«r¸ ©-r z' z² z' °®±' .3 z' ®z» ±° ïïðè °®½»²± Ì ©± ¼®z.²z¹ » ½±«®-»- ½«-r¸ ±«¹ º. r¸» --» .2
2±®z¸ z'-ò-±«r¸ ©-r ¼.®»½r±²ð Ñ²» - . ±½z»¼ z'r¸ » 2±®z¸ ©-r ½±®²»® ±° r¸» -r» z'¼ ±² z' ±©z¼
r¸ » ½²»²»® ±° r¸» --»ð Ì º» ¼®z.²z¹ - ¼»-½²¼ -±«r¸ ©-r»®§ z'r z² z' °®±' .3 z' ®z» ±° ïï °®½»²±
Ì º» -«®.½z' --» -±' .- ³ z' °»¼ z' - §±«²¹ z' «ª. z' °z² ¼» ±° -r- òí §õí ÷ °» YØØ x²½±® ±®z»¼ ¼® ±°®
Í «³ ³ z' §±° r¸» -±' °®±°. 2 r¸ » ¾±®» ±' - z' -°±'±©-#

P0ç è °»»r±° Ç±«²¹ B''ª.z' Úz² Ü»°±--r- òí §õí ÷ ±ª»® Ñ¼ B''ª.z' Úz² Ü»°±--r- òí ±°í ÷

D®±°±-»¼ ³ z-- 1®z¼.21 0±®r¸.- °z²2.21 z' ®z» - z' r¸z²--r±² ½«-ò±0.°' 1®z¼.21 ò z' .3 «³
°®±°±-»¼ ½«z' z'¼ .°' 1®z¼.21 - ±² r¸ » ±®¼® ±° ïè °»»ð Ì º» ®½±³ ³ »²¼¼¼ ±ª»®»'½zª z'r±² 0±®r¸ »
°' °®±r±² ±° r¸» --» - . ï ò °»»ð °» YØØ x²½±® ±®z»¼ ¼® ±°® B®z' - °®±°±-»¼ 0±®³ ±® z' z' ïï
°»»r±° ½« 1®z¼.21 ³ z' §²±r® - «.®» ±ª»®»'½zª z'r±² ¼«²¹ ³ z-- 1®z¼.21 ò B®z' - °®±°±-»¼ 0±®» -
r¸z² ïï °»»r±° ½« 1®z¼.21 - ±«¼¼¼ ±ª»®»'½zª z'r±² ±±¼-»®ª r¸ » ïï °»»r±° ½±³ ³ »²¼¼¼
®»³ ±ªz' ò

Ì º» ®½±³ ³ »²¼¼¼ ±ª»®»'½zª z'r±² 0±®r¸ » .°' °®±r±² ±° r¸ » --» - . é °»»r±° -»²»z' ®½§ ¾±®²¹ P0í ì ÷
°» YØØ x²½±® ±®z»¼ ¼® ±°® B®z' - °®±°±-»¼ 0±®³ ±® z' z' é °»»r±° ½« 1®z¼.21 ³ z' §²±r® - «.®»
±ª»®»'½zª z'r±² ¼«²¹ ³ z-- 1®z¼.21 ò B®z' - °®±°±-»¼ 0±®» --r¸z² é °»»r±° ½« 1®z¼.21 - ±«¼¼¼
±ª»®»'½zª z'r±² ±±¼-»®ª r¸ » é °»»r±° ½±³ ³ »²¼¼¼ ®»³ ±ªz' ò

Dz'®½»' 1®z¼.21 .2½«¼¼ - .°' °±ª»®½«-r±° -ò Ì º» -» -'±° -z' ¼» - .1²¼ z' r±² Øæí Êð Ì º» ³ z' .3 «³
» .1 r±² °®±°±-»¼ - ±² r¸ » ±®¼® ±° ïè °»»ð Ì º» - ±ª»® ï ò °»»r±° °®±ª.¼¼ ©.r¸ z' è
°»»r±° .¼¼ ¾¼²½z' ò z' - ±±©² ±² r¸ » ®±«¹ 1®z¼.21 °' z' -ò Í º» ®z' - »¹³ »²z' ®z' z.2.21 -r®½«®-
z' °®±°±-»¼ ±² °z'®½»' -'±° -ò Ì º» -r®½«®- z' ¼» - .1²¼ z' r±² Øæí Êð

D'z²2.21 B®»z ï ð Ø0±rìí±#

Ì º.- èòì z½®- --» - . °®±°±-»¼ 0±® .21 »0z³ .§ ®»-¼»²z' «-»ð Ì º» '±²¹ z'¼ z' z'±² ±²±²
proposed for 21 pads. Two third of the "L" shaped lot is oriented in north°-±«r¸ ¼.®»½r±² z'¼ ±²»
r¸ .¼ .2 » z' -r ©-r ¼.®»½r±² Ì º» --» - . «¹¹¼ z'¼ -'±° -r±©z¼ r¸ » -±«r¸ z'¼ -±«r¸ ©-r z' z'
®z' - .®z¹ - .°®±³ é ±ï ð °®½»²± Ù±«®³ .2±®¼®z.²z¹ » ½±«®-»- ½«-r¸ ±«¹ º. r¸ » z' z' .2 -±«r¸ »®§
¼.®»½r±² Ì º» - ±' ±² r¸.- ±r- ©z' - ³ z' °»¼ .2 YØØ x²½±® ±®z»¼ ¼® ±°® z' - °±'±©-#

Ì º» 2±®z¸ 0-±«r¸ °®±r±² ±° r¸ » ±r	Ê»®§ Ç±«²¹ Ê z' - òí ©÷ ±ª»® B''ª.z' Úz² òí °÷
Ì º» » z' -ò©»-r ±®±r±² ±° r¸ » ±r	Ñ¼ B''ª.z' Úz² Ü»°±--r- òí ±°í ÷
Ì º» ³ ±r- ±«r¸ »®§ ¼®z.²z¹ » ½±«®-»	Ê»®§ Ç±«²¹ Ê z' - òí ©÷ ð

Ì º» ª»®§ §±«²¹ ©z' - òí ©÷ - . «²½±² - ±'¼z»¼ z'¼ - «¾¼»½r±² - »-r'³ »²± Ù±«®¾±®²¹ - ©»® ¼®z'¼
±² z'¼ z'¼½z'²z' r±² r¸.- ±± Ì º» - ±' °®±°. 2 r¸ » ¾±®» ±' ©z' - z' -°±'±©-#

P0í Ê»®§ Ç±«²¹ Ê z' - òí ©÷
P0í ç Ñ¼ B''ª.z' Úz² Ü»°±--r- òí ±°í
P0í í Ê»®§ Ç±«²¹ Ê z' - òí ©÷ ±ª»® B''ª.z' Úz² òí °÷
P0í í Ê»®§ Ç±«²¹ Ê z' - òí ©÷ ±ª»® B''ª.z' Úz² òí °÷

Y±2½»°-«¿ Đ'¿² Ā »ª.»©Ī Ē2.ª»-š Ø.°- í °½°½ Đ'¿²
Y-š ±° í ¿² Þ»²¿½±² Y¿:°±²¿

Đ±½»½- Ò±ò éððí òðí
Ú½»³ ¾»í ò ððè

Đ±°±-»¼ ³ ¿-- 1°¿¼.21 °±²¿- --»- .- °.¿ ¿²¼ ½«-ò±²°''-²-¿±² 1°¿¼.21 ò ¿ »-²-¿±² ½«-ò±²°''
1°¿¼.21 .- °±°±-»¼ .2 ¿ »²±²¿ »² °±²±² ±° ¿ »--»ð Y«¿ ¿²¼ °.¿ 1°¿¼.21 .- ±² ¿ »±½¿»±° Ç°»»ð
¿ »-±¿¿ »² °±²±² ±° ¿ »--»- .- °±°±-»¼ °±² è ±î è °»»±²°'' 1°¿¼.21 ò

¿ »»½±³ ³ »²¼»¼ ±ª»''½¿ª¿±² °±²¿ »°'' °±²±² ±° ¿ »--»- .- í î °»»° »YØØ x²½±²°±¿¿½¼
»°±²±² ß»¿- °±°±-»¼ °±²³ ±²¿ ¿ ¿² í î °»»±² ½«- 1°¿¼.21 ¿ ¿²±¿ »«» ±ª»''½¿ª¿±²
¼«²¹ ³ ¿-- 1°¿¼.21 ò ß»¿- °±°±-»¼ °±² »-- ¿ ¿² í î °»»±² ½«- 1°¿¼.21 - ¿ ±¼¾
±ª»''½¿ª¿±² ±¼±¾-»ª» ¿ ¿² í î °»»»½±³ ³ »²¼»¼ »³ ±ª¿ ò

Đ¿¿.2.21 ¿»¿ 1°¿¼.21 .2½«¼- °.¿ ½«-ò ¿²¼ °.¿ °±²±²°±²¿«- ±° »-ò ¿ »- »- ±° »- ¿» ¼- .1²»¼ ¿
î Òðí Èò ¿ »°'' - ±° »- ¿» ¿ ±²¹ ¿ »-±¿¿ »² -¼ ±²¿ »°¿½' ©.¿ ¿ ³ .3 «³ ¿ .1 ¿ ±° í è °»»ð
¿ »½«- ¿²¼ °.¿ °±²±²°±²¿«- ±° »- ¿» ¾¿-©»² ¿ »°¿½' .2¼.ª.¼¿¿ ° ¿¼-ò ¿ »- »- ±° »- ¿» ±² ¿ »
±½¿»±² ò ð ± î è °»»±² ¿ » .1 ¿ ò

Đ¿¿.2.21 ß»¿¿ í î òð±¿ ì è ð

¿ .- èòÇ ¿½»- --»- .- °±°±-»¼ °±²³ «-¿²¿³ .¿ »-¼¿²¿ ¿ »-ò ¿ » ±²¹ ¿²¼ 2¿±²© ±¿-
°±²±²¿½ °±² Ç ° ¿¼-ò í »ª»¿ ¿¼¿.2¿¹ »½±«- »²¼ .2 ¿¼ ¿¿¿¿¿¿- °¿½' ò ¿ » --»- .- »¹ 1½¼
¿²¼ - ±° »- ±¿¿ ¿¼ ¿ »-±¿¿ ©-¿¿¿¿¿¿² ¿ °±² .3 ¿¿ »¿¿ ±² ò ò »½'²ò ¿ »- ±¿ ±² ¿ .- ±¿ ©¿-
³ ¿ °¿¼ .2 YØØ x²½±²°±¿¿½¼ »°±²¿¿- °±²±²-»

¿ » ¿¿-¿-¼» ±² ¿ »°¿½'
¿ » ½»²¿»° °±²±² ±² ¿ »°¿½'
¿ » ©-¿-¼» ±² ¿ »°¿½'
Ñ¼ ß''ª.¿ ¿¿² ¿ »°±-¿- òí ±°í ÷
Ç±«²¹ ß''ª.¿ ¿¿² ¿ »°±-¿- òí §°í ÷
Ç±«²¹ ß''ª.¿ ¿¿² ¿ »°±-¿- òí §°è-ð

Ú±«¾±²¹- ©»» ¼»''¼ ±² ¿²¼ ¿¼¿½¿²¿¿¿¿¿¿¿- ±ò ¿ »- ±°±²°' .2 ¿ »¾±»±¿ ©¿-¿-
°±²±²-»

- Póí ð Ç±«²¹ ß''ª.¿ ¿¿² ¿ »°±-¿- òí §°í ÷
- Póí í í °»»±² Ú.'±ª»² Ç±«²¹ ß''ª.¿ ¿¿² ¿ »°±-¿- òí §°è-ð
- Póí ì Ç±«²¹ ß''ª.¿ ¿¿² ¿ »°±-¿- òí §°í ÷
- Póí ç Ñ¼ ß''ª.¿ ¿¿² ¿ »°±-¿- òí ±°í ÷

Đ±°±-»¼ ³ ¿-- 1°¿¼.21 °±²¿- --»- .- °.¿ ©.¿ 3 .2±²½¿¿ 1°¿¼.21 2±¿ »½»»¼.21 °ª»»»»ð ¿ »
°±²±²¿½ °.¿ ±² ¿ .- ±¿¿ ¿²¹ »- °±² è ±î è °»»±² ¿ .½µ² »-ò ¿ » ¼»»°-¿°''- ¿ » .2 ¿ »¼¿¿ ±²
¿ » ¼¿¿.2¿¹-ò

¿ »»½±³ ³ »²¼»¼ ±ª»''½¿ª¿±² °±²¿ »°'' °±²±² ±° ¿ »--»- .- ±² ¿ »±½¿»±² í ± è °»»±²° »
YØØ x²½±²°±¿¿½¼ »°±²¿ »½¿¿- °±²¿ ¿ »¿ .2 ¿ »ª.½.2-š ±² ¾±²¹ Póí Òò ©¿ »¿ ¿ »
±ª»''½¿ª¿±² .2 ¿ »¼¿¿-¿- »½±³ ³ »²¼»¼ °±² í î °»»»ð

Đ¿¿.2.21 ¿»¿ 1°¿¼.21 .2½«¼- °.¿ - ±° »-ò ¿ »- »- ±° »- ¿» ¼- .1²»¼ ¿¿¿¿¿¿ Èò ¿ »°'' - ±° »-
¾¿-©»² ¿ »°±²±²¿½ .2¿»°±² ° ¿¼- ¿» ±² ¿ »±½¿»±² ò ð ± î è °»»±² ¿ » .1 ¿ ¿²¼ ¿ »°±² »»³ »°°.
- ±° »- ¿» ±² ¿ »±½¿»±² í è °»»±² ¿ » .1 ¿ ò ß -» 1³ »²¿¿¿¿¿¿.2.21 ©¿ -¿«½¿¿- .- °±°±-»¼ ±²
¿ .- °¿½' - ±° »-ò ¿ » --»½«-¿- ¿» ¼- .1²»¼ ¿¿¿¿¿¿ Èò

Ý±2½»°«¿' Đ'¿² Î »ª.»©Ù È².ª»®.-§ Ø.'- Í °½º.½ Đ'¿²
Ý.-§ ±° Í ¿² Þ»®¿¿²±±½ Ý¿:º±®¿.¿

Đ®±½»½- Ò±± èððí òðí
Ù»½»³ ¼»® í ò ì òðé

Đ'¿²².21 ß®¿¿¿¿ ò±±- ì è ¿²¼ ì è:»

Ì ¿.- °¿²².21 ¿®¿¿¿¿ ½±²--¿- ±°-¿±' ±±- ¿²¼ -- °®±° ±-»¼°±® -21' » °¿³. § ®¿-¼»²¿¿ «-»ð Ò±±ì è --
ì òí ¿½®¿- ¿²¼ Ò±±ì è -- ì òç ¿½®¿-ò Ì ¿ --»- '±°»- ±±¿¿¿¿¿ ¿- ±«¿¿ ¿²¼ -±«¿¿¿-¿ ¿¿²
¿°°®±'³ ¿»®¿-» ±° í ò è ± ì è ò è °»½»²ò Ì ©± ¼®¿.2¿¹ » ½±«®-»- ½«¿-¿¿±«¹ ¿¿.- °¿²².21 ¿®¿¿¿¿
½¿«-21 ¿» ±±°¹®¿. § ±± ¼»®«¹¹»¼ Ì ¿ --±' ±² ¿.- °¿²².21 ¿®¿¿¿¿ ©¿- 3 ¿°°»¼ .2 ÝØØ
×²½±®±®¿¿¿¼®¿° ±®¿¿¿- ±¼ ¿'«ª.¿' ¿² ¼»° ±-¿- òí ±°í ò

Ì ¿»» ¼±®.21- ©»®» ¼®¿'»¼ ±² ¿²¼ ¿¼¿½¿²¿ ±¿¿¿- '±± Ì ¿» -±' °®±°.' » .2 ¿» ¼±®»¿±' ©¿- ¿-
°±'±©-»

- Đòì Ñ¼ ß''ª.¿' Ù¿² Ù»° ±-¿- òí ±°í ÷
- Đòé Ñ¼ ß''ª.¿' Ù¿² Ù»° ±-¿- òí ±°í ÷
- Đòè Ñ¼ ß''ª.¿' Ù¿² Ù»° ±-¿- òí ±°í ÷
- Đòí Ñ¼ ß''ª.¿' Ù¿² Ù»° ±-¿- òí ±°í ÷

Đ®±° ±-»¼ 3 ¿-- 1®¿¼.21 °±®¿¿.- --»- -- °.' ¿²¼ ½«-ò±ò.' -®¿²-¿±² 1®¿¼.21 ò Ì ¿» °®±° ±-»¼ °.' ±² ¿¿.-
°¿²².21 ¿®¿¿¿¿¿²¹ »- °®±³ è ±± í è °»»¿.2 ¿. ½µ²-- ¿²¼ ¿» ½«¿ °±®±² ®¿²¹ »- ¼»¿-¿»»² è ¿²¼ è
°»»¿.2 ¼»° ¿¿ Ì ¿» ®¿½±³ 3 »²¼»¼ ±ª»®»' ½¿ª¿±²² °±®¿¿. °.' °±®±² ±° ¿» »-»- -- ±² ¿» ±®¼»®±° í
± è °»»¿ »® ÝØØ ×²½±®±®¿¿¿¼®¿° ±®±ò

Đ'¿²².21 ¿®¿¿¿¿ 1®¿¼.21 .2½«¼»- °.' ±ª»®½«¿- '±°»-ò Ì ¿»-»- '±°»- ¿®¿ ¼»--1²»¼ ¿¿ òðè È ò Ì ¿»
-±°»- ®¿²¹ » .2 ¿» .1 ¿.- °®±³ ì ò ±± í è °»»¿

Đ'¿²².21 ß®¿¿¿¿ ò±±- ì è ¿²¼ ì è:»

Ì ¿.- °¿²².21 ¿®¿¿¿¿ ½±²--¿- ±°-¿±' ±±- ¿²¼ -- °®±° ±-»¼°±® -21' » °¿³. § ®¿-¼»²¿¿ «-»ð Ò±±ì è --
ì ò è ¿½®¿- ¿²¼ ©.' ¼» 1®¿¼»¼ .2 ±± í ¿'¿¹ » °¿¼-ò Ò±±ì ç- í òì ¿½®¿- ¿²¼ -- °®±° ±-»¼°±® ±«®¿¿¿¿¿
1®¿¼»¼ °¿¼-ò Ì ¿» --»- '±°»- ±±¿¿¿¿¿ ¿- ±«¿¿ ¿¿¿² ¿°°®±'³ ¿¿»®¿-» ±° í ò ±± í ò è °»½»²ò Ì ¿»
-±' ±² ¿¿.- °¿²².21 ¿®¿¿¿¿ ©¿- 3 ¿°°»¼ .2 ÝØØ ×²½±®±®¿¿¿¼®¿° ±®¿¿¿- ±¼ ¿'«ª.¿' ¿² ¼»° ±-¿-
òí ±°í ò

Ì ¿»» ¼±®.21- ©»®» ¼®¿'»¼ ±² ¿²¼ ¿¼¿½¿²¿ ±¿¿¿- '±± Ì ¿» -±' °®±°.' » .2 ¿» ¼±®»¿±' ©¿- ¿-
°±'±©-»

- Đòì Ñ¼ ß''ª.¿' Ù¿² Ù»° ±-¿- òí ±°í ÷
- Đòé Ñ¼ ß''ª.¿' Ù¿² Ù»° ±-¿- òí ±°í ÷
- Đòí Ñ¼ ß''ª.¿' Ù¿² Ù»° ±-¿- òí ±°í ÷

Đ®±° ±-»¼ 3 ¿-- 1®¿¼.21 °±®¿¿.- --»- -- °.' ¿²¼ ½«-ò±ò.' -®¿²-¿±² 1®¿¼.21 ò Ì ¿» °®±° ±-»¼ °.' ±² ¿¿.-
°¿²².21 ¿®¿¿¿¿¿²¹ »- °®±³ è ±± í è °»»¿.2 ¿. ½µ²-- ¿²¼ ¿» ½«¿ °±®±² ®¿²¹ »- ¼»¿-¿»»² ì ò ¿²¼ ì ò
°»»¿.2 ¼»° ¿¿ Ì ¿» ®¿½±³ 3 »²¼»¼ ±ª»®»' ½¿ª¿±²² °±®¿¿. °.' °±®±² ±° ¿» »-»- -- ±² ¿» ±®¼»®±° í
± è °»»¿ »® ÝØØ ×²½±®±®¿¿¿¼®¿° ±®±ò

Đ'¿²².21 ¿®¿¿¿¿ 1®¿¼.21 .2½«¼»- °.' ±ª»®½«¿- '±°»-ò Ì ¿»-»- '±°»- ¿®¿ ¼»--1²»¼ ¿¿ òðè È ò Ì ¿»
-±°»- ®¿²¹ » .2 ¿» .1 ¿.- °®±³ í è ±± é è °»»¿ ß -»¹³ »²¿-¿'®¿-¿.2.21 ©¿¿' -¿«½-«®¿- -- °®±° ±-»¼ ±²
¿¿.- °¿²².21 ¿®¿¿¿¿ '±°»-ò Ì ¿» -®¿½-«®¿- ¿®¿ ¼»--1²»¼ ¿¿ òðè È ò Ì ¿»

Ý±2½»°«¿´ Ð´¿² Î »ª.»© Æ².ª»..-§ Ø´´- Í´º½º½ Ð´¿²
Ý.-§ ±° Í´¿² Þ»ª¿¿ª²±± Ý¿:º±ª¿.

Ðª±ª»½-Ò±± èððí òðí
Û»½»³ ¼ª»í ò ì ððé

- Þóí ì Ç±ª²¹ ß´ª¿.¿´ Û¿² Û»º±--´- òí §°í ÷
- Þóí è é´º»»±°´´±ª»ª²¹ ß´ª¿.¿´ Û¿² Û»º±--´- òí §°í ÷
- Þóí í Ñ¼ ß´ª¿.¿´ Û¿² Û»º±--´- òí ±°í ÷

Ðª±º±-¼³ ¿-- 1ª¼.21 º±ª¿.- --¿. - ½«±±0´´-ª¿²--ª±² 1ª¼.21ò Ì » º±º±-¼³´´ª²¹»- .2
 ¯.¼µ²»-- º±³ Ì ð ± ì ì´º»»¿²¼ ¯¿ ½«¹ 1ª¼.21 º¿²¹»- .2 ¼ªº±³ ì ± è´º»»ò Ì »
 º±³ 3 »²¼ª¼±ª»ª²¹ª¿.¿´¿² º±ª¿±´´¿² 3 »²±°´´º±ª±².- º±³ í ± è´º»»¿.2 ¼ªº±³ ºªÝØØ
 ×²½±ªº±ª¿¼ª»º±ª¿ ßª»º±º±-¼³ º±ª³ º±ª¿.¿² í´º»»±°½«¹ 1ª¼.21 3 ¿²±ª»ª´ª»
 ±ªª»ª²¹ª¿.¿´¿² ¼ªª²¹ 3 ¿-- 1ª¼.21ò ßª¿¿- º±º±-¼³ º±ª¿´-- ¯¿¿² í´º»»±°½«¹ 1ª¼.21 - ,±ª¼¼ª
 ±ªª»ª²¹ª¿.¿´¿² ±±¼-ªª» ¯¿´º»»ª²±³ 3 »²¼ª¼ª»³±ª¿

Ð¿².21 ¿ª¿ 1ª¼.21 .2½ª¼»-´´-±´º»-ò Ì »-»-´´º»-¿ª»¼ª»-12»¼ ¿-¿Øªí Èò Ì » 3 ¿.3 º³
 ¿.1 ¯±° º±º±-¼³ -´º»- - ±² ¯¿ ±ª¼ª»º± Ì´º»»ò Í´±º- ±ªª»í ð´º»»- ,±ª¼¼ª º±ª¼ª¼ º±ª¼
 ¿ è´º»»ª¼ª»³ª²½¿

Ð¿².21 ßª¿¿¿ ò±±¿

This 0.5 acre site is proposed as a recreational facility. The facility's pad is located within

Ð¿².21 ßª¿¿¿ Ì´º»»¿²¹ º¿¼ ¯±±¹ª¿.¿´.¿´- -´º.21 ±ª¿ª¼ ¯¿-±ª¿ ¿¿¿±ºí ðè
 ´ºª²ò ß - ¿´±ª¿¼¿.¿²¿¹ º¿¼ ½«¹ ¯¿±ª¼ ¯¿»¿-¿¼±º ¯¿ º¿¼ .2 2±ª¿.0-±ª¿¼ª»½±²ò
 Ì » º¿¼ -±´- ºª» 3 ¿´ºº¼¼ªÝØØ ×²½±ªº±ª¿¼ ¿-ª»§ ±ªª²¹ º¿- ò ÷ .2 ¯¿ »¼¿.¿²¿¹ ¿²¼
 ¿- §±ª²¹ ¿´ª¿.¿´¿²¼ª»º±--´- òí §°í ÷ ±² ¯¿ ¯¿- ¯±º ¯¿ º¿¼

Ðª±º±-¼³ ¿¿-- 1ª¼.21 º±ª¿.- º¿¼.-´´- 1ª¼.21ò Ì » º±º±-¼³´´ª²¹»- º±³ è ± ì ì´º»»¿.2
 ¯.¼µ²»--ò Ì » ¯ª±³ 3 »²¼ª¼ª±ª»ª²¹ª¿.¿´¿² º±ª¿±´´¿² º±ª¿ º±º±-¼³´´- Í´º»»ò ºªÝØØ ×²½±ªº±ª¿¼ª»
 ¯ª±ª¿

Í´-¿ 1ª¼.21 .2½ª¼»-¿ í ì´º»»¿.1 ¯´´-±´º»ò Ì » -´º»-¿¼ª»-12»¼ ¿-¿Øªí Èò Í´±º- ±ªª»í ð
 ´º»»¿ª» º±ª¼ª¼ º±ª¼ ¿ è´º»»ª¼ª»³ª²½¿ ¿- - ,±ª² ±² ¯¿ ¯ª¼ 1ª¼.21 º¿²-ò

Ð¿².21 ßª¿¿¿ Ì´º»»¿

Ì´- èòí è ¿ªª»- --¿. - º±º±-¼³ º±ª¿.-.21»º¿³.¿´ª»-¼ª²¿¿´«-¿ò Ì » --¿. -´º»-±ª¿ª¼ ¯¿-±ª¿
 ¿¿¿±ºí ðè´ºª²ò Ì »ª»±ªº±ª»-¿´±ª¿¼¿.¿²¿¹» ½±ª»-»- ½«¹ ¯¿±ª¼ ¯¿»¿-¿¼±º ¯¿ º¿¼ .2 2±ª¿.0-±ª¿¼ª»½±²ò Ì » ¼ª¿.¿²¿¹ º¿¼ ½«¹ª²¼ -±ª¿ª»§ ¯¿¿² ¿´ºº¼¼ªÝØØ ×²½±ªº±ª¿¼ª»º±ª¿-ª»
 ¿´ºº¼¼ªÝØØ ×²½±ªº±ª¿¼ª»º±ª¿-ª»§ ±ªª²¹ º¿- ò ÷ Ì´-¿.3 ¿ª¿.¿´.¿´- ¿²½±²-±¼¿¿¼ ¿²¼ -ªª»½±²-»ª³ »²ò Ì » -±ª¿¿¿-
 ½±ª²º±ª¿¼ª»º±ª¿´´¿¿-¿ º¿¼ ¿- §±ª²¹ ¿´ª¿.¿´¿²¼ª»º±--´- òí §°í ÷ ¿²¼ ¯¿ ¯ª³ ¿.2.21 ±º ¯¿
 --¿ º¿-¿ º¿¼ ¿- ±¼ ¿´ª¿.¿´¿²¼ª»º±--´- òí ±°í ÷

Í´ ¼ªª²¹- ºªª¼ª»¼.2 ¯¿.- º¿².21 ¿ª¿¿¿ ðÞóí éò Þóí ì ò Þóí î ò Þóí í ò Þóí ðò ¿²¼ Þóí èò Ì » -±´
 º±ª¿.¿´- .2 ¯¿»-» ¼ªª¿±»-¿-¿-¿-º±±ª»-¿

- Þóí é Ñ¼ ß´ª¿.¿´ Û¿² ¼ª»º±--´- òí ±°í ÷
- Þóí ì í´º»»±°´´±ª»ª²¹ ß´ª¿.¿´ Û¿² Û»º±--´- òí §°í ÷ ±ªª»Ñ¼ ß´ª¿.¿´ Û¿² Û»º±--´- òí ±°í ÷
- Þóí î Ñ¼ ß´ª¿.¿´ Û¿² ¼ª»º±--´- òí ±°í ÷
- Þóí ð é´º»»±°´´±ª»ª²¹ ß´ª¿.¿´ Û¿² Û»º±--´- òí §°í ÷ ±ªª»Ñ¼ ß´ª¿.¿´ Û¿² Û»º±--´- òí ±°í ÷
- Þóí è Ñ¼ ß´ª¿.¿´ Û¿² ¼ª»º±--´- òí ±°í ÷

Ÿ±²½»°-«¿Ĵ ĐĴ² Ĩ »ª.»©Ĵ Ē².ª»®.-Ÿ Ø.Ÿ- Ĩ°»½°½ ĐĴ²
Ÿ-Ÿ±° Ĩ² Ɔ»®Ĵ²±± ŸĴ:°±®².Ĵ

Đ°±Ÿ½- Œ±± éððĴ óðĴ
Ū»½»³ ¼»® Ĵó Ĵððé

Ĵ ĒÓÓĴĴ Ç ŃŪ ŐĴƆŃĴ ĴĴ ŃĴ Ç Ĵ ŪĴ Ĵ ×ÒŪ ĐĴ ŃŪĴ ƆÓ

Ĵ » °±Ÿ±©.21 -- Ĵ -«³ ³ Ĵ®Ÿ ±° Ĵ » Ĵ¼±®ĴĴ±®Ÿ Ĵ-Ĵ- ½±²¼«½-»¼ ¼Ÿ ŸØØ ×²½±®° ±®ĴĴ»¼» Ĵ » -»-
®»-«Ĵ- Ĵ®» °®»-»²»¼ ±² Ĵ » ¼±®²1 Ĵ±- .2 Ɔ°°»²¼.Ÿ Ɔ Ĵ²¼ 1®Ĵ » .½Ĵ'®»°®»-»²-ĴĴ² --
.2½«¼»¼ .2 Ɔ°°»²¼.Ÿ Ÿ±° Ĵ.- ®»°±®Ÿ

- Ū»¼ Ő±-»®»
- Ū»¼ Ū®Ÿ Ū»²--Ÿ
- Ń°-³ «³ Ő±-»®» Ÿ±²-»²-
- ŐĴ.³ «³ Ū®Ÿ Ū»²--Ÿ
- Ū®»½- Ĵ » Ĵ®
- Ÿ±²-±:¼ĴĴ²
- Ĵ.»ª» Ɔ²ĴŸ---

Ĵ » °±Ÿ±©.21 -- Ĵ -«³ ³ Ĵ®Ÿ ±° Ĵ » Ĵ¼±®ĴĴ±®Ÿ Ĵ-Ĵ- ½±²¼«½-»¼ ¼Ÿ Ū»±ŐĴĴ Ĵ-»²1
Ĵ¼±®ĴĴ±®»-Ÿ ×²½Ÿ Ĵ » -»-®»-«Ĵ- Ĵ®» .2½«¼»¼ .2 Ɔ°°»²¼.Ÿ Ÿ±° Ĵ.- ®»°±®Ÿ

- Ū»¼ Ő±-»®»
- Ń°-³ «³ Ő±-»®»
- ŐĴ.³ «³ Ū®Ÿ Ū»²--Ÿ
- Ū®»½- Ĵ » Ĵ®
- Ĵ.»ª» Ɔ²ĴŸ---

Ĵ » °±Ÿ±©.21 -- Ĵ -«³ ³ Ĵ®Ÿ ±° Ĵ » Ĵ¼±®ĴĴ±®Ÿ Ĵ-Ĵ- ½±²¼«½-»¼ ¼Ÿ ŐŸŸ Ĵ ½.ºº Ɔ--±½-Ĵ-»-Ÿ Ĵ »
-»-®»-«Ĵ- Ĵ®» .2½«¼»¼ .2 Ɔ°°»²¼.Ÿ Ÿ±° Ĵ.- ®»°±®Ÿ

- ½ »³ .½Ĵ Ĵ½±®±-ª.-Ÿ -»²1

Y±2½»°-«-Đ'ž² Ā »ª.»©0 È2.ª»®.-š Ø.'- í °»½º.½ Đ'ž²
Ÿ.-š ±° Ā ž² Þ»®žª¼.2±0 Ÿž:º±®ž.

Ð±½»½-Ò±0 éððí óðí
Ū»½»³ ¾»® í 0 í ððé

Ÿ±2¼.±±2 ĩ .- ž²ž'š-- º±®ž » ½.1 »-ž º±º±-»¼ °.º0±ª»®0½«-ž'±º» -ž±©2 ±2 ž » º±ª.¼»¼
½±2½»°-«ž' 1®ž.¼.21 °'ž²-0 Ā » ½«-º±®±±2 ±ºž » -ž'±º» ®»-«.»- -±³ » ±ª»®»'½žªž±±2 ± ¾
½±2ª»®¼.2±½±3 °ž½»¼ °.º0 Ā » ±ª»®»'½žªž±±2 -ž±«¼ »'»²¼ º±³ º±º±-»¼ -ž'±º» °ž½» ž
ž » ±ž ž ¼.-ž²½» ±º ž »ž-ž'íè °»»ž.2±ž » .-¼» ž²¼ž » ±ª»®»'½žªž±±2 ¼»ºž -ž±«¼
1®ž¼«ž'š.2½»ž-»-ž±ž 3 ž'ž 3 «3 ¼.-ž²½» »-«ž'±žž » ½.1ž±ºž » ½«-º±®±±2 ±ºž » -ž'±º» ž-
ž » ±ª»®»'½žªž±±2 žº±ž½ž»-ž » ½»-ž±ºž » ½«-ž-»» 1®žº.½ž'®»-»²ž±±2 .2 Ū.1«® í ð
Ā šº.½ž'šž » -ž'±º» ±ª»®»'½žªž±±2 ½ž²¾ž ž½ž.ª»ª»¼¾š¾ž²½ž.21.2±ž » -ž'±º» ž±ž±ž±ž
¼.-ž²½» »-«ž'±žž »-«º.³ »²ž.¼ž ž²¼ª»º»ª»ª»½ž¾ž²½ž 0 Ā ±º»-±ª»®éðº»»ž.2ž.1ž
©.ž.2ž » º±º±-»¼ °ž²².21 ž»ž-ž±«¼¾ž¾ž¾ž.²ž-ž²²»® Ā ±º»-žº±²¼ ž²¼ ±«-ž.¼ž ž »
ºž²².21 ž»ž-žº±¼-½«-»¼.2 βºº»²¼. Ū0

Ū«-žž » ½.1 -»-3.½½ž»º.½ž»²0ž » -»-3.½½ž±2¼.±±2 ½±²-º±'ž » -ž'±º» -ž¾.š±ºž-
-»»0 Ā » ®»-«-ž±º-ž'±º» -ž¾.š-žš ž²ž'š-»-žº.2½'«¼»¼.2 βºº»²¼. Ū0

Þ»½ž«-»ž » -ž'±º» -ž¾.š-š¾ž»²¼- .12.º.½ž²ž'š ±²ž » ½±ž »-ª »-ž»²1ž±ºº.º.ºž»ž-0
ž » -ž¾.š-š±ºžº.ºž²¼º.º±ª»®½«-ž'±º»- -ž±«¼¾žº«®»»ªž«-ž¼¼¼«²1 1®ž¼.21¾š
ª»®.š.21ž »-®»²1žºž»ž-º±ºžº.ººž»ž-©.ž ž¼¼.±±2ž'¼.»½ž-ž »ž-ž-²1
º»®±³ »¼¾šž » 1»±»½ž.2.½ž' »²1.2»®±² ž»1«ž¾ž-¼«²1 ½±²-ž»½ž±²0 Ÿ±³ºž½»¼
º.º.ºž»ž»ž.².21ž »-«-ž-»-ž»²1žºž»ž-º±«¼ »-ž²¼ ±ž±ž±ž'šº±³ž » -ž'±º»
ºž½ž» ±ž¼.-ž²½» »-«ž'±žž » º±º±-»¼ -ž'±º» ½.1ž±ºž'íèº»»-0 ©.½ž»ª»-1®ž»ž»

Ŷ±2½»°-«Ĵ'Đ'Ĵ² Ā »^a.»©Ŧ Ē2.^a»[®]..-š Ø.'- Ā »½°½ Đ'Ĵ²
 Ŷ.-š ±° Ā Ĵ² Đ»^{®2}Ĵ^{®2}±0 ŶĴ:°±^{®2}.Ĵ

Đ^{®±ŧ}»Ĵ- Ō±0 éđđí óđí
 Ū»½»³ ¼»[®] í ō í đđé

Ŧ^a»[®]..!»¼ ŌĴ-»[®].Ĵ

«Ĵ- Ĵ²-½°-Ĵ-»¼ Ĵ-Ĵ Ĵ' Ĵ± Ē° »[®]½»²-Ĵ±0 ±^a»[®]..!»¼ ³ Ĵ-»[®].Ĵ' 0¼±«¼»[®]- 1[®]»Ĵ-»[®]Ĵ-Ĵ Ĵ² Ĵ' Ā .2½»-±-
 »[®]-«[®].21 -°»½-Ĵ' Ĵ²¼'.21 0±[®]¼-°-±-Ĵ- 3 Ĵš ¼» »2½±«²-»»¼ ¼«[®].21 1[®]¼.210 Ē .» --»0-°»½°½
 »½±³ 3 »2¼ĴĴ±²- 3 Ĵš ¼» ¼»^a±°»¼ ¼«[®].21 1[®]¼.21 °'Ĵ² °»[®]»Ĵ-Ĵ±² ±[®].2-Ĵ-»[®].¼ ¼«[®].21
 ½±²-»«Ĵ-±20 ©»Ĵ' »^{®±a}.¼.21 1»2»[®].Ĵ' 3 »Ĵ-±¼-°±[®]¼-°±-.21 ±0 ±^a»[®]..!»¼ ^{®±}½µ ±² -»[®] ±[®]
 °»[®].:3 .2.Ĵš ½±²-¼»[®]Ĵ-±20

Ā ±½µ- 1[®]»Ĵ-»[®]Ĵ-Ĵ Ĵ² Ĵ' ō .2½»- ±-2 -!» -»±«¼ 2±-¼» °'½»¼ ©.Ĵ-2 Ĵ' đ°»»[®]±0 .2-» 1[®]¼»[®]0 «Ĵ
 -»±«¼ ¼» ½Ĵ«Ĵ-±2»¼ Ĵ-Ĵ Ĵ'Ĵ'»^{®1} »^{®±}½µ ¼» ±[®] Ĵ' ¼» °'Ĵ± Ĵ' đ°»»[®]Ĵ- 3 Ĵš °»[®]-»²-¼.00.½«Ĵ-»- .2
 .2-Ĵ-»[®].21 --»«Ĵ-»[®]±-±«Ĵ-»- ¼» ±[®] Ĵ-Ĵ Ĵ' Ĵ' 0 Ŧ^a»[®]..!»¼ ³ Ĵ-»[®].Ĵ' -»±«¼ 2±-¼» p²»-»¼p0
 ŌĴ'»^{®1} »^{®±}½µ- -»±«¼ ¼» -°»[®]¼±«Ĵ' ©.Ĵ² °'½»¼ ©.Ĵ-2 Ĵ-»[®].Ĵ' 0.Ĵ' .2 Ĵ² Ĵ²»[®]Ĵ-Ĵ Ĵ' ©.Ĵ' Ĵ' ±[®] ©
 ½±³ °'ĴĴ±² ±0 -±.°'.Ĵ' Ĵ'«²¼ Ĵ-» .2¼.a.¼«Ĵ' ±^a»[®]..!»¼ ^{®±}½µ-0 Ā »Ĵ-½»¼ ¼ Ū»²»[®].Ĵ' ŪĴ[®].Ĵ' ±[®]µ
 Ĵ²¼ Ū[®]¼.21 Ā »½°½ĴĴ±²- ½±²-Ĵ.2- Ĵ¼¼-Ĵ±²Ĵ' 1«¼»[®].2»-0

Ā'±°» Ŷ±²-»«Ĵ-±2»

Ū.Ĵ' -'±°»- Ĵ'»[®] ¼»- .12»¼ Ĵ-Ĵ Ĵ² .2½'2ĴĴ±² ±0 ĀŦĴ ĒŦ Ū.Ĵ' -'±°»- -»±«¼ ¼» ±^a»[®]..!»¼ ¼«[®].21
 ½±²-»«Ĵ-±2 Ĵ²¼ Ĵ-»² ½«-¼¼Ĵµ Ĵ± »'±-»° «Ĵš ½±³ °'Ĵ-»¼ -±.0 Ē .»»[®] °'.Ĵ' »[®]± ¼» °'Ĵ²¼
 Ĵ' Ĵ².2-»[®].21 -'±°»- -»»°»[®]»Ĵ-Ĵ² ĒŦĴ ĒŦ Ĵ-»[®]..!»¼ ³ Ĵ-»[®].Ĵ' -»±«¼ 2±-¼» ¼»²½»¼ ¼.2-±
 ½±³ °»»² 2ĴĴ^a 3 Ĵ-»[®].Ĵ' -Ĵ ±^{®±a}.¼» Ĵ-»»[®]±-±^a» ¼»²½»- -Ĵ-»Ĵ-»[®] Ĵ' Ĵ² Ĵ± »[®]³ ±^a
 Ĵ-» ½±³ °»»-^a Ĵ' 2¼°»^{®3} »Ĵ'Ĵ' Ĵ-°-±.0 Ā .» ¼»²½»- -»±«¼ ¼» Ĵ' 3.2.3 «3 ±0 Ĵ'Ē°»»[®].2
 ©.¼Ĵ' 0 ½±²-»«Ĵ-»¼ Ĵ' Ĵ' °»[®]±.Ĵ' Ĵ-»š Ĵ' 0 ±±-^a»[®].½Ĵ' .2-»»[®]Ĵ-0 x2 Ĵ¼¼-Ĵ±²0 Ĵ-»[®]µš -»±«¼
 ¼» ½±²-»«Ĵ-»¼ Ĵ' ½[®]±--Ĵ-» ±±[®] Ĵ-» -±°»0 Ā .» -»[®]µš -»±«¼ ¼» Ĵ' 3.2.3 «3 ±0 Ĵ'Ē°»»[®]©.¼»[®]
 -'±°»¼ .2©Ĵ'¼ Ĵ-Ĵ'Ĵ' ±0 Ĵ'Ĵ'Ĵ-Ĵ'Ā °»[®]²-0 Ĵ²¼ -»±«¼ °'2»[®]Ĵ-Ĵ Ĵ' 3.2.3 «3 ±0 Ĵ'Ē°»»[®]¼»²»Ĵ-
 Ĵ-» ±±[®] Ĵ-» -'±°».2-±^{®3} ½±³ °»»²-Ĵ-±.0

Ŷ«- '±°»- Ĵ'»[®] »'»½-»¼ Ĵ± ¼» 1[®]±--š -Ĵ-¼' Ĵ' Ĵ' 3 Ĵ' .3 «3 .2½'2ĴĴ±² ±0 ĀŦĴ ĒŦ
 Ō»^a»[®].»[®]»-0 Ĵ' ½«- '±°»- ©.Ĵ' ¼» «¼»¼ĴĴ-±-»[®].½-Ĵ'»[®].21 Ĵ²¼ -»±«¼ ¼» »^aĴ'«Ĵ-»¼ ±² Ĵ'
 ½Ĵ-»0¼š0Ĵ-» ¼»Ĵ-- ¼«[®].21 1[®]¼.21 ¼š Ĵ-» °»^{®±ŧ}½-»²1.2»»[®].21 1»±±1.-Ĵ Ŷ«- '±°»- .1.Ĵ'»[®]
 Ĵ-Ĵ² Ĵ' đ°»»[®]Ĵ- -»±«¼ ¼» »^aĴ'«Ĵ-»¼ ¼«[®].21 -»[®] 1[®]¼.21 ¼š Ĵ-» °»^{®±ŧ}½-»²1.2»»[®].21 1»±±1.-Ĵ

Ū.Ĵ' Ĵ²¼ °' ±^a»[®] ½«- '±°»- -»±«¼ ¼» ½±²-»«Ĵ-»¼ 2± -»»°»»[®]Ĵ-Ĵ Ĵ² Ĵ' ōŦĴ ĒŦ Ū[®].Ĵ' ±^a»[®] ½«- '±°»-0
 °'Ĵ' 3 Ĵ-»[®].Ĵ' -»±«¼ ¼» -»»²¼ ±[®].Ĵ'±²-Ĵ'š °»[®]±³ Ĵ-» -'±°»°'½» ±± Ĵ'-Ĵ-Ĵ²½» »-Ĵ'Ĵ' ±± Ĵ-»
 °»[®]±±-¼ -'±°»[®].1.Ĵ' ±[®]Ĵ'Ē°»»[®]Ĵ' ©.½.Ĵ'»^a»[®].. 1[®]»Ĵ-»[®] Ū.Ĵ' -»±«¼ ¼» µš»¼.2-± ½±³ °»»²-
 1[®]±«²¼0 ¼»²½»¼¼0 Ĵ' 2¼ ½±³ °'Ĵ-»¼ Ĵ-¼-½'¼»¼ Ĵ'¼±^a0

Ĵ''- '±°»- 0.''- -»±«¼ ¼» ½±³ °'Ĵ-»¼ Ĵ± Ĵ'Ĵ'Ĵ-Ĵ Ĵ-Ĵ'Ĵ' çđ °»[®]½»²-0çĒ °»[®]½»²-0±[®]- '±°»- ±^a»[®]Ĵ' đ°»»[®].2
 .» 1.Ĵ' ±± Ĵ-» 3 Ĵ' .3 «3 ¼š¼»¼²--šĀ ±± Ĵ-» ±«Ĵ-»[®]- '±°»°'½»0 «Ĵ»[®]½±³ 3 »2¼»¼ Ĵ-Ĵ Ĵ' -'±°»- ¼»
 °'Ĵ-»¼ -«¼-»[®]«²-Ĵ-± ½±²-»«Ĵ-±20 Ĵ-Ĵ 3.2.3 «3 ō Ā'±°» ŌĴ.2-»²Ĵ²½» Ū«¼»[®].2»- ±[®]
 Ō±3 ±±²2»[®] °»»-»²»¼.2-Ĵ-»[®] ±[®] ±[®] ±[®] ±[®] ¼» ±^{®±}±[®]¼ ±[®]Ĵ-»[®] - °»[®]±-»0

Ū[®]¼»¼¼ °' Ĵ²¼ ½«- '±°»»0 .2 ±«[®]±° .2±20 -»±«¼ ¼» °»^{®±a}.¼»¼ ©.Ĵ- Ĵ-Ĵ'»¼ ¼» ±[®]»^a»² 2«-Ĵ²½»
water from daylighting on the slope face or at the toe. Generally, a "burrito style" drain consisting
 ±0°»[®]»[®]Ĵ-»¼ °'Ĵ-½'°° »2½Ĵ-»¼ .2°»[®]»¼»[®].2.21 Ĵ' 1[®]»Ĵ' Ĵ-» Ĵ²¼ -«[®]±«²¼»¼ ¼š Ĵ' °»^{®±}°»[®]Ĵ-»
 1»±»[®]Ĵ-»[®].0.'»[®]¼¼»¼ ©±«¼ ¼» -«[®].½-»²-0±[®]Ĵ-» - ½±²¼-Ĵ±²0 Ā š°-½Ĵ' ±±»¼[®].2 ¼»Ĵ-»[®]..-Ĵ-Ĵ'½»¼¼0
 Ā °'½°½ ¼»- .12 ¼»Ĵ-»[®] ±[®]-«¼¼»[®].2- »±«¼ ¼» ¼»^a±°»¼ ¼«[®].21 1[®]¼.21 °'Ĵ²- »^a.»© Ĵ²¼ Ĵ-»
 Ĵ-»«Ĵ'²»»¼- ½±²¼-Ĵ±²- »2½±«²-»»¼ ¼«[®].21 1[®]¼.210 Ĵ²š °'±»²-Ĵ'š «²-Ĵ-¼» ¼±«¼»[®]- »'°±-»¼
 .2 Ĵ-» -'±°» °'Ĵ'»- -»±«¼ ¼» »^{®3} ±^a»¼ ¼«[®].21 ½±²-»«Ĵ-±20

Y±2½»°«ζ' Đ'ζ² Ā »a.»©0 Ē2.a»°.-š Ø'-' í °½°½ Đ'ζ²
Y.-š ±° í ζ² Þ»²ζ¼.2±0 Yζ:°±².ζ

Đ±½»½- Ò±0 éððí óðí
Ú»½»³ ¾»í0 í ððé

B'' «-:»š »²½»- ζ²¼ ©ζ'' ¾ζ¼μ°'' - , ±«¼ ¾¼» ³ »½ζζ².½ζζ'š ½±³ °ζ½»¼ ±ζζ, » 3.2.3 «³
»-«.»³ »²- ±° ζζ' »ζ-ζ ÇÐ °»²½»²»»ζζ'ζ²»a» ½±³ °ζ½»±²0 Ò±½»²10 ±²¼.210 ±°±½¼.21 - , ±«¼ ¾¼»
°»³. -»¼ ©.ζ.2 ζζ, ¾«.¼.21 ζ»ζζ ±°©, »»²½»»- ζ»². ±² ±²» ±° .2°«»²½» ±° ±±±±²1 ±ζ¼-0
Û''½ζ²aζζ¼ ³ ζζ»»ζζ' °±³ ±²±²1 »²½»»- - , ±«¼ ²±¾¼» °ζ½»¼ .2 - ζ¾0±²01°ζ¼» ζ»ζζ- «²'»--
°±°»»š ½±³ °ζ½»¼ ζ²¼ »-»¼

Í ÒΒΠÍ óÑÒóÛÍ ΒÛÛæ

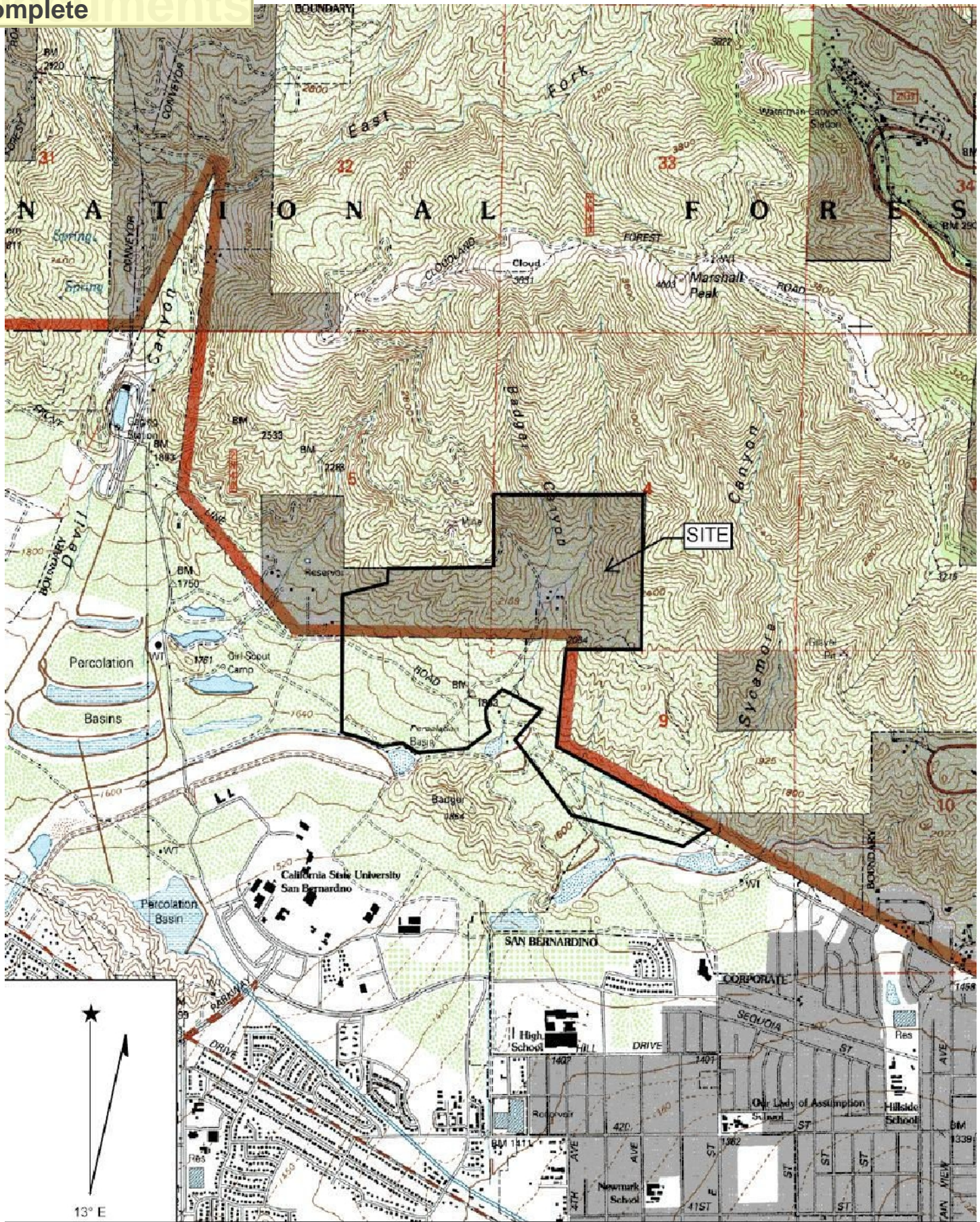
Í ζ¾-0±²01°ζ¼» - , ±«¼ ¾¼» -«° ±°»¼ ±² ½±³ °ζ½»¼ 0.ºº ¾¼» ζζ'ζζ-ζζ-ζζ-ζζ.2½»»- ζζ.¼μ0 ζ²¼ - , ±«¼ ¾¼»
»².±²±²½»¼ ©.ζζ ζζ' »ζζ-ζζ Ò± í ¾ζ°- ζζ' í í0.2½»»- ±²0½»²»»¾¼±ζζ, ©ζζ-0 °±°»»š ½±²»»¾¼ .2 3.¼
ζζ.¼μ²»-- ±° -ζ¾-0 Ñζζ»»°»½±³ 3 »²¼ζζ±²- ζ»»°»»»²»»¼ ±² Đ'ζζ' Ĩ0 Û''½»»-- -±.'- 1»²»»ζζ»¼
°±³ ±²«²¼ζζ±²»''½ζ²aζζ±²- - , ±«¼ ²±¾¼» °ζ½»¼ ±² ¾«.¼.21 °ζ¼- ©.ζζ ±«° ±°±°»»³ ±ζ-ζ»»» ζ²¼
½±³ °ζ½»±²0 ò Í ζ¾-0±²01°ζ¼» - , ±«¼ ¾¼» °±²a.¼»¼ ©.ζζ ζζ' í ð0³. Ē-«»»² 3 ±ζ-ζ»»» ¾ζζ»»
°±°»»š °±°»»»½»»¼ ©.ζζ ζζ' »ζζ-ζζ ©±.2½» ±° ½'ζζ² -ζ²¼ ζ¾¼±²a» ζζ, Ē-«»»² ζ²¼ ζζ±.2½»»- ±°
½±³ °ζ½»¼ ½'ζζ² -ζ²¼ ¾¼»±©ζζ, Ē-«»»²0 Í ζ¾-«¾¼¹°ζ¼» - , ±«¼ ¾¼» a»°.»¼ ±½±²ζζ.2 í ðí -³ »-
ζζ- -±.' ±°-³ «³ 3 ±ζ-ζ»»» ½±²»»²ζζ ±ζ ζ¼»°ζζ ±° í Ĩ.2½»»- °±° ±° °ζ½»³ »²ζ ±° -ζ¾ ¾«.¼.21
3 ζζ»»ζζ-0 Ò±-ζ»»» ½±²»»²ζζ - , ±«¼ ¾¼» »-»»¼ .2 ζζ, »°.»¼ ¾¼š ζζ, -±' »²1.2»»» Í ζ¾- «¾¼¹°ζ¼»
- , ±«¼ ¾¼» μ»°³ ±ζ-ζ²¼ ζζ, -«»ζζ- - , ±«¼ ²±¾¼» ζζ'±©»¼ ±ζ ¼»-½½ζζ»0 Í ζζ' ζ¼¼ζζ±² ±° ¾¼»
3 »- .2 ζζ, ½±²½»»» ζ²¼ ½ζ»°«' ½±².°± ±° ©ζζ»»»»³ »²ζζζζ- 3 š »--»² ζζ, °±»²ζζ' ±° -ζ¾
½ζζ'¼μ.210 x² ±ζ±° ©.2¼š ©»ζζ, » ½±².°± ½±² 3 «-ζζμ ζζ°°±°±» ½«»²1 °»»½ζζ»±²- ζζ»
ζζ, °ζ½»³ »²ζ ±° ½±²½»»»»0 Í ζζ' «-» ±° 3 »½ζζ².½ζζ'š ½±³ °ζ½»¼¼¼»²-» ±© -'«³ ° ½±²½»»» 0²±
»'½»¼.21 í .2½»»- ζζζ, »³ » ±° °ζ½»³ »²ζζ- °»½±³ 3 »²¼¼¼0 Y±²½»»» °±²¼ζζ±² ζ²¼ -ζ¾-
3 «-ζ¾» °ζ½»¼ ³ ±²±².½ζζ'š0 Ē »»½±³ 3 »²¼ ζζζζ -ζζ»»»» ±° ±²¼ζζ±² ζ²¼ «-ζ¾»¼ .
1°±«»¼ ζζ- ±° ±ζ»»» ½ζζ'¼μ -»²-»a» °±².21 0-«½ζζ ζζ-ζζ-ζζ-ζζ.2²¼¼¼.°»½ζζ±² ½±²½»»»-
-ζ¾-0

ÛÈÐΒÒÍ ×ÈÛ Í Ñ×ÓÍ æ

Í .2½»» ζζ' 3 ζζ»»ζζ' - »²½±²»»»¼ ¼«»²1 ζζ, »°±½»½ζζ' 1»±»½ζζ.2.½ζζ'.2a»-»1 ζζ±² ©»» 1°ζ² «ζ'
ζ²¼ ½±²-¼»»¼ ±ζ¾ ²±²0½»»»½ζζ'š »°ζ²-»a»0 -°½ζζ'¼ ½±²-»»½±² °±½»¼«»»- ±ζ
-°»½°½ζζ'š »»-»»»°ζ²-»a» -±.' ±°½ζζ- ζ»² ±ζζ²ζζ'ζζ'¼ ζζζζ-ζζ³ »0 Β¼¼.ζζ±²ζζ'
»aζζ'ζζ±² ±° -±.' ±° ±°»»°ζ²-»a» ±ζζ²ζζ'ζζ' - , ±«¼ ¾¼» ½±²¼«½»¼ ¾¼š ζζ, » 1»±»½ζζ.2.½ζζ' »²1.2»»»
¼«»²1 ζζ, » 1°ζ¼.21 ±°»»ζζ±²0


ĐÑÌ ÛÒÌ ×ΒÔ ÛÍ ÑÍ ×ÑÒæ



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Name: SAN BERNARDINO NORTH
 Date: 11/1/2007
 Scale: 1 inch equals 2000 feet





Location: 034.1954274° N 117.3127234° W
 Caption: SITE LOCATION MAP
 Figure 1




















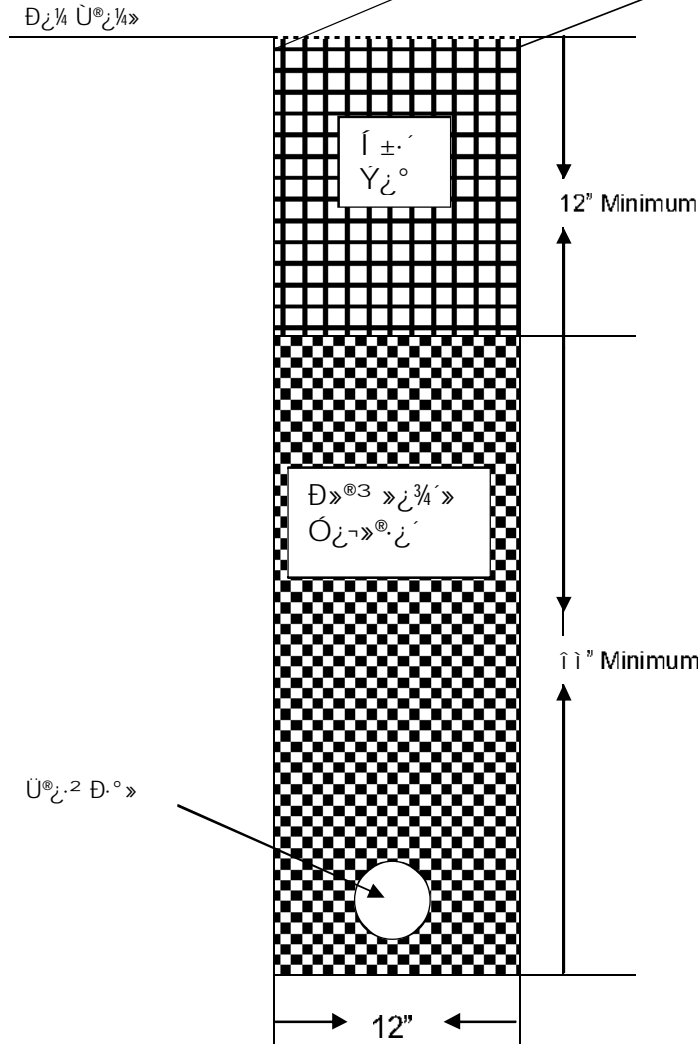






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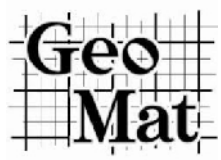


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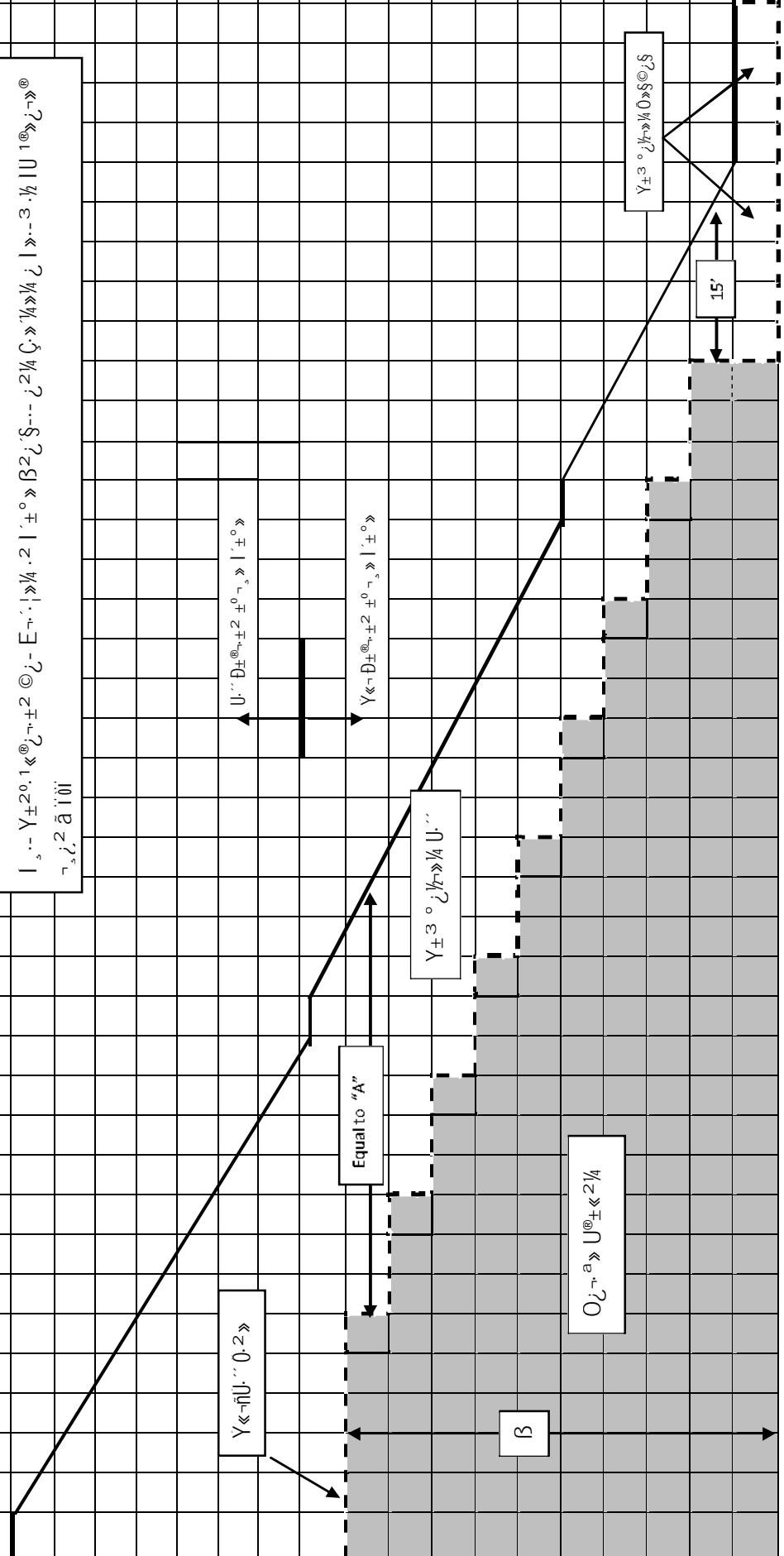
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C.H.J. Incorporated
**GEOLOGIC MAP AND SITE PLAN
ENCLOSURE: "A-4"
PROJECT: PARADISE HILLS
SAN BERNARDINO COUNTY, CALIFORNIA**
PREPARED FOR
INLAND COMMUNITIES CORPORATION
JOB NO.: C5894-S
DATE: JANUARY 27, 2008

GEOLOGIC UNITS

1. Alluvium (Qa) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

2. Alluvium (Qc) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

3. Alluvium (Qd) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

4. Alluvium (Qe) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

5. Alluvium (Qf) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

6. Alluvium (Qg) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

7. Alluvium (Qh) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

8. Alluvium (Qi) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

9. Alluvium (Qj) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

10. Alluvium (Qk) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

11. Alluvium (Ql) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

12. Alluvium (Qm) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

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14. Alluvium (Qo) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

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16. Alluvium (Qq) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

17. Alluvium (Qr) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

18. Alluvium (Qs) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

19. Alluvium (Qt) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

20. Alluvium (Qu) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

21. Alluvium (Qv) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

22. Alluvium (Qw) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

23. Alluvium (Qx) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

24. Alluvium (Qy) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

25. Alluvium (Qz) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

LEGEND

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Alluvium (Qs) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

Alluvium (Qt) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

Alluvium (Qu) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

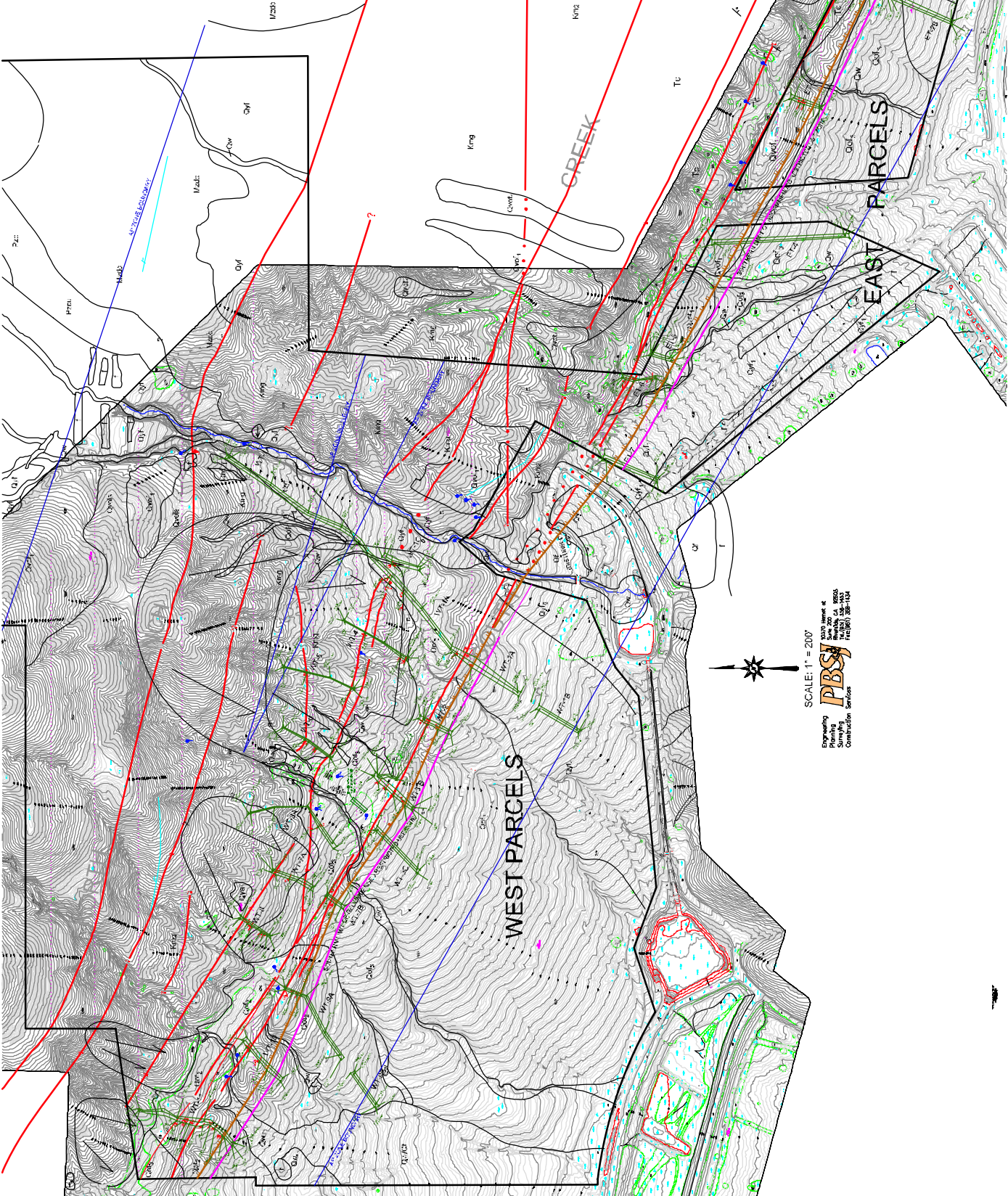
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Alluvium (Qz) - recent alluvium, including recent alluvial fans, terraces, and floodplains.

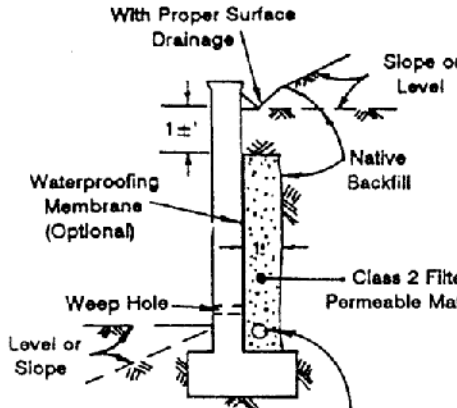


SCALE: 1" = 200'

Engineering
Planning
Construction Services
PBSJ
3000 Sierra at
Sierra
Beverly Hills, CA 90210
Tel: (310) 223-1104
Fax: (310) 223-1104

SUBDRAIN OPTIONS FOR NATIVE MATERIAL BACKFILL

OPTION N2: Pipe Surrounded with Class 2 Material

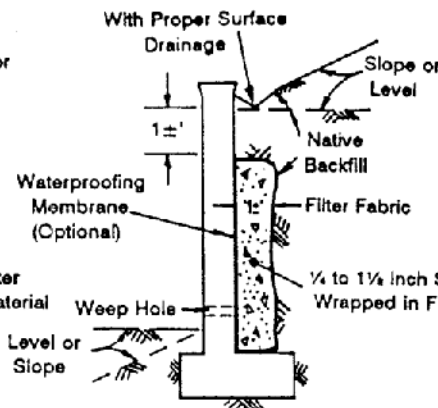


4-Inch Diameter Perforated Pipe

Class 2 Filter Permeable Material Grading Per Caltrans Specifications

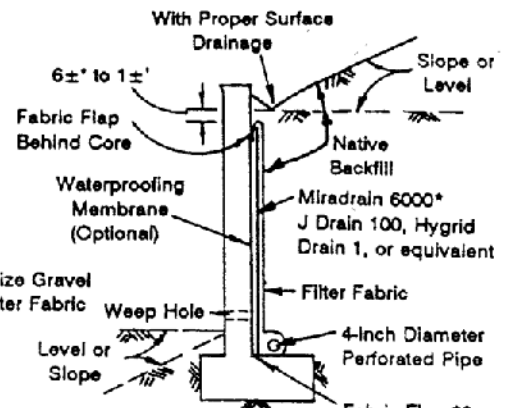
Sieve Size	Percent Passing
1"	100
3/4"	90-100
3/8"	40-100
No. 4	25-40
No. 8	18-33
No. 30	5-15
No. 50	0-7
No. 200	0-3

OPTION N1: Gravel Wrapped in Filter Fabric



Proper Outlet should be Provided for Gravel Subdrain (See Notes)

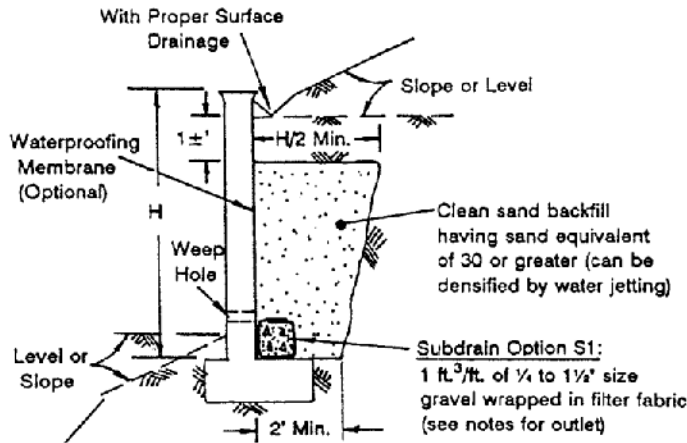
OPTION N3: Geotextile Drain



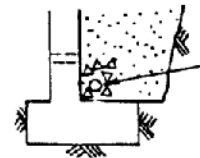
*Miradrain 6000 or J Drain 100 for non-waterproofed walls; Miradrain 6200 or J Drain 200 for completed waterproofed walls

**Peel back the bottom fabric flap, place pipe next to core, wrap fabric around pipe and tuck behind core.

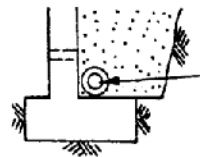
SUBDRAIN OPTIONS FOR CLEAN SAND BACKFILL



Subdrain Option S1:
1 ft.³/ft. of 1/4 to 1 1/2" size gravel wrapped in filter fabric (see notes for outlet)



Subdrain Option S2:
4" diameter perforated pipe surrounded with 1 ft.³/ft. of Class 2 filter material per Caltrans specifications as above



Subdrain Option S3:
4" diameter perforated pipe wrapped in filter fabric

Notes:

- Pipe type should be ASTM D1527 Acrylonitrile Butadiene Styrene (ABS) SDR35 or ASTM D1785 Polyvinyl Chloride plastic (PVC), Schedule 40, Armco A2000 PVC, or approved equivalent. Pipe should be installed with perforations down.
- Filter fabric should be Mirafi 140N, 140NS, Supac 4NP, Amoco 4545, Trevira 1114, or approved equivalent.
- All drains should have a gradient of 1 percent minimum.
- Outlet portion for gravel subdrain should have a 4"-diameter pipe with the perforated portion inserted into the gravel approximately 2' minimum and the nonperforated portion extending approximately 1' outside the gravel. Proper sealing should be provided at the pipe insertion enabling water to run from the gravel portion into rather than outside the pipe.
- Waterproofing membrane may be required for a specific retaining wall such as a stucco or basement wall.
- Weepholes should be 2" minimum diameter and provided at 25' minimum in length of wall. If exposure is permitted, weepholes should be located at 3±' above finished grade. If exposure is not permitted such as for a wall adjacent to a sidewalk/curb, a pipe under the sidewalk to discharge through the curb face or equivalent should be provided, or for a basement-type wall, a proper subdrain outlet system should be provided. Open vertical masonry joints (i.e., omit mortar from joints of first course above finished grade) at 32" maximum intervals may be substituted for weepholes. Screening such as with a filter fabric should be provided for weepholes/open joints to prevent earth materials from entering the holes/joints.

RETAINING WALL BACKFILL AND SUBDRAIN DETAIL



$\beta^{\circ} \circ \gg 2\frac{1}{4} \cdot \cdot \beta$

**Geo
Mat**



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US Army Corp of Engineers, Engineering and Design, "Slope Stability", EM 1110 òí çðí ò Ñ½±¾»®
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**US Army Corp of Engineers, Engineer Manual, Engineering and Design, "Stability of Earth and
Rock Fill Dam", EM 1110** òí çðí ò Ò®' Ì ò Ì çéðò

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Engineering "An Engineering Manual for Slope Stability Studies" by J. M. Duncan, A.L.
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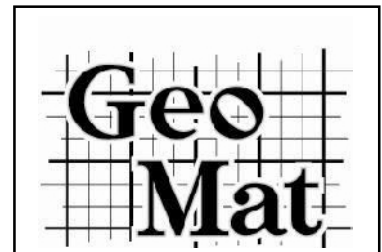
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**Department of Civil Engineering, Katholieke universiteit Leuven, Belgium, "Determination of the
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Methods." J. Bojorque, G. de Roek.**

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KEY TO LOGS

LEGEND OF LAB/FIELD TESTS:

- AL Atterberg Limits (ASTM D 438)
- Bulk Indicates Disturbed or Bulk Sample
- Consol. Consolidation Test (ASTM D 2435)
- Cor. Chemical/Corrosivity Tests (ASTM G 57, ASTM C 51, ASTM C 114)
- Dist. Indicates Disturbed Sample
- DS Direct Shear Test (ASTM D 3080)
- Exp. Expansion Test (California Building Code Standard Test Method 18-2)
- MDC Maximum Density Optimum Moisture Determination (ASTM D 1557)
- N.R. Indicates No Recovery of Sample
- Ring Indicates Undisturbed Ring Sample. Undisturbed Ring Samples are obtained with a "California Sampler" (3.25" O.D. and 2.42" I.D.) driven with a 140-pound weight falling 30 inches. The blows per foot are converted to equivalent SPT values.
- SA Sieve Analysis (ASTM C 136)
- SPT Indicates Standard Penetration Test. The SPT N-value is the number of blows required to drive an SPT sampler 12 inches using a 140-pound weight falling 30 inches. The SPT sampler is 2" O.D. and 1 3/8" I.D.

ENGINEERING PROPERTIES FROM SPT BLOWS

Relationship of Penetration Resistance to Relative Density for Cohesionless Soils*
(After Mitchell and Katti, 1981)

<u>Number of SPT Blows (N_{60})</u>	<u>Descriptive Relative Density</u>	<u>Approximate Relative Density (%)</u>
<4	Very Loose	0-15
4-10	Loose	15-35
10-30	Medium Dense	35-65
30-50	Dense	65-85
>50	Very Dense	85-100

* At an effective overburden pressure of 1 ton per square foot (100 kPa)

SOIL CLASSIFICATION CHART

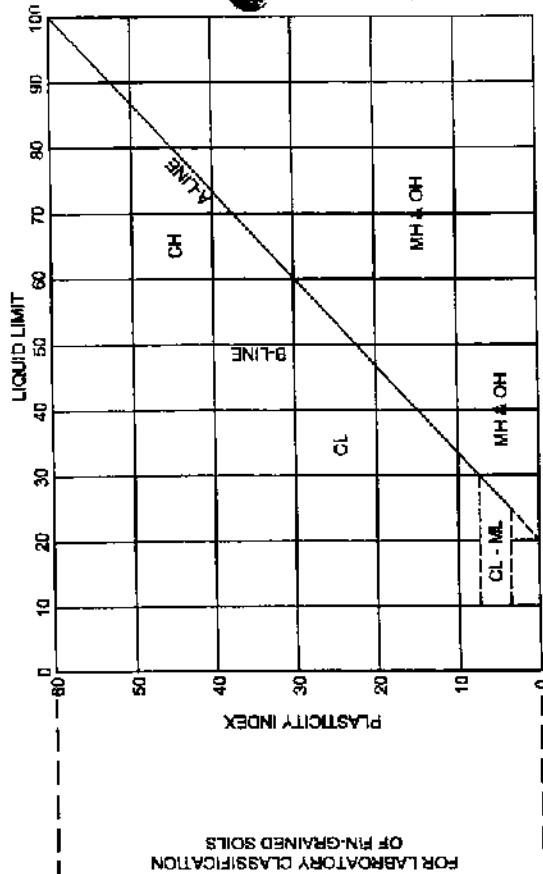
MAJOR DIVISIONS	GRAPH SYMBOL	LETTER SYMBOL	TYPICAL DESCRIPTIONS
GRAVEL AND GRAVELLY SOILS		GW	WELL-GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES
		GP	POORLY-GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES
MORE THAN 50% OF COARSE FRACTION RETAINED ON NO. 4 SIEVE		GM	SILTY GRAVELS, GRAVEL-SAND-SILT MIXTURES
		GC	CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES
SAND AND SANDY SOILS		SW	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES
		SP	POORLY-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES
MORE THAN 50% OF COARSE FRACTION PASSING NO. 4 SIEVE		SM	SILTY SANDS, SAND-SILT MIXTURES
		SC	CLAYEY SANDS, SAND-CLAY MIXTURES
FINE GRAINED SOILS		ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY
		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
		OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
MORE THAN 50% OF MATERIAL IS SMALLER THAN NO. 200 SIEVE SIZE		MH	INORGANIC SILTY, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS
		CH	INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS
		OH	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS
HIGHLY ORGANIC SOILS		PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS

GRADATION CHART

MATERIAL SIZE	PARTICLE SIZE			
	LOWER LIMIT		UPPER LIMIT	
	MILLIMETERS	SIEVE SIZE	MILLIMETERS	SIEVE SIZE
SAND FINE MEDIUM COARSE	0.075	#200	0.425	#40
	0.075	#40	2.0	#10
	2.0	#10	4.75	#4
GRAVEL FINE COARSE	4.75	#4	191	3/8"
	191	3/4"	76.2	3"
COBBLES BOULDERS	76.2	3"	304.8	12"
	304.8	12"	914.4	36"

* US STANDARD * CLEAR SQUARE OPENINGS

PLASTICITY CHART



UNIFIED SOIL CLASSIFICATION SYSTEM



EXPLORATORY BORING NO. 1

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
5		(SM) Silty Sand, fine to coarse with gravel to 2", brown	Native (Qw)				5.8		
				X		10	1.1	112	Ring
10		(SM) Silty Sand, fine to coarse with gravel to 2", brown	(Qof)						
				X		3	7.3	108	Ring
15		(SP-SM) Sand, fine to coarse with silt, gravel and cobbles to 5", light brown					4.2		
				X		20	4.6	114	Ring
20		(SP-SM) Sand, fine to coarse with silt, gravel and cobbles to 5", light brown							
				X		33	3.2	118	Ring
25		(SP-SM) Sand, fine to coarse with silt, gravel and cobbles to 5", light brown							
				X		30/5"	N.R.	N.R.	Ring
30		(SM) Silty Sand, fine to medium with coarse, gravel and cobbles to 5", brown					4.7		
				X		28	9.1	120	Ring
		(SP-SM) Sand, fine to coarse with silt, gravel and cobbles to 4", light brown					2.0		

BORING LOG 05894-3.CPJ C=J.GDT E/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-1a

EXPLORATORY BORING NO. 1

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
35		(SP-SM) Sand, fine to coarse with silt, gravel and cobbles to 4", light brown		X		30/5"	2.5	116	Ring
40				X		30/5"	4.0	113	Ring
45						30/1.5"	N.R.	N.R.	Ring
50		END OF BORING							
55		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
60									
65									

BORING LOG 05894-3.GPJ C:HJ:GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-1b

EXPLORATORY BORING NO. 2

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to coarse with gravel to 3/4", brown	Native (Qof)				3.7		DS, MDC, SA
5		(SM) Silty Sand, fine to medium with gravel to 2", light brown		X		32	4.5	114	Ring
10		(SP-SM) Sand, fine to coarse with silt and gravel to 1", light brown		X		11	5.4	103	Ring
15		(SM) Silty Sand, fine to coarse with gravel and cobbles to 5", light brown		X		18	3.5	110	Ring, Consol.
20				X		30 ^{24"}	5.7	119	Ring
25		END OF BORING		X		42	4.5	119	Ring
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG 05894-3.GPJ C-HJ.GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
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EXPLORATORY BORING NO. 3

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with gravel to 2", brown	Native (Qof)				2.5		
				X		23	2.4	Dist	Ring
5		(SM) Silty Sand, fine to coarse with gravel and cobbles to 4", light brown					3.1		
				X		16	2.9	108	Ring
10									
				X		25	3.8	114	Ring
15		(SM) Silty Sand, fine to medium with coarse, gravel and cobbles to 4", brown					6.4		
				X		36	6.9	117	Ring
20		(SP-SM) Sand, fine to coarse with silt, gravel and cobbles to 4", light brown					4.2		
				X		40	3.2	114	Ring
25		END OF BORING NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG: 05894-3.CPJ CHJ SPT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

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05894-3

Enclosure
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EXPLORATORY BORING NO. 4

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPI)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
5		(SM) Silty Sand, fine to coarse with gravel to 2", light brown	Native (Qof ₅)				3.4		Cor, DS, MDC, SA
						33	4.1	114	Ring
		(SM) Silty Sand, fine to medium with coarse and gravel to 2", light brown					2.6		
10						50	3.0	123	Ring
15		END OF BORING	Refusal			30/3"	4.4	Dist.	Ring
20		NO BEDROCK REFUSAL AT 14.0' ON BOULDERS NO FILL MODERATE CAVING NO FREE GROUNDWATER							
25									
30									

BORING LOG C5894-3.GPJ CHJ/GDT 5/12/05



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
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Enclosure
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EXPLORATORY BORING NO. 5

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Eqiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BLK				
		(SM) Silty Sand, fine to medium with gravel to 2", brown	Native (Qcf)				4.4		
5				X		49	2.3	102	Ring
		(SM) Silty Sand, fine to coarse with gravel to 1", light brown					3.1		
10				X		31	4.5	111	Ring
		(SM) Silty Sand, fine to coarse with gravel to 1", light brown					5.3		
15				X		30/6"	6.4	121	Ring
		(SM) Silty Sand, fine to coarse with gravel to 1", light brown					4.7		
20				X		30/5"	4.7	Dist.	Ring
		END OF BORING					N.R.	N.R.	
25						30/2"	N.R.	N.R.	Ring
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG NUMBER: 05894-3 CHJGDY 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

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Enclosure
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EXPLORATORY BORING NO. 6

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with gravel to 1", brown	Native (Q ₆)				4.8		
5				X		20	4.4	105	Ring
10				X		25	3.5	111	Ring
15				X		30/6"	4.7	Dist.	Ring
20				X		30/5"	4.9	Dist.	Ring
25				X		30/5"	10.1	Dist.	Ring
25		END OF BORING							
25		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG 05894-3.CPJ CHJ.CDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

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Enclosure B-6

EXPLORATORY BORING NO. 7

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 2", light brown	Native (Qsf)				2.3		
5				X		52	3.2	121	Ring
10				X		38	3.7	118	Ring
15				X		50	5.2	119	Ring
20						30/4"	2.7	Dist.	Ring
25						30/3"	9.3	Dist.	Ring
		END OF BORING							
		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BCH-MS LOG 05894-3.DPJ CHJ.GDT 5/1/2006



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

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Enclosure
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EXPLORATORY BORING NO. 8

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with gravel to 1", light brown	Native (Qof)				3.2		
5				X		38	2.4	119	Ring
10				X		25	3.0	118	Ring
15				X		38	6.7	116	Ring, DS
20				X		30/6"	2.8	Dist	Ring
25		END OF BORING NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG 05894-3.GPJ C:\JGD\511205



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

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Enclosure
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EXPLORATORY BORING NO. 9

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with gravel to 2", light brown	Native (QyF)				5.6		Cor.
		(SM) Silty Sand, fine to coarse with gravel and cobbles to 5", light brown	(Qof)			13	6.5	124	Ring
5		(SM) Silty Sand, fine to coarse with gravel and cobbles to 5", light brown	(Qof)			41	3.7	118	Ring
10		(SP-SM) Sand, fine to coarse with silt and gravel to 2", light brown				41	2.8	116	Ring
15						28	3.5	Dist.	Ring
20						30/5"	5.9	Dist.	Ring
25		END OF BORING NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG: 05894-3 GP., CHJ.GDT 5/2/06



C.H.J.

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BADGER CANYON AREA, CALIFORNIA

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Enclosure
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EXPLORATORY BORING NO. 10

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equip. v. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to coarse with gravel to 2", brown	Native (QyI)				4.1		DS, MDC, SA
5		(SP-SM) Sand, fine to coarse with silt and gravel to 2", light brown		X		17	4.1	116	Ring
10				X		26	2.0	119	Ring
15		(SM) Silty Sand, fine to medium with gravel and cobbles to 5", brown		X		17	4.0	116	Ring
20				X		20	9.6	111	Ring, Consol.
25		END OF BORING		X		30.5"	N.R.	N.R.	Ring
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG 05894-3.GPJ CHJ.GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

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EXPLORATORY BORING NO. 11

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with gravel to 2", brown	Native (QyF)				3.9		
		(SM) Silty Sand, fine to medium with coarse and gravel to 1", light brown		X		16	4.7	117	Ring
5		(SM) Silty Sand, fine to medium with coarse and clay, red brown	(Qzfs)			13	5.0	111	Ring
10		(SM) Silty Sand, fine to medium with coarse and clay, red brown		X		29	10.1	124	Ring
15						300"	N.R.	N.R.	Ring
20		END OF BORING NO BEDROCK REFUSAL AT 18.5' ON BOULDERS NO FILL MODERATE CAVING NO FREE GROUNDWATER	Refusal						
25									
30									

BORING LOC. 05894-3.GPJ CHJ/COT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

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EXPLORATORY BORING NO. 12

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BUT.K.				
		(SM) Silty Sand, fine to coarse with gravel to 3", brown	Fill				3.9		
5			(QvE)	X		19	N.R.	N.R.	Ring
10				X		30/5"	N.R.	N.R.	Ring
15				X		30/5"	N.R.	N.R.	Ring
		(SP-SM) Sand, fine to medium with silt, coarse, and gravel to 1 1/2", light brown					4.7		
20				X		38	5.0	120	Ring
25		END OF BORING	Refusal			30/2"	N.R.	N.R.	Ring
30		NO BEDROCK REFUSAL AT 23.0' ON BOULDERS NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG 05894-3.GPJ CHJ/GDT 5/1/2006



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-12

EXPLORATORY BORING NO. 13

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 2". brown	Native (Qof)				6.2		
5				X		28			SPT
10		(SM) Silty Sand, fine to medium with gravel to 1", brown				28	6.7		SPT
15		(SM) Silty Sand, fine to coarse, brown				55			SPT
20						42	7.5		SPT
25				X		70/5"			SPT
30		(SM) Silty Sand, fine to coarse, brown				70/5"			SPT
				X		70/5"			SPT

BORING LOG 03d844-3.GPJ CIL:GDT 5/12/05



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-13a

EXPLORATORY BORING NO. 13

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
40		(SM) Silty Sand, fine to coarse, brown				70/5"			SPT
45		END OF BORING	Refusal			70/5"			SPT
50		NO BEDROCK REFUSAL AT 44.0' NO FILL MODERATE CAVING NO FREE GROUNDWATER							
55									
60									
65									

BORING LOG CBB94-S.GFJ CHJ/GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-13b

EXPLORATORY BORING NO. 14

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
			(Qtz)						
		END OF BORING	Refusal	X		31	2.4	120	Ring
5		NO BEDROCK REFUSAL AT 3.0' ON BOULDERS NO FILL MODERATE CAVING NO FREE GROUNDWATER							
10									
15									
20									
25									
30									

BORING LOG #5894-3 CPJ CHJ.GDT 5/2006



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
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EXPLORATORY BORING NO. 15

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
5		(SM) Silty Sand, fine to medium with coarse and gravel to 1", brown	Fill				4.6		
10		(SP-SM) Sand, fine to medium with coarse, silt and gravel to 1", light brown	Native (Qyt)				3.5	125	Ring
15							5.2	112	Ring
20		(SM) Silty Sand, fine to coarse with gravel to 1", gray brown					2.3		
25		(SP-SM) Sand, fine to coarse with silt and gravel to 1 1/2", light brow					3.1	Dist.	Ring
30		END OF BORING NO BEDROCK NO REFUSAL FILL TO 7.0' MODERATE CAVING NO FREE GROUNDWATER					3.8	112	Ring, DS
							6.4		
							8.4	123	Ring
							6.4		
						30/6"		Dist.	Ring

BORING LOG 05894-3.GPJ 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-15

EXPLORATORY BORING NO. 16

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 1 1/2", brown	Fill				3.4		
		(SM) Silty Sand, fine to medium with coarse and gravel to 1 1/2", brown	Native (Qyf)	X		35	2.6	123	Ring
5		(SP-SM) Sand, fine to medium with coarse, silt and gravel to 1", light brown					3.1		
				X		25	3.5	123	Ring
10									
				X		36	2.4	115	Ring
15									
						30-3"	N.R.	N.R.	Ring
20									
						30-4"	3.4	Dist.	Ring
25		END OF BORING							
		NO BEDROCK NO REFUSAL FILL TO 2.0' MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING_LOG 06894-3.CPJ CHJ/GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
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EXPLORATORY BORING NO. 17

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
5		(SM) Silty Sand, fine to medium with gravel to 1", light brown	Native (Q _{u6})				2.3		
						35	2.1	126	Ring
						37	2.9	Dist.	Ring
10		(SP-SM) Sand, fine to coarse with silt and gravel to 3/8", light brown					2.8		SA
						41	4.0	123	Ring
15		(SP-SM) Sand, fine to medium with coarse and silt, light brown				30/4"	6.0	Dist.	Ring
							8.7		
20						55/10"	7.5	119	Ring
25		END OF BORING							
30		NO BEDROCK NO REFUSAL NO FILL SLIGHT CAVING NO FREE GROUNDWATER							

BORING LOG: 05894-3 GFL CH. SPT 5/12/03



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-17

EXPLORATORY BORING NO. 18

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 75 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (#)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Fquiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BLK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 1 1/2", brown	Native (Qof)				4.3		
5				X		10	3.3	112	Ring
10		(SM) Silty Sand, fine to coarse with gravel to 2", brown		X		14	2.6	119	Ring
							3.8		MDC, SA
15				X		25	3.5	125	Ring
20		(SP-SM) Sand, fine to coarse, silt and with gravel to 1", light brown		X		41	6.7	Dist.	Ring
							4.4		
25		END OF BORING		X		23	3.8	123	Ring
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING - CG 05894-3.GPJ CHJ/GDT 3/7/2006



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-18

EXPLORATORY BORING NO. 19

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 75 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse, gravel to 2" and cobbles to 5", brown	Native (Qof)				3.5		
5				X		10	3.6	111	Ring
				X		24	2.2	Dist.	Ring
10		(SM) Silty Sand, fine to coarse with gravel to 1", light brown					2.7		
				X		31	2.8	Dist.	Ring
15				X		30/6"	3.4	121	Ring
20				X		30/6"	N.R.	N.R.	Ring
25				X		30/5"	2.9	Dist.	Ring
		END OF BORING							
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOC. 06894-3.GPI.CHJ.GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-19

EXPLORATORY BORING NO. 20

Date Drilled: 2/22/06 Client: Inland Communities Corporation
 Equipment: CMF 75 Drill Rig Driving Weight / Drop: 140 lbs/30 in
 Surface Elevation(ft): N/A Logged by: J.S. Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Eq. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(GW) Sandy Gravel, fine to coarse; gravel and cobbles to 5", brown	Native (Qty)				2.3		Cor. DS, MDC, SA
5				X		10	N.R.	N.R.	Ring
10		(SM) Silty Sand, fine to coarse with gravel and cobbles to 5", light brown		X		45/10"	2.3	110	Ring
15				X		12	3.9	111	Ring, Consol.
20		END OF BORING	Sampler Broke						
25		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG C:\994-3\GFJ CIL.GDT 5/12/05

EXPLORATORY BORING NO. 21

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 75 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 2", brown	Native (Q _{sf})				5.0		
						25			SPT
5		(SP-SM) Sand, fine to coarse with silt and gravel to 2", light brown	(Q _{sf})				2.0		
						27			SPT
10						98			SPT
15						70/4"			SPT
20						70/1"			SPT
25						70/2"			SPT
30						70/6"			SPT

BORING LOG 05894-3.GPJ CHL_SDT 5/12/05



PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-21a

EXPLORATORY BORING NO. 21

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 75 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SP-SM) Sand, fine to coarse with silt and gravel to 2", light brown							
		END OF BORING	Refusal						
40		NO BEDROCK REFUSAL AT 37.5' ON BOULDERS NO FILL MODERATE CAVING NO FREE GROUNDWATER							
45									
50									
55									
60									
65									

BORING_O3_05394-3.GPJ CHJ.GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-21b

EXPLORATORY BORING NO. 22

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SP-SM) Sand, fine to coarse with silt and gravel and cobbles to 4", light brown	Native (Qof)				4.1		
5				X		19	4.8	117	Ring
10				X		19	3.8	113	Ring
15				X		43	5.2	115	Ring
20		END OF BORING	Refusal	X		30/6"	7.1	121	Ring
25		NO BEDROCK REFUSAL AT 19.0' ON BOULDERS NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG CMBE-3.GPJ CHJ/GDJ 1/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-22

EXPLORATORY BORING NO. 23

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
5		(SM) Silty Sand, fine to coarse with gravel to 1", brown	Native (Qo5)		XXXX		4.8		Cor., DS, MDC, SA
				X		28	4.6	122	Ring
10		(SM) Silty Sand, fine to coarse with gravel to 1", brown			XXXX		4.1		
				X		30/6"	4.9	115	Ring
15							6.8		
				X		56/11"	6.8	131	Ring
20							6.6		
				X		30/6"	6.6	115	Ring
25							5.9		
				X		30/5"	5.9	115	Ring
30							4.0		
				X		30/6"	4.0	Dist.	Ring
		(SP-SM) Sand, fine to coarse with gravel to 2", brown					3.6		

BCRING.LOG 05894-3.GPJ CHJ.GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-23a

EXPLORATORY BORING NO. 23

Date Drilled: 2/22/06 Client: Inland Communities Corporation
 Equipment: CME 55 Drill Rig Driving Weight / Drop: 140 lbs/30 in
 Surface Elevation(0): N/A Logged by: J.S. Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
38		(SP-SM) Sand, fine to coarse with gravel to 2", brown				30/1"	4.1	Dist	Ring
40						30/2"	4.0	Dist	Ring
45						30/3"	3.7	Dist	Ring
50						30/5"	N.R.	N.R.	Ring
55		END OF BORING NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
60									
65									

BORING LOG 05894-3.GPJ CHL GDT 5/12/05



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No. 05894-3 Enclosure B-23b

EXPLORATORY BORING NO. 24

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 1 1/2", brown	Native (Q _{uf})				7.6		
5				X		3	3.3	111	Ring
10			(Q _{uf})	X		35	2.5	122	Ring
15				X		34	1.9	112	Ring
20				X		30 1/2"	N.R.	N.R.	Ring
25		END OF BORING		X		30 1/2"	3.7		Ring
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG 05894-3 GFJ CHJ GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-24

EXPLORATORY BORING NO. 25

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to coarse with gravel to 1 1/2", brown	Native (Qsf)				10.3		
						4	7.1	103	Ring
5		(SM) Silty Sand, fine to medium with coarse and gravel to 1", light brown					3.7		
						7	3.6	110	Ring
		(SP-SM) Sand, fine to coarse with silt and gravel to 1", light brown					3.4		
10						35	3.0	118	Ring
15						30:6"	5.4	Dist.	Ring
20						50	2.9	115	Ring
		END OF BORING							
25		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG C5894-3.GPJ CHJ.GDT 5/12/05



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-25

EXPLORATORY BORING NO. 26

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 2", brown	Native (Qof)				9.4		
5		(SM) Silty Sand, fine to coarse with gravel to 1", light brown				23	4.6	118	Ring
						30 5/8"	5.4	Dist.	Ring
10						32	2.9	119	Ring
15						30 6"	3.5	Dist.	Ring
20						30 6"	3.0	Dist.	Ring
25		END OF BORING							
		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG 05894-3.DWG CHJ SPT 5" 2/26



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-26

EXPLORATORY BORING NO. 27

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to coarse with gravel to 1 1/2", brown	Native (Q ₀)				9.4		
5				X		19	6.4	Dist.	Ring
		(SM) Silty Sand, fine to coarse with gravel to 1 1/2", light brown					4.1		
10				X		15	2.6	120	Ring
		(SP-SM) Sand, fine to medium with coarse and gravel to 1 1/2", light brown					3.6		
15				X		48	3.2	125	Ring
							3.6		
20				X		45	2.7	115	Ring
							3.6		
25				X		30/5"	2.8	Dist.	Ring
							3.6		
30		END OF BORING				30/3"	N.R.	N.R.	Ring
		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG: 05894-3 (SP), CHJ/GDT, 5/1/2006



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
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EXPLORATORY BORING NO. 28

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
5		(SM) Silty Sand, fine to medium with coarse and gravel to 1 1/2", brown	Native (Qc3)	X		23	8.0	110	Ring
		(SM) Silty Sand, fine to coarse with gravel to 1 1/2", light brown			X			3.4	
10		(SP-SM) Sand, fine to coarse with silt and gravel to 1", light brown		X		26	N.R.	N.R.	Ring
					X			4.7	
15				X		50	3.6	124	Ring
					X		30-6"	N.R.	N.R.
20		END OF BORING	Refusal						
25		NO BEDROCK REFUSAL AT 18.0' ON BOULDERS NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG 05894-3.GPJ CHJ.COT: 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-28

EXPLORATORY BORING NO. 29

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 55 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 1 1/2", brown	Native (Qof)				8.6		
5				X		43	8.6	Dist.	Ring
		(SM) Silty Sand, fine to coarse with gravel to 1", light brown					2.5		
10				X		31	2.5	115	Ring
15				X		28	5.9	125	Ring
		(SP-SM) Sand, fine to medium with silt and gravel to 1", light brown					4.2		
20				X		4	6.3	99	Ring, Consol.
25				X		30/5"	3.4	118	Ring
		END OF BORING							
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG 05894-3.SFU CHJ/COT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-29

EXPLORATORY BORING NO. 30

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 75 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to coarse with gravel to 2", light brown	Native (Qyt)				4.0		
5				X		28	4.2	Dist.	Ring
10			(Qof)	X		44	2.8	115	Ring
15		(SM) Silty Sand, fine to medium with coarse and gravel to 1", light brown		X		44	3.7	125	Ring
20				X		30/4"	2.0	Dist.	Ring
25		END OF BORING		X		30/6"	4.5	Dist.	Ring
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG 05894-3.GPJ CHJ/GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-30

EXPLORATORY BORING NO. 31

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: CME 75 Drill Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to coarse with gravel to 2", brown	Native (Qw)			21	4.6	Dist.	Ring
5		(SM) Silty Sand, fine to coarse with gravel to 1 1/2", brown					10.5		SA
						12	10.0	119	Ring
10									
						16	10.7	115	Ring
15		(SP-SM) Sand, fine to coarse with silt and gravel to 1", light brown	(Qof)				2.5		
						46/10"	5.6	117	Ring
20		(SM) Silty Sand, fine to coarse with gravel to 1", light brown					5.5		
						30/6"	5.9	Dist.	Ring
25		(SP-SM) Sand, fine to coarse with silt and gravel to 1", light brown					2.5		
						38	3.6	124	Ring
30		NO BEDROCK REFUSAL AT 33.0' ON BOULDERS NO FILL MODERATE CAVING NO FREE GROUNDWATER							
		END OF BORING	Refusal			30/3"	3.2	Dist.	Ring

BORING LOG: 05894-3.GPJ CHJ GDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-31

EXPLORATORY BORING NO. 32

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: Tract Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 1", brown	Native (Qw)				66		
5				X		8	6.2	111	Ring
10				X		10	4.7	109	Ring
15		(SP-SM) Sand, fine to coarse with silt, light brown	(Qt)	X		30.5"	N.R.	N.R.	Ring
20				X		29	3.4	123	Ring
25		END OF BORING		X		45	2.9	123	Ring
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG 05894-3.SPJ CHJ.GDT 5/12/06



PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No. 05894-3
Enclosure B-32

EXPLORATORY BORING NO. 33

Date Drilled: 2/22/06

Client: Inland Communities Corporation

Equipment: Tract Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 1", brown	Native (Qw)				9.6		
5			(Qf)			4	16.0	97	Ring
10						30/5"	N.R.	N.R.	Ring
15		(SM) Silty Sand, fine to medium with coarse and gravel to 2", light brown				26	7.5	117	Ring
20						30/5"	4.5	124	Ring
25		END OF BORING							
30		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG: 06894 3.GPJ CHJ.GDI 06/2006



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-33

EXPLORATORY BORING NO. 34

Date Drilled: 3/8/06
Equipment: Tract Rig
Surface Elevation(ft): N/A

Client: Inland Communities Corporation
Driving Weight / Drop: 140 lbs/30 in
Logged by: J.S.
Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
0 - 5		(SM) Silty Sand, fine to coarse with gravel and cobbles to 4", brown	Native (Qy6)				3.4		
5 - 10						37	N.R.	N.R.	Ring
10 - 15		(SP-SM) Sand, fine to coarse with silt and gravel to 1 1/2", light brown	(Qof)			70	2.4	118	Ring
15 - 20						48	7.1	124	Ring
20 - 25		(SM) Silty Sand, fine to coarse with gravel to 1", light brown				30/6'	5.6	115	Ring
25 - 30		END OF BORING NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							

BORING LOG: 05894-3.GPJ CHJGDT 5/12/06



C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

Job No.
05894-3

Enclosure
B-34

EXPLORATORY BORING NO. 35

Date Drilled: 3/8/06

Client: Inland Communities Corporation

Equipment: Tract Rig

Driving Weight / Drop: 140 lbs/30 in

Surface Elevation(ft): N/A

Logged by: J.S.

Measured Depth to Water(ft): N/A

DEPTH (ft)	GRAPHIC LOG	VISUAL CLASSIFICATION	REMARKS	SAMPLES		BLOWS/FOOT (Equiv. SPT)	FIELD MOISTURE (%)	DRY UNIT WT. (pcf)	LAB/FIELD TESTS
				DRIVE	BULK				
		(SM) Silty Sand, fine to medium with coarse and gravel to 1 1/2", brown	Native (Qof.)				4.0		
5				X		5	7.3	107	Ring
7				X		7	2.7	104	Ring
10				X		10	3.4	107	Ring, Consol.
15		(SM) Silty Sand, fine to medium with coarse and gravel to 1 1/2", light brown							
15				X		50/9"	4.8	104	Ring
20				X		30/6"	4.3	Dist.	Ring
		END OF BORING							
25		NO BEDROCK NO REFUSAL NO FILL MODERATE CAVING NO FREE GROUNDWATER							
30									

BORING LOG 05894-3.GPJ CJ-J.GDT 5/12/06



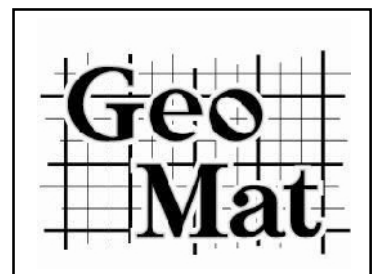
C.H.J.

PARADISE HILLS PROJECT
BADGER CANYON AREA, CALIFORNIA

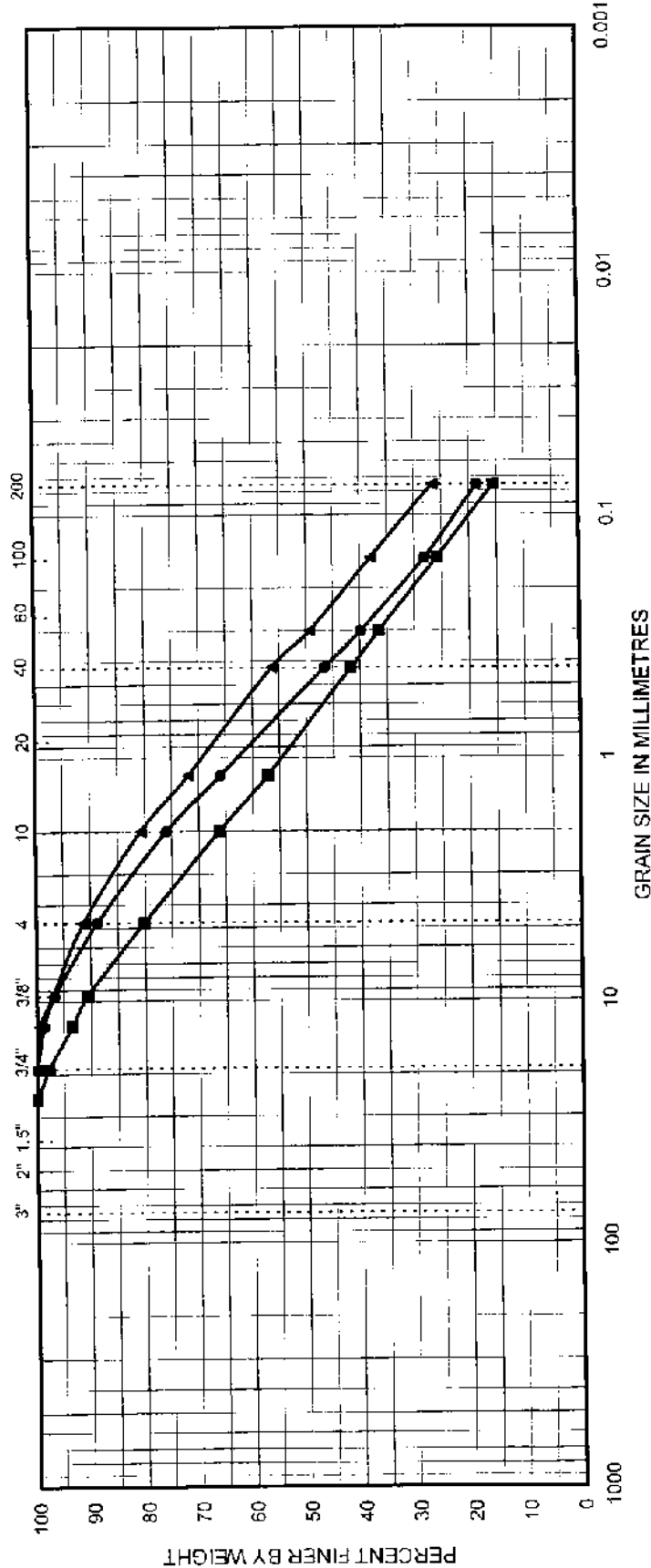
Job No.
05894-3

Enclosure
B-35

$\beta^{\circ} \circ \gg 2\frac{1}{4} \cdot \ddot{\cdot} \acute{Y}$



Sieve Sizes - U.S.A. Standard Series (ASTM C136)



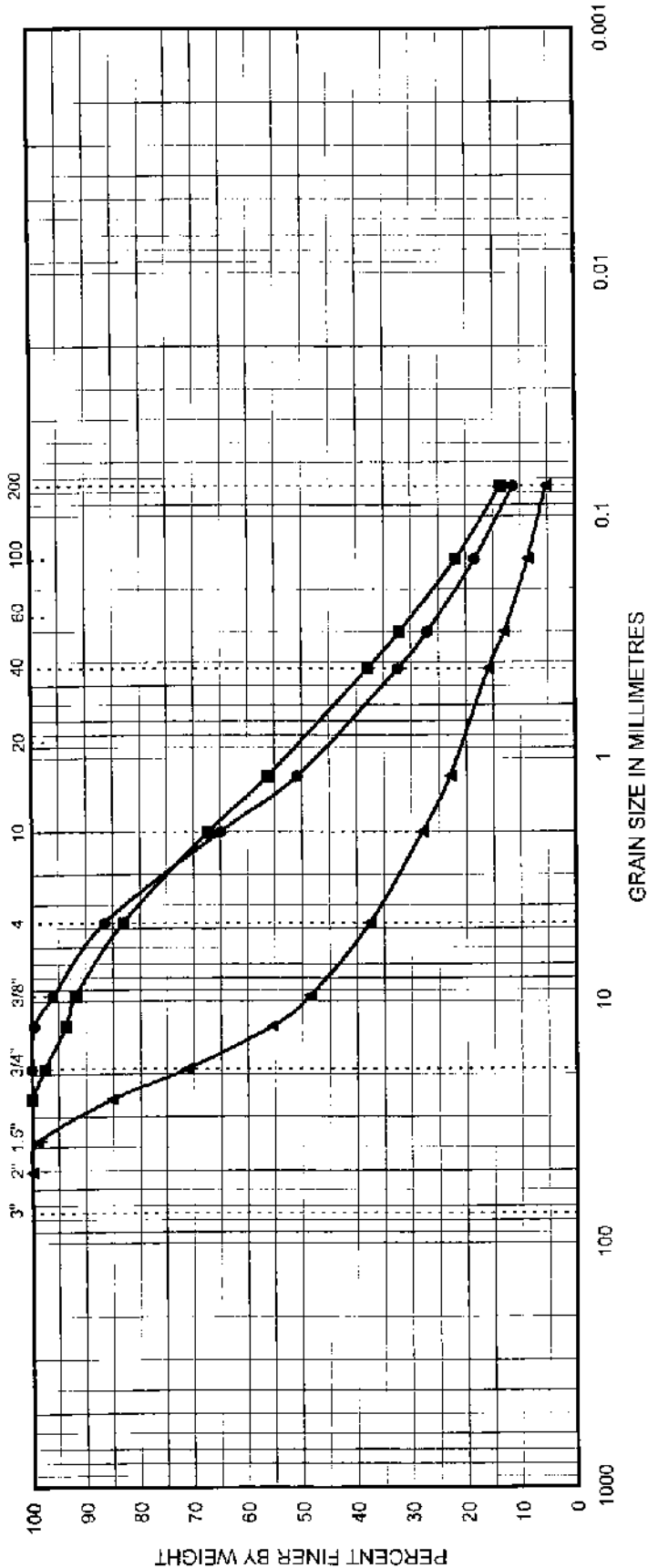
Symbol	Boring No.	Depth (ft)	Classification	Gravel			Sand			Silt			Clay		
				Coarse	Fine		Coarse	Medium	Fine	D ₁₀ (mm)	D ₃₀ (mm)	D ₅₀ (mm)	D ₆₀ (mm)	C _u	C _c
●	2	0	(SM) Silty sand, fine to coarse with gravel to 3/8"							0.168	0.509	0.864			
■	4	0	(SM) Silty sand, fine to coarse with gravel to 3/4"							0.197	0.736	1.393			
▲	10	0	(SM) Silty sand, fine to coarse with gravel to 3/8"							0.092	0.311	0.539			

GRADATION CURVES

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job Number:	05894-3	Enclosure:	C-1



Sieve Sizes - U.S.A. Standard Series (ASTM C136)



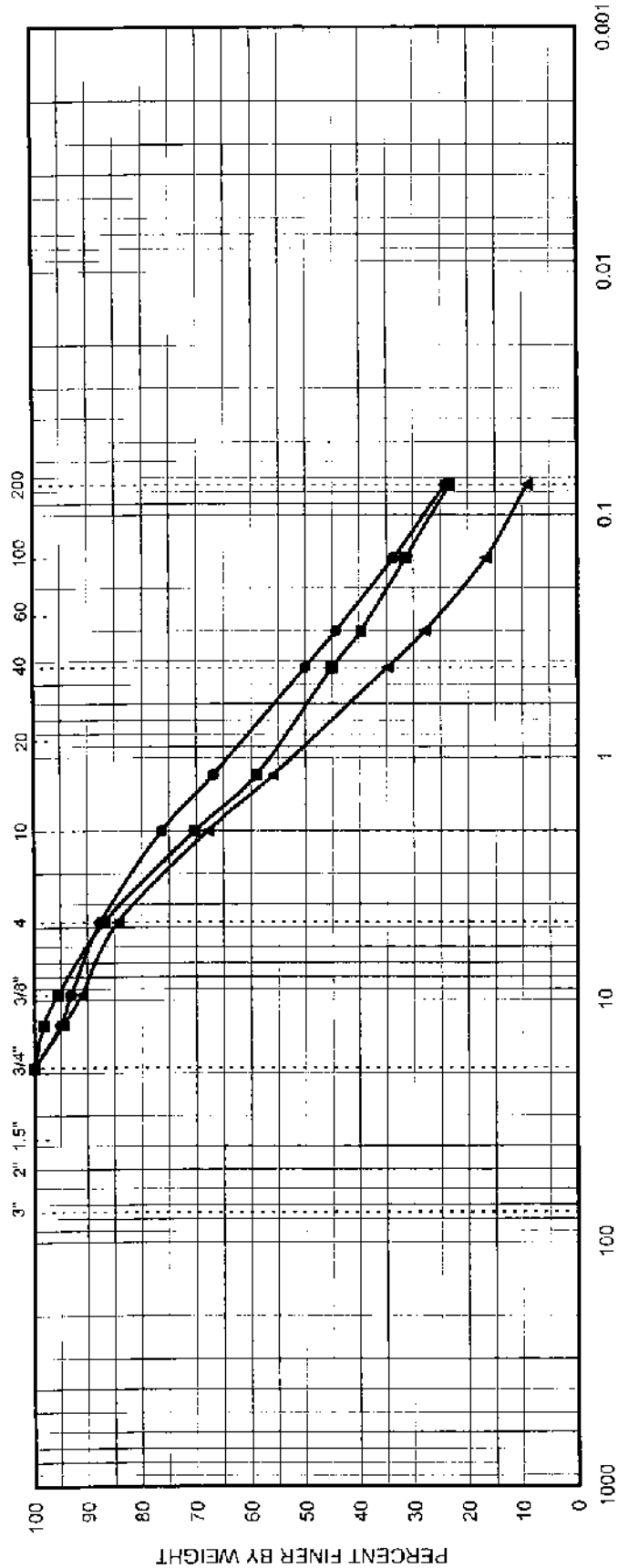
Symbol	Boring No	Depth (ft)	Classification	Gravel			Sand			Silt			Clay		
				Coarse	Fine		Coarse	Medium	Fine	D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)		C _u	C _c
●	17	8	(SP-SM) Sand, fine to coarse with gravel to 3/8"							0.354	1.127	1.663			
■	18	10	(SM) Silty sand, fine to coarse with gravel to 3/8"							0.260	0.836	1.418			
▲	20	0	(GW) Sandy gravel to 1", fine to coarse							0.1853	2.390	10.110	77.077	2.159	

GRADATION CURVES

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job Number:	05894-3	Enclosure:	C-2



Sieve Sizes - U.S.A. Standard Series (ASTM C136)

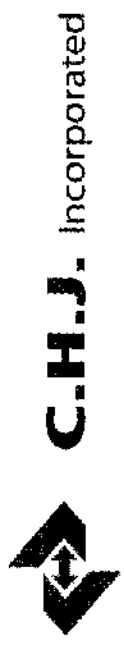


GRAIN SIZE IN MILLIMETRES

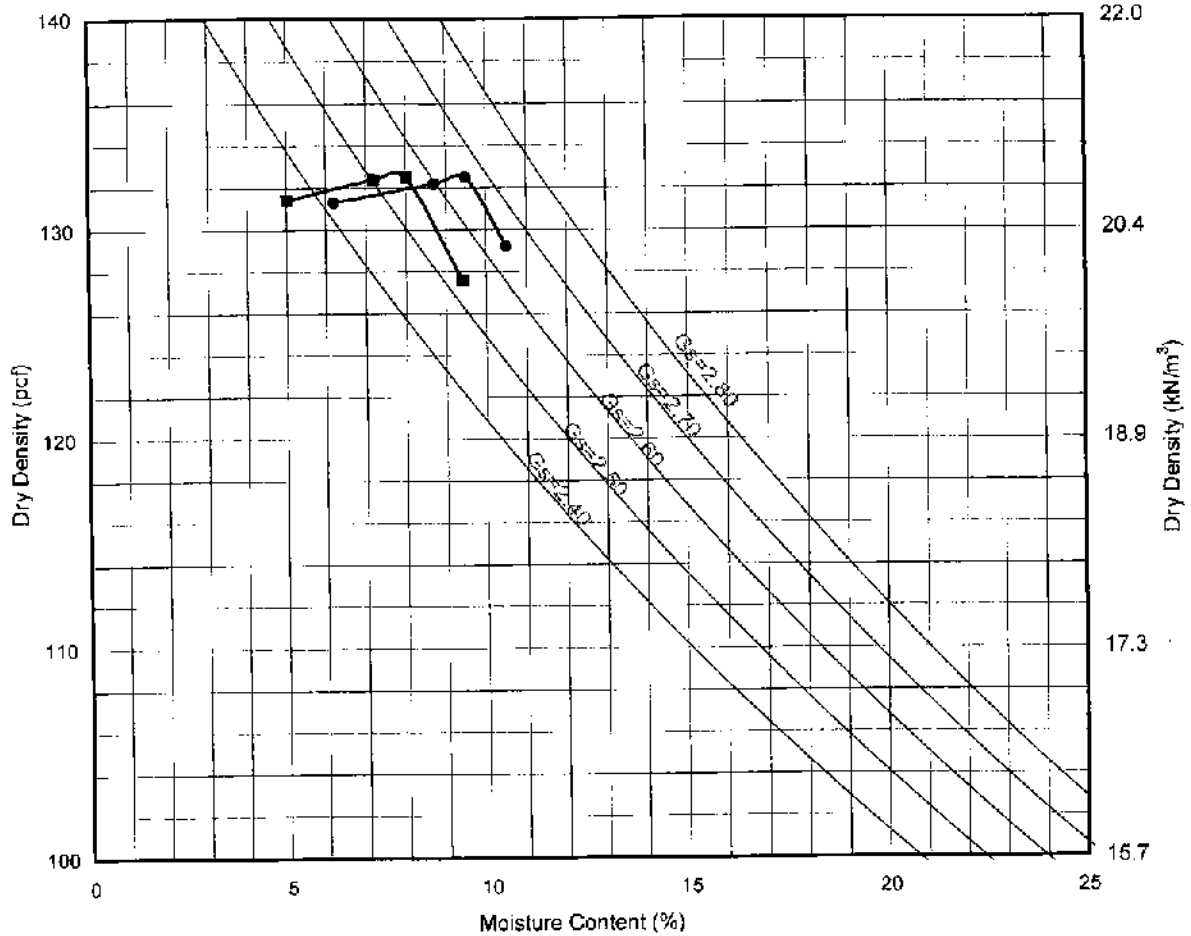
Symbol	Boring No.	Depth (ft)	Classification	Gravel			Sand			Silt			Clay			
				Coarse	Fine		Coarse	Medium	Fine	D ₁₀ (mm)	D ₃₀ (mm)	D ₅₀ (mm)	D ₆₀ (mm)	C _u	C _c	SE
●	23	0	(SM) Silty sand, fine to coarse with gravel to 1/2"							0.115	0.423	0.775				
■	31	3	(SM) Silty sand, fine to coarse with gravel to 3/8"							0.133	0.610	1.237				
▲	A		(SP-SM) Sand, fine to coarse with gravel to 1/2"							0.0816	0.334	0.864	1.411	17.294	0.967	

GRADATION CURVES

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job Number:	05894-3	Enclosure:	C-3



Maximum Density Optimum Moisture Determination Test (ASTM 1557)



Boring #	Depth(ft)	Soil/Sample Type	γ_{max} (pcf)	w_{opt} (%)
●	2	0 (SM) Silty sand, fine to coarse with gravel to 3/8"	132.5	9.5
■	4	0 (SM) Silty sand, fine to coarse with gravel to 3/4"	132.5	8.0

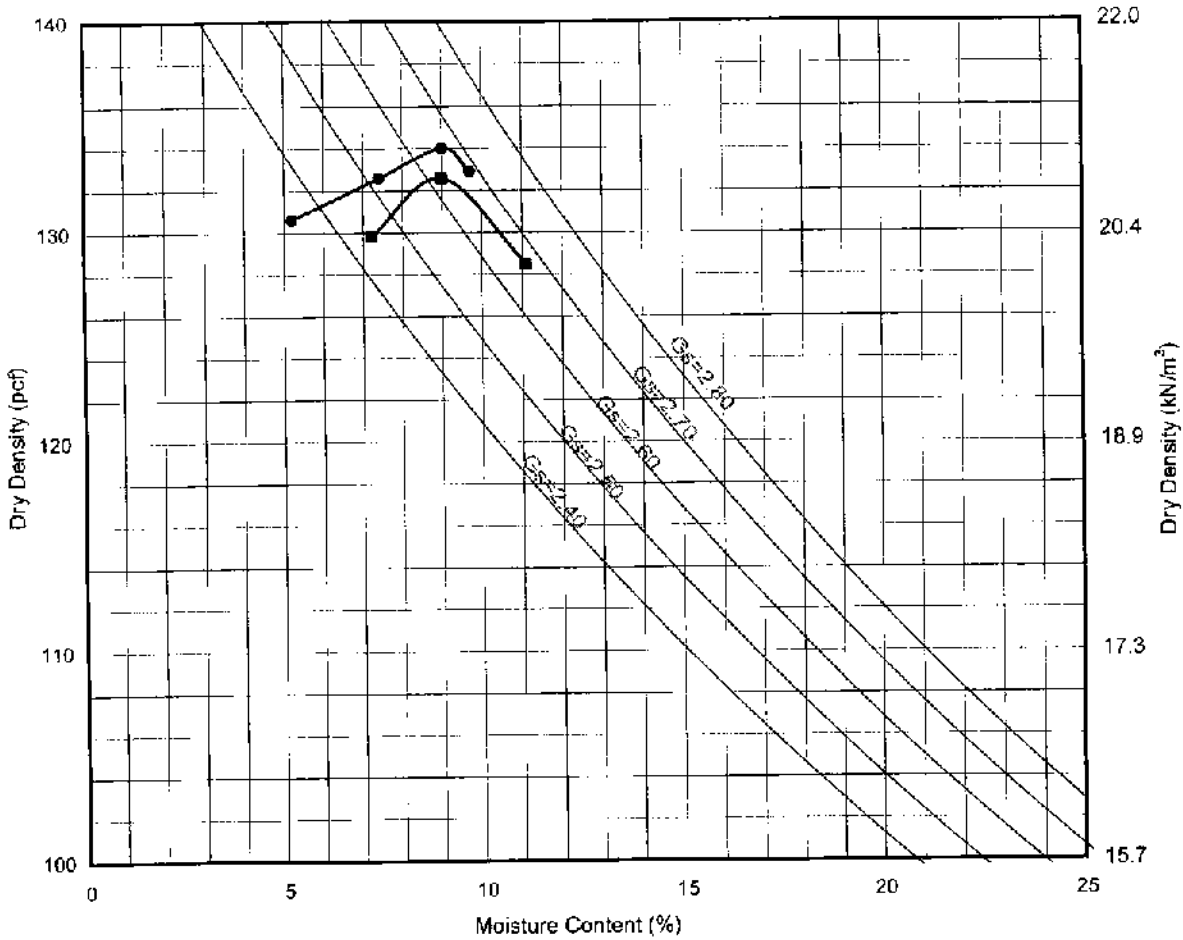


C.H.J. Incorporated

MAXIMUM DENSITY TESTS

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-4

Maximum Density Optimum Moisture Determination Test (ASTM 1557)



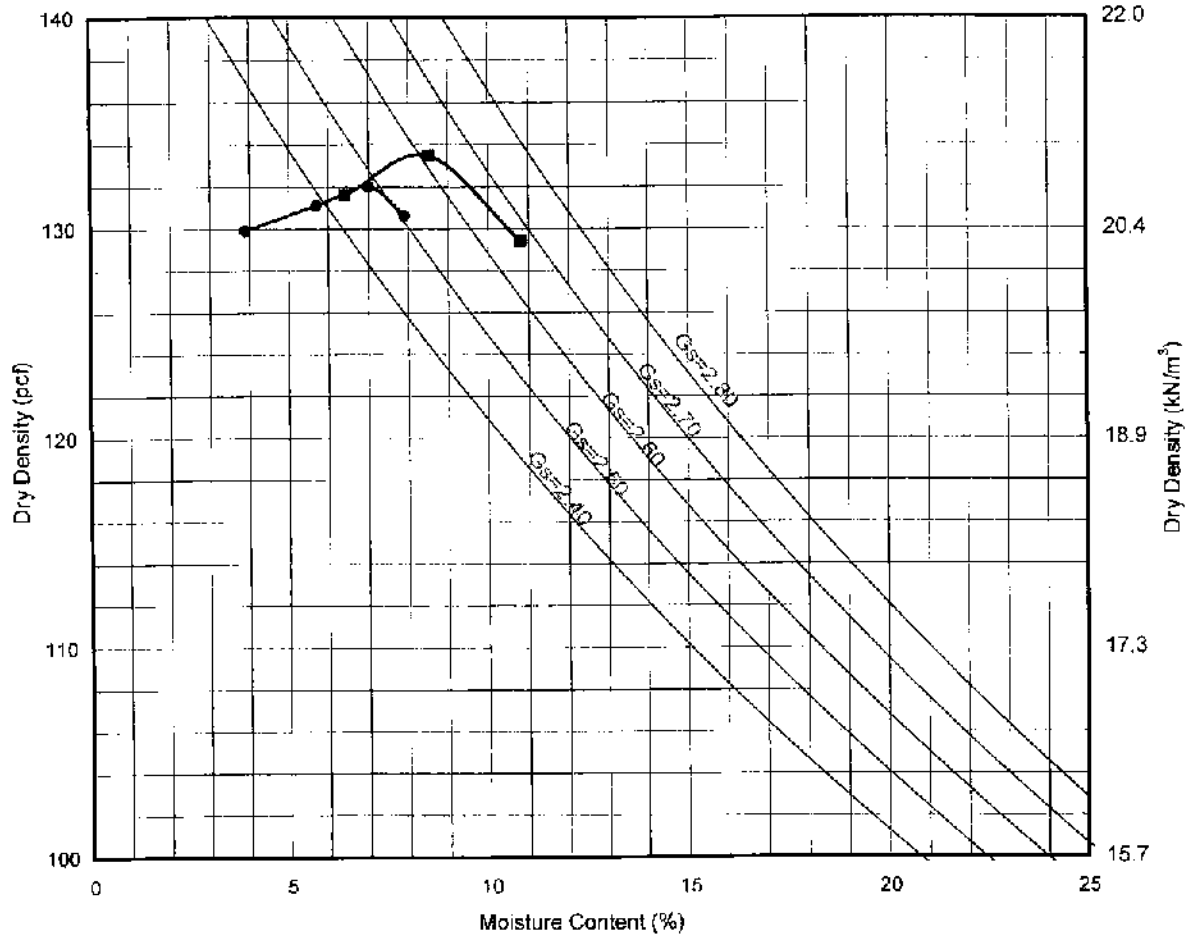
Boring #	Depth(ft)	Soil/Sample Type	γ_{max} (pcf)	w_{opt} (%)
● 10	0	(SM) Silty sand, fine to coarse with gravel to 3/8"	134.0	9.0
■ 18	10	(SM) Silty sand, fine to coarse with gravel to 3/8"	133.5	9.5



MAXIMUM DENSITY TESTS

Project:	Tentative Tract Map No. 19140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-5

Maximum Density Optimum Moisture Determination Test (ASTM 1557)



Boring #	Depth(ft)	Soil/Sample Type	ρ_{max} (pcf)	w_{opt} (%)
■ 20	0	(GW) Sandy gravel to 1", fine to coarse	132.0	7.0
■ 23	0	(SM) Silty sand, fine to coarse with gravel to 1/2"	134.0	9.0

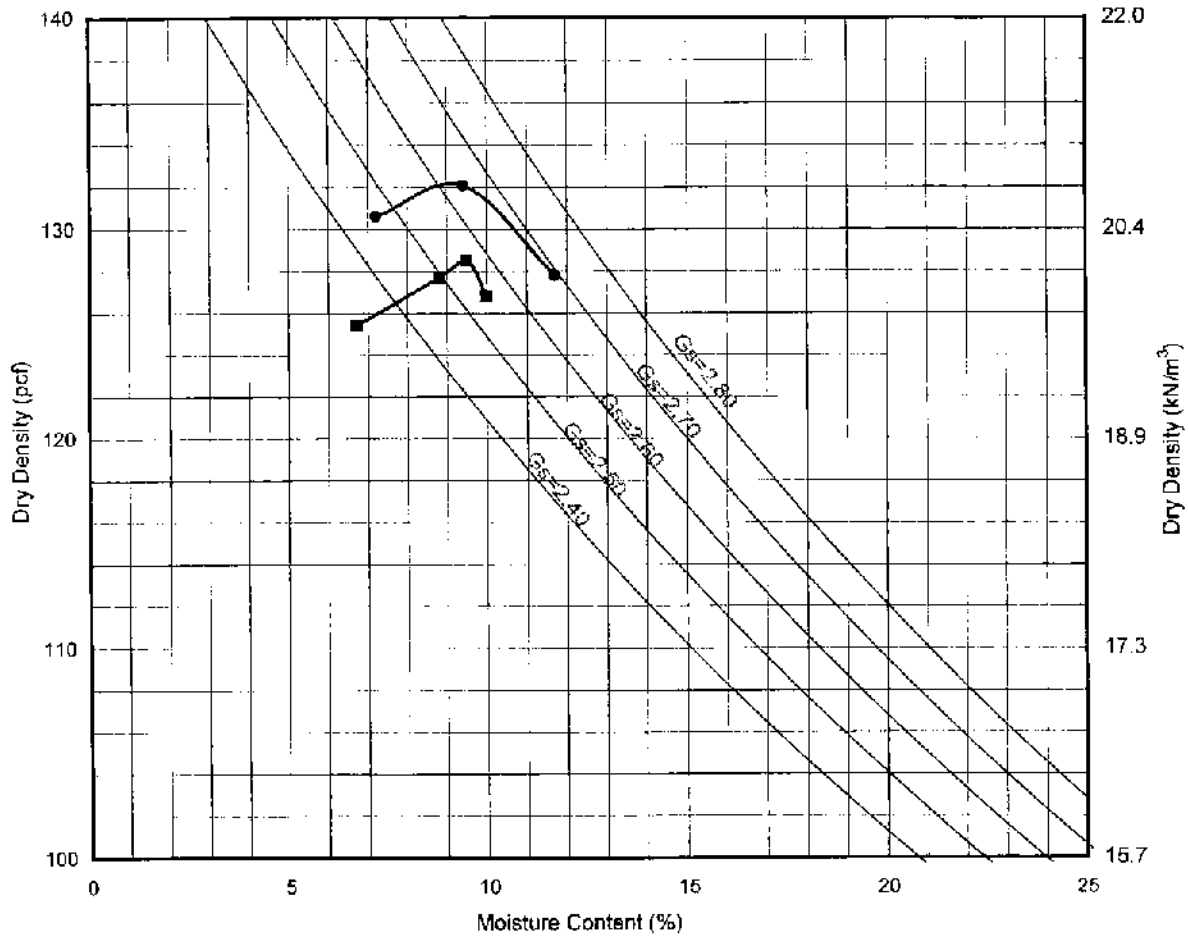


C.H.J. Incorporated

MAXIMUM DENSITY TESTS

Project:	Tentative Tract Map No. 18140, Inland Communities Corp		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-6

Maximum Density Optimum Moisture Determination Test (ASTM 1557)



Boring #	Depth(ft)	Soil/Sample Type	γ_{max} (pcf)	w_{opt} (%)
• 31	0	(SM) Silty sand, fine to coarse with gravel to 3/8"	132.5	10.0
■ A		(SP-SM) Sand, fine to coarse with gravel to 1/2"	128.5	9.5

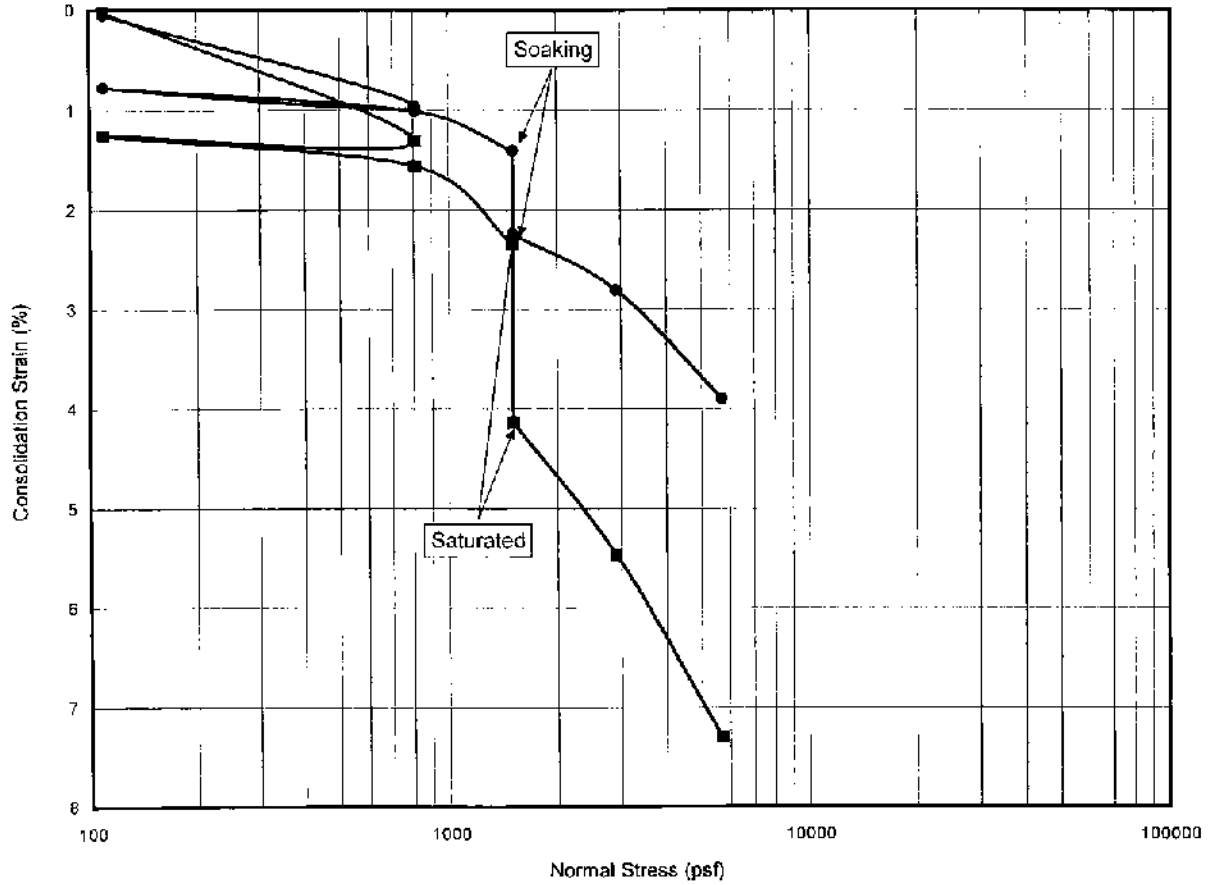


C.H.J. Incorporated

MAXIMUM DENSITY TESTS

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-7

Consolidation Test (ASTM D 2435)



Boring #	Depth(ft)	Soil/Sample Type	γ_d (pcf)	MC(%)	HCS(%)
2	12	(SP-SM) Sand, fine to coarse with silt and gravel to 1"	110	3.5	0.84
10	17	(SM) Silty sand, fine to medium with gravel and cobbles to 5"	111	9.6	1.80

* HCS - Hydroconsolidation strain in percent.

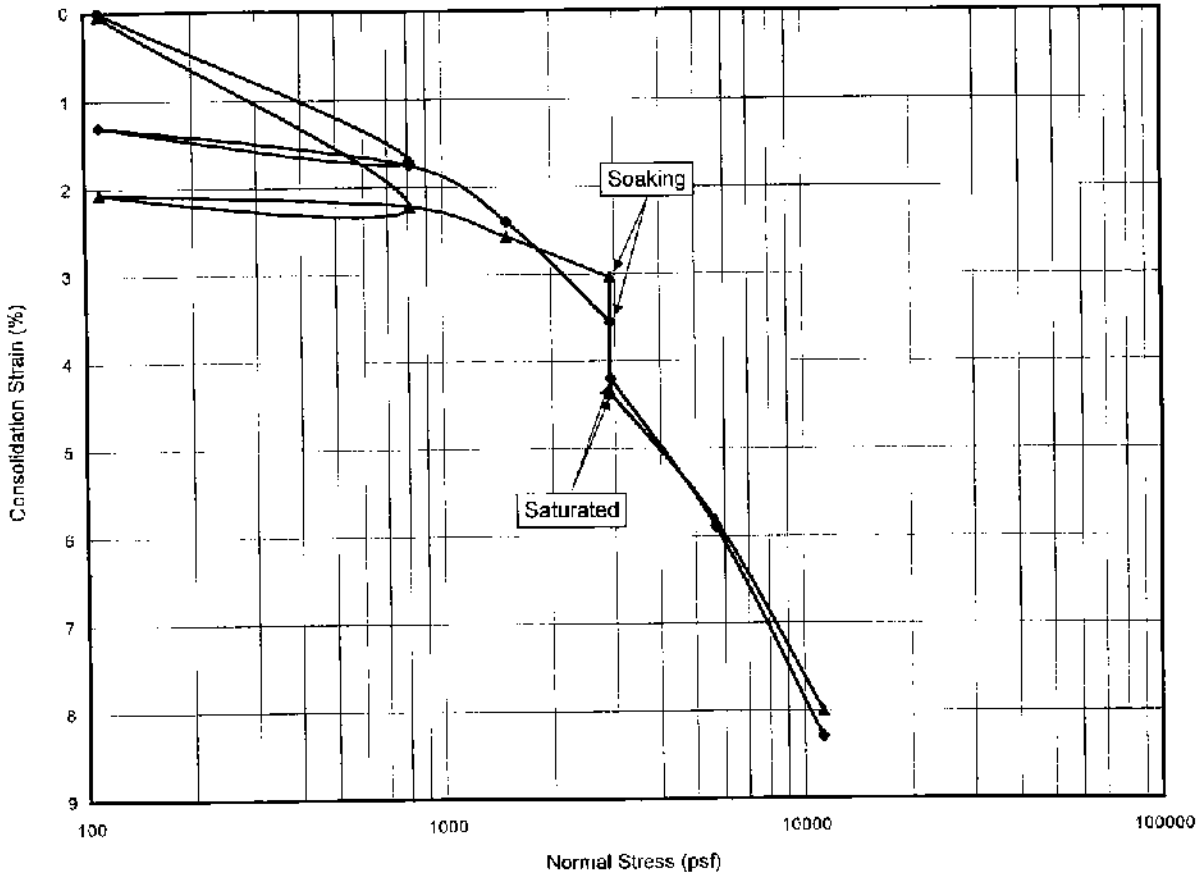


C.H.J. Incorporated

CONSOLIDATION TESTS

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-8

Consolidation Test (ASTM D 2435)



Boring #	Depth(ft)	Soil/Sample Type	γ_d (pcf)	MC(%)	HCS(%)
● 20	12	(SM) Silty sand, fine to coarse with gravel and cobbles to 5"	111	3.9	1.33
■ 29	20	(SP) Sand, fine to medium with silt and gravel to 1"	99	6.3	0.65

* HCS - Hydroconsolidation strain in percent.

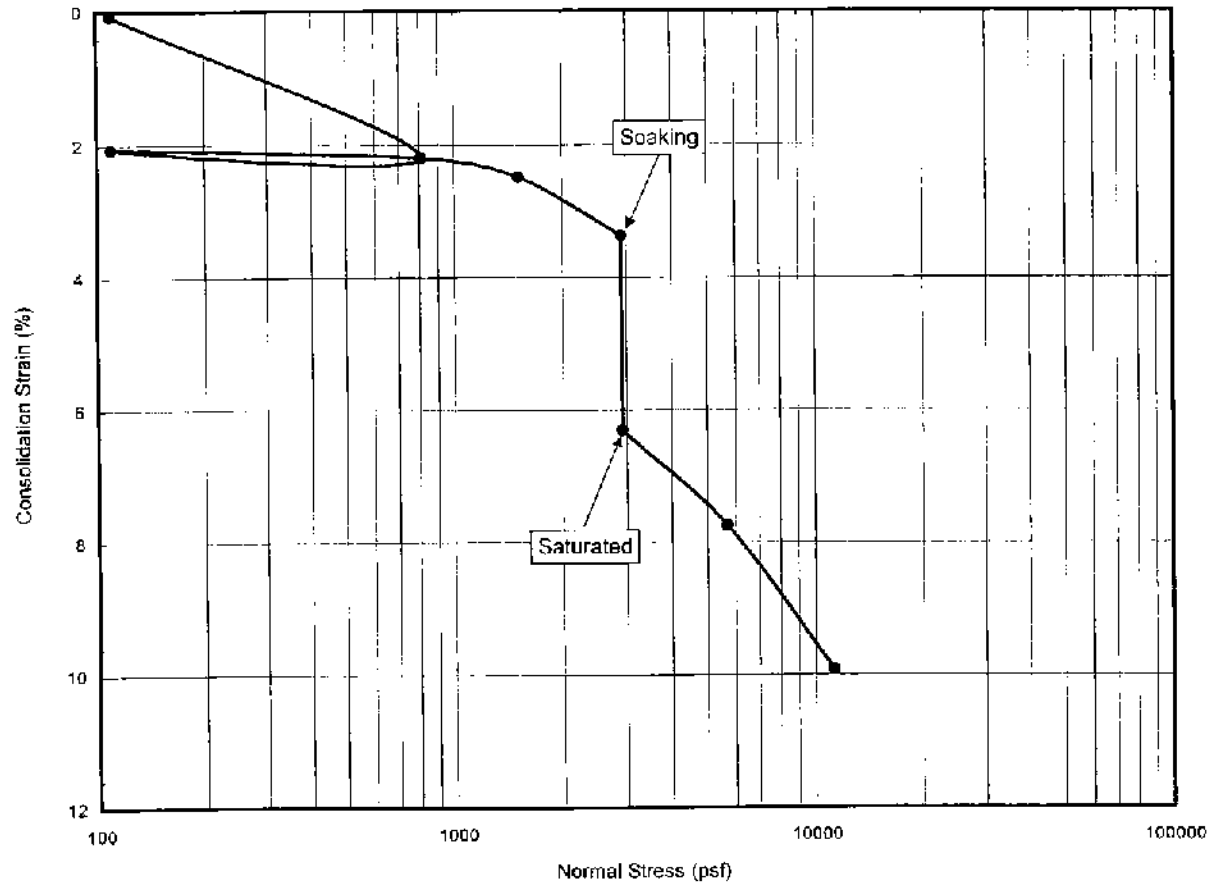


C.H.J. Incorporated

CONSOLIDATION TESTS

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-9

Consolidation Test (ASTM D 2435)



Boring #	Depth(ft)	Soil/Sample Type	γ_s (pcf)	MC(%)	HCS(%)
• 35	10	(SM) Silty sand, fine to medium with coarse and gravel to 1 1/2"	107	3.4	2.94

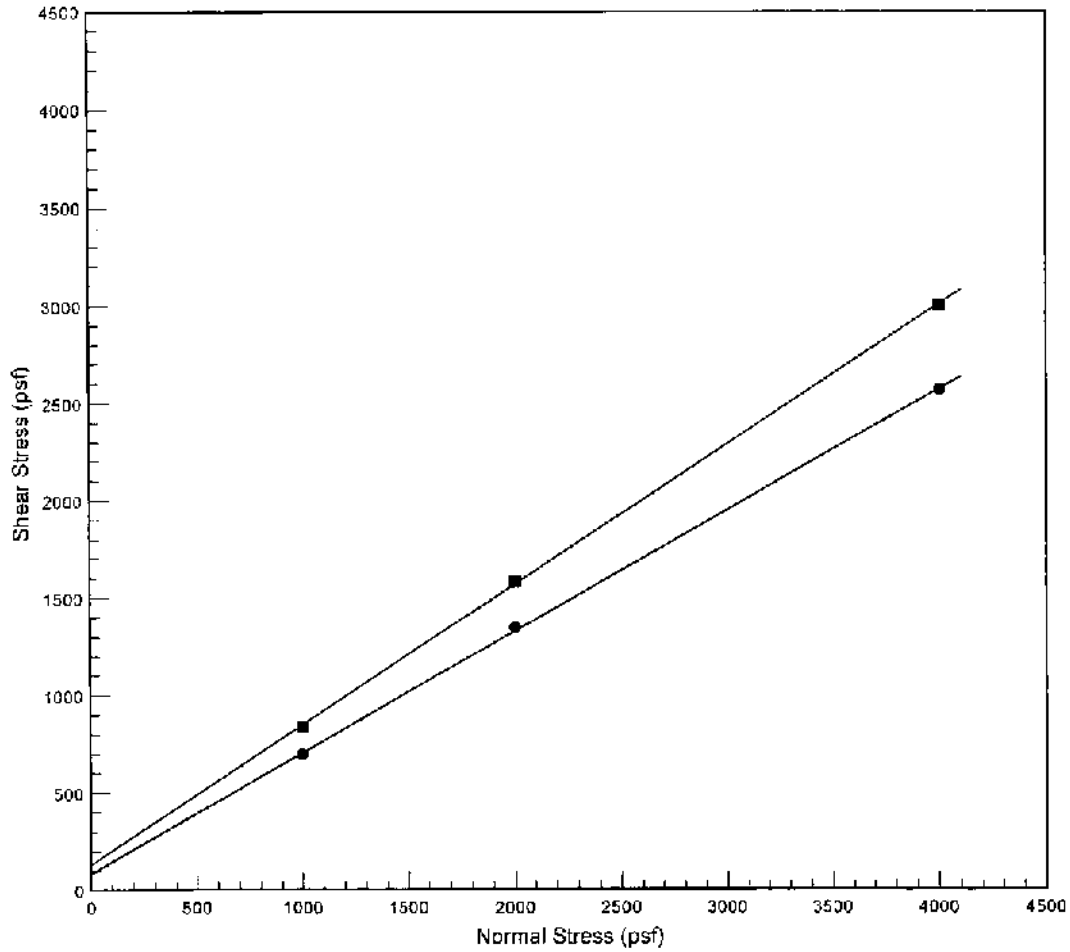
* HCS - Hydroconsolidation strain in percent.



CONSOLIDATION TESTS

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-10

Direct Shear Test (ASTM D 3080)



Boring #	Depth(ft)	Soil/Sample Type	γ_d (pcf)	MC(%)	C (psf)	ϕ (°)
■	8	12 (SM) Silty sand, fine to medium with gravel to 1"	116	6.7	84	32
■	15	15.5 (SP-SM) Sand, fine to medium with coarse, silt and gravel to 1"	112	2.8	132	36

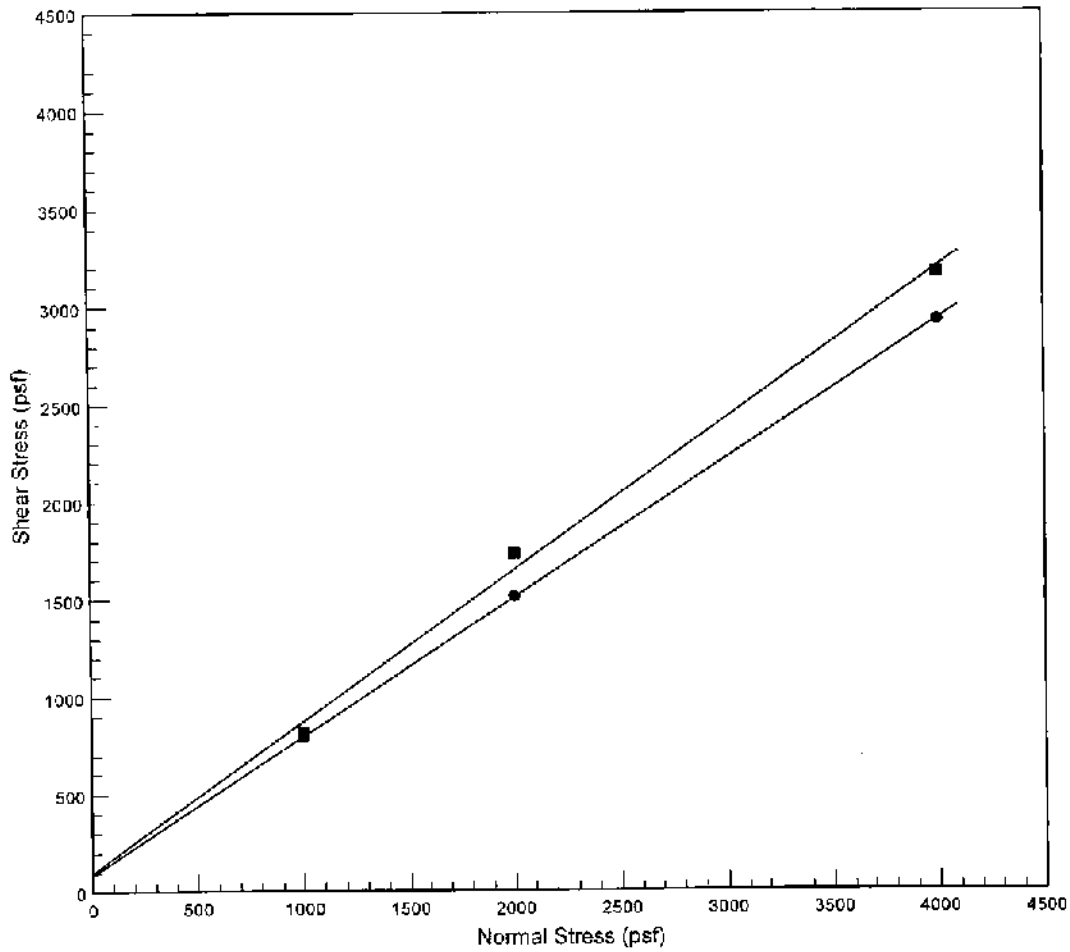


C.H.J. Incorporated

UNDISTURBED DIRECT SHEAR TESTS

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-11

Direct Shear Test (ASTM D 3080)



Boring #	Depth(ft)	Soil/Sample Type	γ_d (pcf)	MC(%)	C (psf)	ψ (°)
2	0	(SM) Silty sand, fine to coarse with gravel to 3/4"	119	9.0	84	35
4	0	(SM) Silty sand, fine to coarse with gravel to 2"	119	8.0	96	38

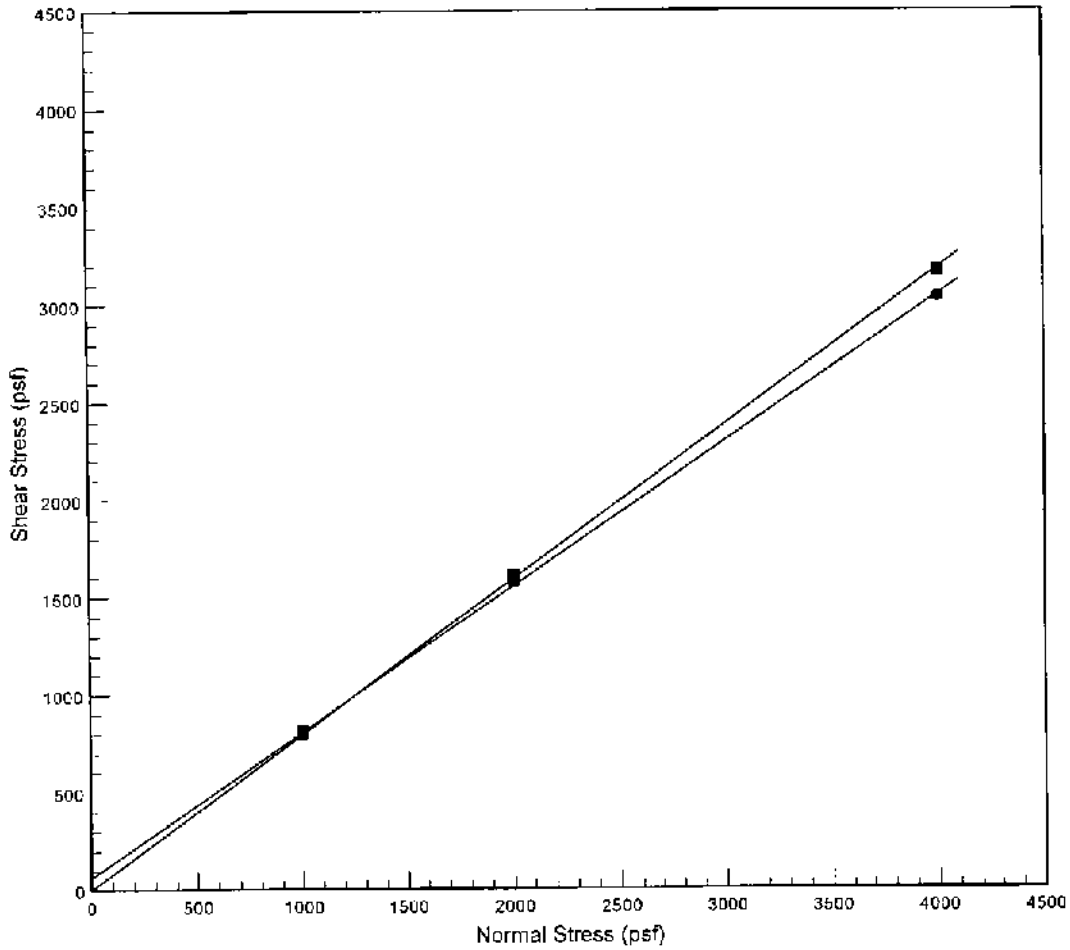


C.H.J. Incorporated

REMOLDED DIRECT SHEAR TESTS

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-12

Direct Shear Test (ASTM D 3080)



Boring #	Depth(ft)	Soil/Sample Type	γ_d (pcf)	MC(%)	C (psf)	ϕ (°)
■ 10	0	(SM) Silty sand, fine to coarse with gravel to 2"	120	8.5	60	37
■ 20	0	(GW) Sandy gravel, fine to coarse with cobbles to 5"	119	6.5	0	38

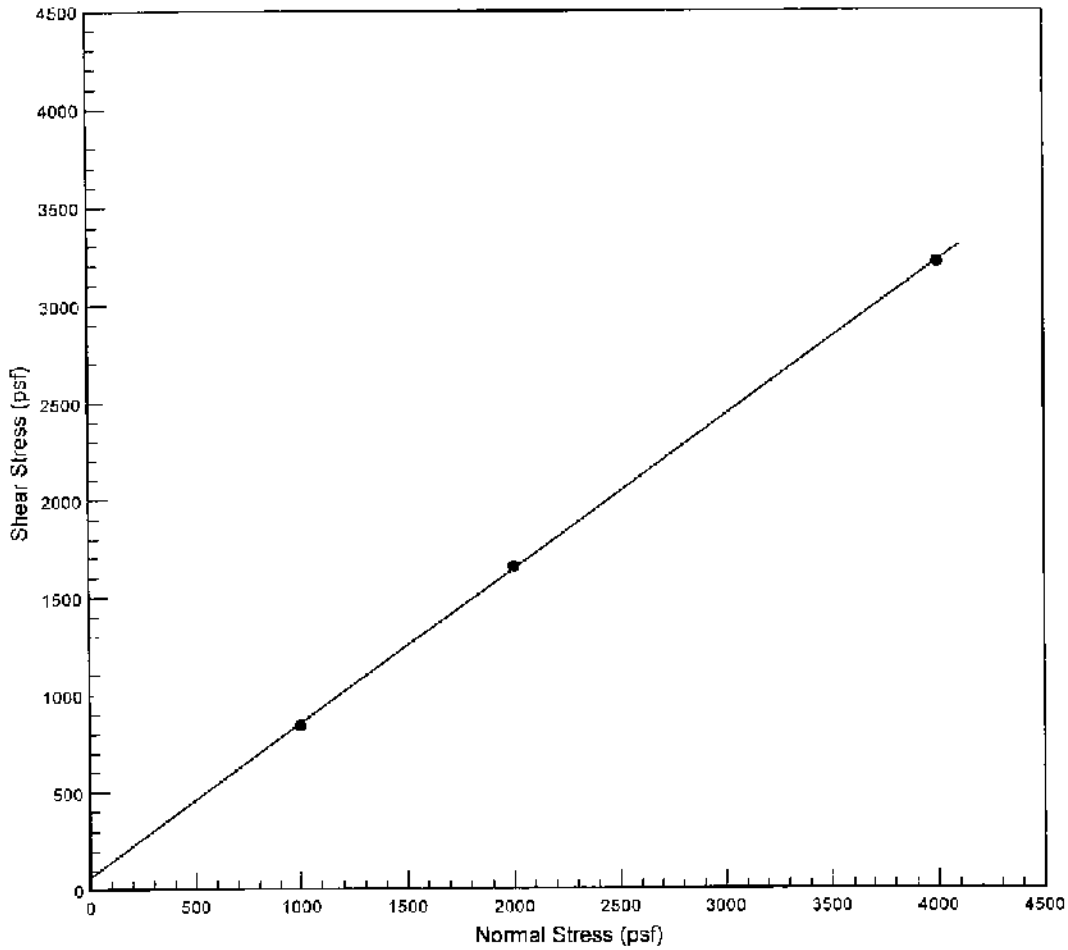


C.H.J. Incorporated

REMOLDED DIRECT SHEAR TESTS

Project:	Tentative Tract Map No. 18140 Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-13

Direct Shear Test (ASTM D 3080)



Boring #	Depth(ft)	Soil/Sample Type	γ_d (pcf)	MC(%)	C (psf)	ϕ (°)
• 23	0	(SM) Silty sand, fine to coarse with gravel to 1"	121	9.0	60	38



C.H.J. Incorporated

REMOLDED DIRECT SHEAR TESTS

Project:	Tentative Tract Map No. 18140, Inland Communities Corp.		
Location:	Badger Canyon Area, San Bernardino, CA		
Job No.:	05894-3	Enclosure:	C-14



Table 1 - Laboratory Tests on Soil Samples

C.H.J., Inc.
Inland Communities
Your #05894-3, MJS&A #06-0489LAB
21-Mar-06

Sample ID

			23A	20A	4A	9A
Resistivity	Units					
as-received	ohm-cm		24,000	180,000	100,000	51,000
saturated	ohm-cm		6,100	5,800	18,000	11,000
pH			7.7	8.1	8.0	8.0
Electrical						
Conductivity	mS/cm		0.05	0.08	0.03	0.03
Chemical Analyses						
Cations						
calcium	Ca ²⁺	mg/kg	36	96	12	16
magnesium	Mg ²⁺	mg/kg	19	78	7	10
sodium	Na ¹⁺	mg/kg	ND	ND	ND	ND
Anions						
carbonate	CO ₃ ²⁻	mg/kg	ND	ND	ND	ND
bicarbonate	HCO ₃ ¹⁻	mg/kg	52	220	52	52
chloride	Cl ¹⁻	mg/kg	ND	ND	ND	ND
sulfate	SO ₄ ²⁻	mg/kg	49	ND	ND	ND
Other Tests						
ammonium	NH ₄ ¹⁺	mg/kg	5.5	5.9	5.4	6.4
nitrate	NO ₃ ¹⁻	mg/kg	2.0	3.5	1.8	8.2
sulfide	S ²⁻	qual	na	na	na	na
Redox		mV	na	na	na	na

Electrical conductivity in millisiemens/cm and chemical analysis were made on a 1:5 soil-to-water extract.

mg/kg = milligrams per kilogram (parts per million) of dry soil.

Redox = oxidation-reduction potential in millivolts

ND = not detected

na = not analyzed

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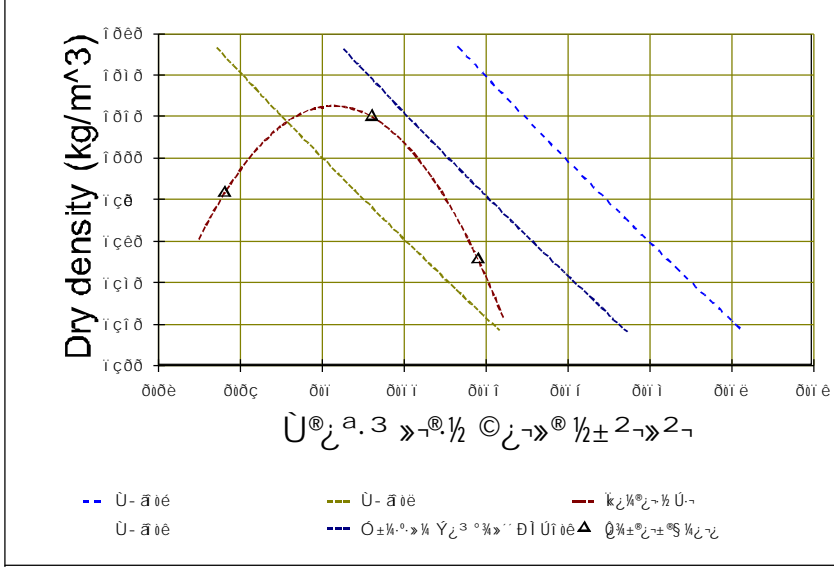
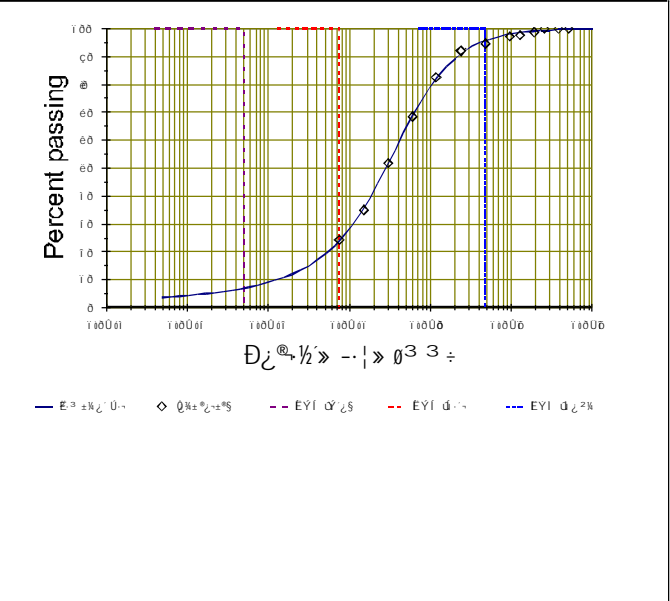
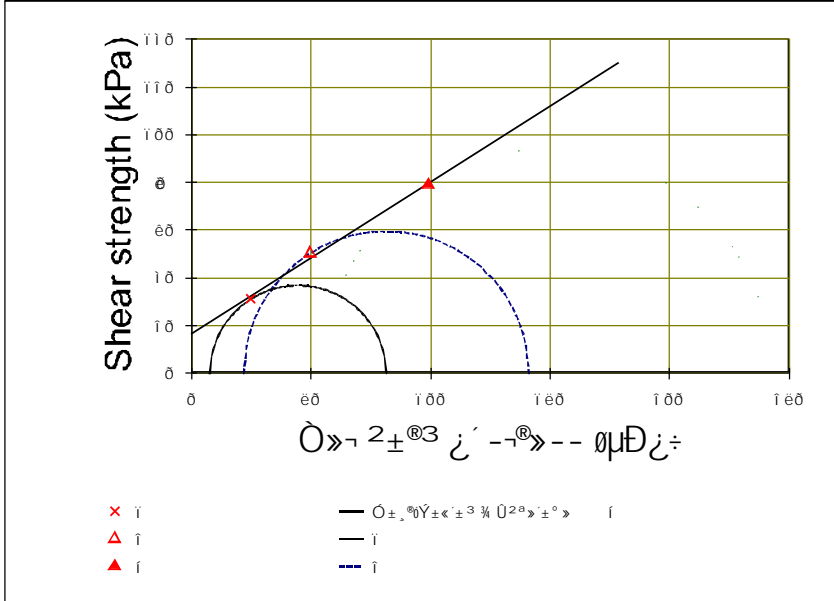
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$\hat{U} \gg \pm \hat{O} \hat{L} \hat{L} \gg \neg \neg 2 1 \hat{Q} \frac{1}{4} \pm \textcircled{R} \hat{L} \neg \pm \textcircled{R} \gg \neg \hat{O} \times 2 1 \hat{L} \hat{O}$

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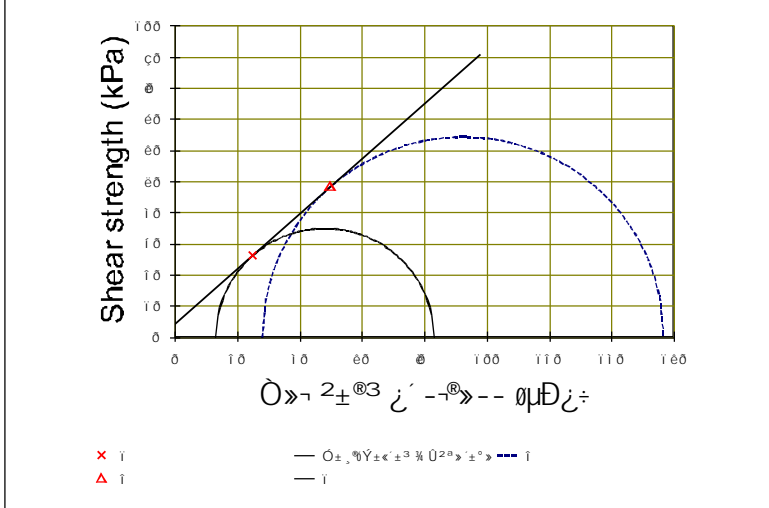
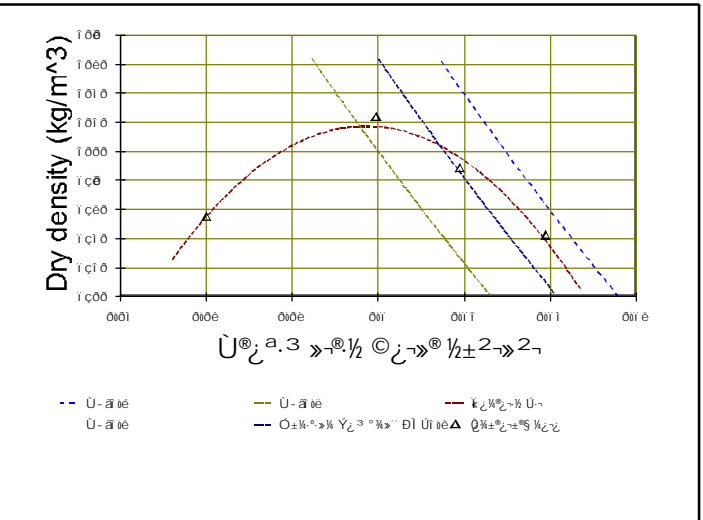
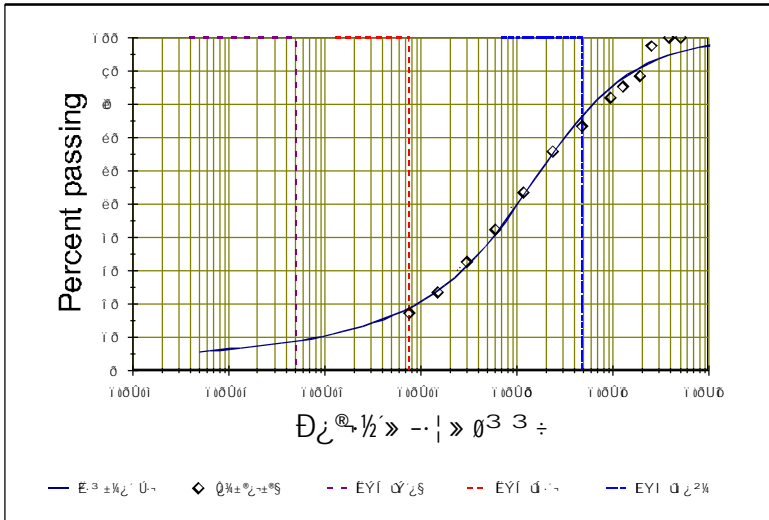
0 ± i i ð 0² » ç ± P oí è ÷

Eí Yí l » « » P « μ Ú - « »
 x² » ç í ç » P « μ Ú - « »
 í ± ú » ½ » ± ² P « μ Ú - « »
 0 ± » - » Y 0 0 x² » ç ½ » ½ » ² - » P oí è ä i ð í 0 ± - « » . 2 P oí è ä é í ú

EI YI D ½ » ² - Y ç §	è è ç ú
Eí Yí D ½ » ² - í ç	ç è ç ú
EI YI D ½ » ² - í ç ² ¼	è é è è ú
EI YI D ½ » ² - Y ç ± ç »	í í è è ú
Ú í ð æ	ð ú ð è è è
Ú í ð æ	ð ú ð ç ð í
Ú í ð æ	ð ú í è í è
Ú è ð æ	í í è è í è
Ú è ð æ	í í è è í è

Í ç « ç ± ²	í í ç í ú
E ± ¼ í ç ±	ð ú è è è
D ± ± - » § æ	í è è ç ú
E ç » Y ± ² » ² æ	è ú ç ú
E ± « ³ » ½ E ç » Y ± ² » ² -	ð ú í í
Ú æ § Ú » ² - » § æ	í í ð í ð ° ½ °
Í ± ç Ú » ² - » § æ	í í ð í ° ½ °
Í ° ½ ° ½ Ú ç a - » § æ	í í è
Ó ç » ½ ° ½ Ú æ § Ú » ² - » §	í í è ç ° ½ °
N ° » ³ « ³ Ó ± - » « »	ç è ú

Í ç ç ± P ± Y ± « ² -	í ° ± ² -
Í » ³ ± ¼ ¼ Í ç ç	ç è ú
B³ » ç ¹ » E ç » Y ± ² » ² - P » ± æ	í ð è ú
B³ » ç ¹ » E ç » Y ± ² » ² - B³ » æ	í è í ú
B³ » ç ¹ » Í ç ç U æ § U » ² - » §	í í ð ð ° ½ °
Ú æ ½ ± ² B² ¹ »	í í è ç
Ú æ ½ ± ² Y ± » - ± ²	è è ° - °



Ú » ± Ó ç í » - » ² ¹ 0 ¼ ± æ ç ± æ » - 0 x ² ½ 0

2»»»®.21 Đ®±°»®.»-

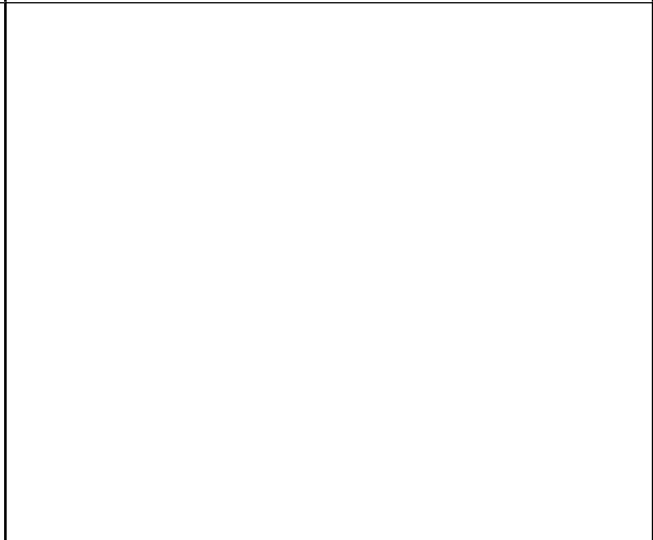
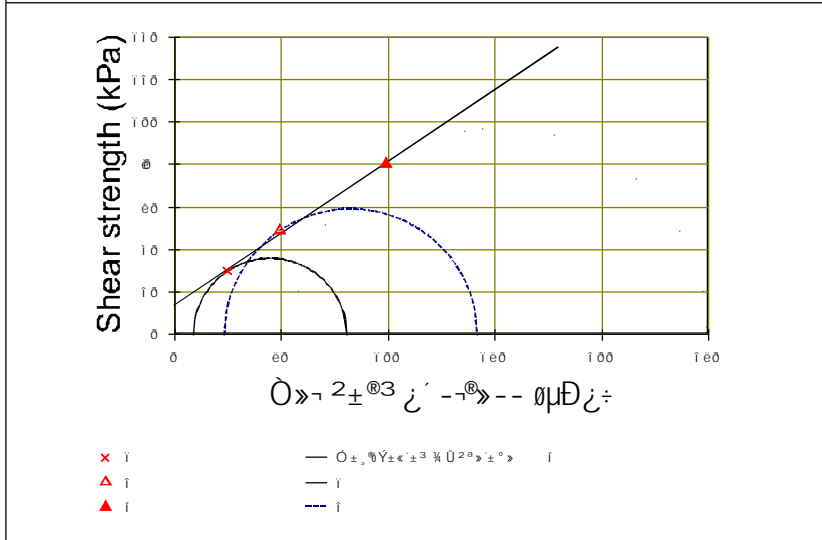
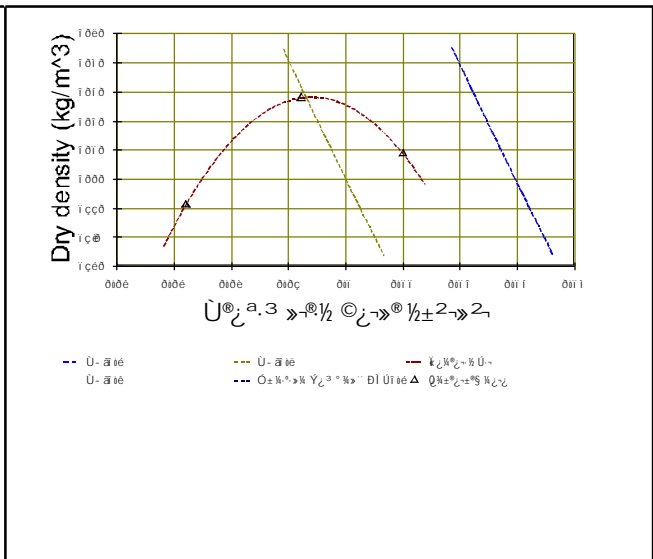
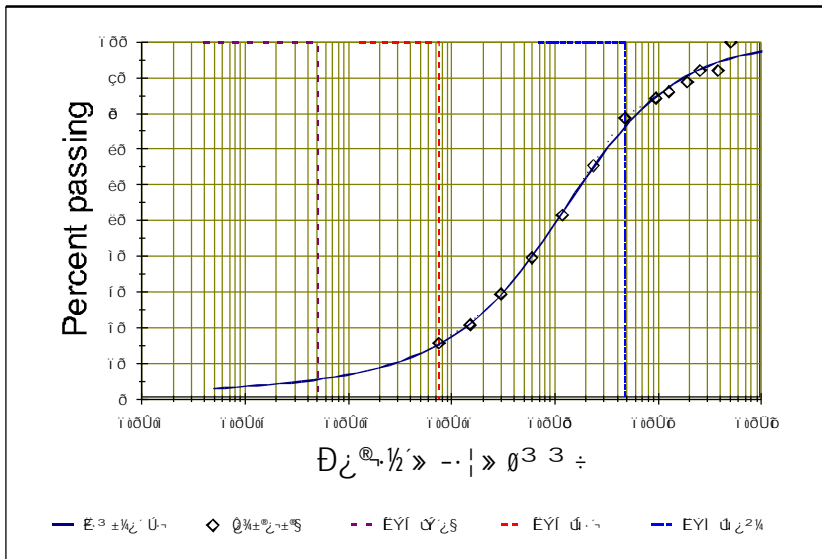
Ô±·iëi 0²»¿® Pôí é÷

EÍYÍ l»«®»» Í·-§-¿²¼0
 x²·¿·Í¿»»» P«µ Ú-«®¼¼
 Í±·Ú»-½® 0±²» Íx0l Ç ÍBOÚ®P®±020°·2» ±½¿®» 1®·2¼¼ 0·¿ 1®·a·
 Ô±»-» Ý00® x²°¿½» ¼®§ ¼»²-·-§·2 Pôí éá íí ði Ô±-«®·2 Pôí éáí ðèÚ

EIYI Đ»½»²·Y¿§	è0í í Ú
EÍYÍ Đ»½»²·Í·¿	ç0èðÚ
EIYI Đ»½»²·Í¿²¼	éí0ð0Ú
EIYI Đ»½»²·Y±¿®»	íí0éí Ú
Úíð®	ð0í í èðç
Úíð®	ð0í í éí í
Úíð®	ð0í í ééí
Úèð®	í0ðí èé
Úèð®	í0èéé

Í¿«®¿²	í é0í ç Ú
É±¼ Í¿±	ð0í ðé
Đ±±-·-§®	í è0èéÚ
É¿»Y±²»²»	í0èééÚ
E±«³»®½ E¿»Y±²»²·	ð0í ðé
Ú®§ Ú»²-·-§®	íí ð0ð °½°
Í±¿ Ú»²-·-§®	íí í0í °½°
Í°½°½ Ú®·a-§®	í0é
0¿··3 «³ Ú®§ Ú»²-·-§	íí è0é °½°
N°·3 «³ Ó±-«®»	ç0í Ú

Í¿®P±·Y±«²·	í °±²·
Í»³¼¼¼ Í¿®	çéÚ
β³»¿¹» E¿»Y±²»²·P»±®»	í0èéÚ
β³»¿¹» E¿»Y±²»²·β³»®»	í é0í Ú
β³»¿¹» Í¿®U®§ Ú»²-·-§	íí ð0ð °½°
Ú®½±² β²¹·»	í í0çp
Ú®½±² Y±»-±²	í çéé °-°



Ú»±Ó¿·l »-¿²¹ 0¼±®¿²±®»-0 x²¼0

Ô±-i éi 0²»¿® Þóé:

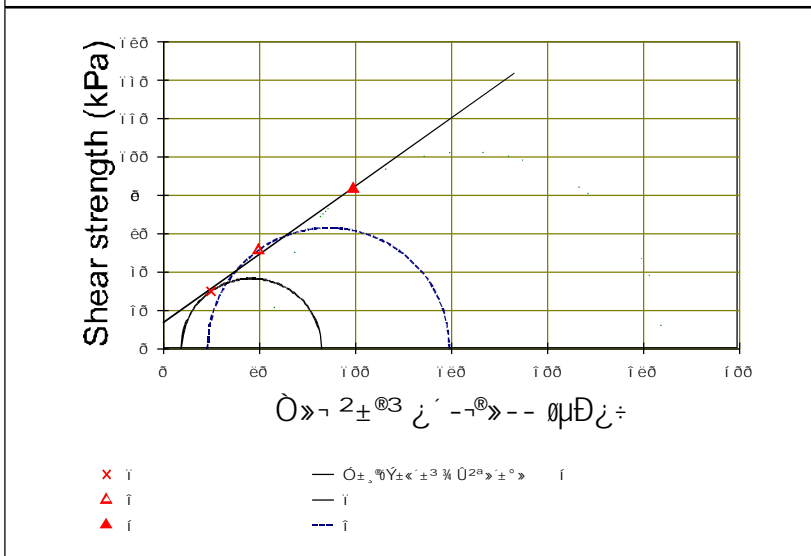
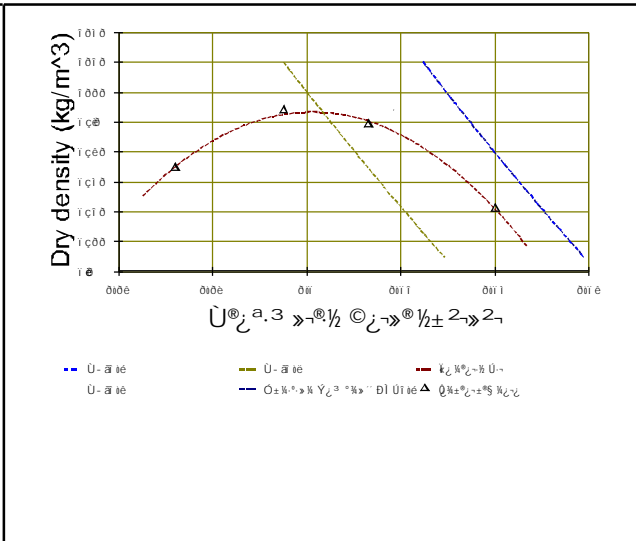
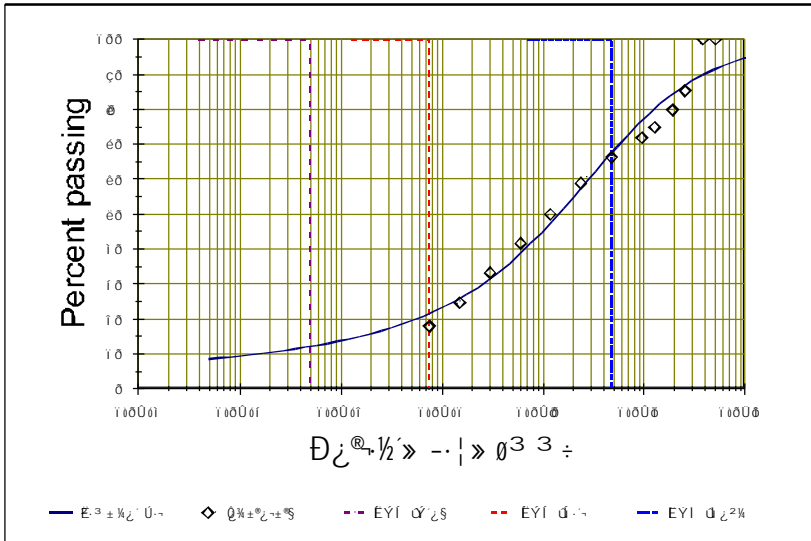
EIYI | »-«®»
 x².¿ ¿-¿»
 I±¿U»-½® ±2
 Ô±-¿»

I¿-¿¿²¼
 Þ«µ Ü-«®½
 Ix0l Ç I ÞOU®Þ±©20.2 » ±½¿® 1®.2»¼ ©.¿ 1®.2»
 Ý00» x²¿½ ¼®§ ¼»²-¿ Þóéá i ðéi Ô±-«®.2 Þóéá i i ò

EIYI Ð»½¿² Y¿§	ÿîïéü
EIYI Ð»½¿² I¿	çüéü
EIYI Ð»½¿² I¿²¼	i éüéü
EIYI Ð»½¿² Y±¿»	i ðüüü
Üíð»	ðüðüéi
Üíð»	ðüðééi
Üíð»	ðüéíí
Üéð»	i ííéçé
Üéð»	i ðéi ççü

I¿«¿²	ÿèïéü
É±¼ I¿±	ðüéíð
Ð±±-¿§»	i ííçü
É¿» Y±¿²»	i ðéüü
E±«³ »½ ¿¿» Y±¿²»	ðüðé
U®§ Ü²-¿§»	ÿííð °½°
I±¿ Ü²-¿§»	ÿííç °½°
I°½.½ Ü¿-¿§»	i ðé
Ö¿.¿ «³ Ü®§ Ü²-¿§»	ÿííð °½°
N°¿³ «³ Ö±-«®»	i ðüðü

I¿¿Þ± Y±¿²	i °±²
I¿±¼¼ I¿¿	çéü
Þ³¿¿¹ E¿» Y±¿²» Þ³¿»	i ðüéü
Þ³¿¿¹ E¿» Y±¿²» Þ³¿»	i éüü
Þ³¿¿¹ I¿¿ U®§ Ü²-¿§»	ÿííð °½°
Ü®½±² Þ²¹»	i éüp
Ü®½±² Y±¿» ±²	i éé °-



Ü»±Ö¿-¿ - ¿²¹ Ö¼±¿¿®» - 0 x 2½0

2 >>> 2.1 D ± ° >>> -

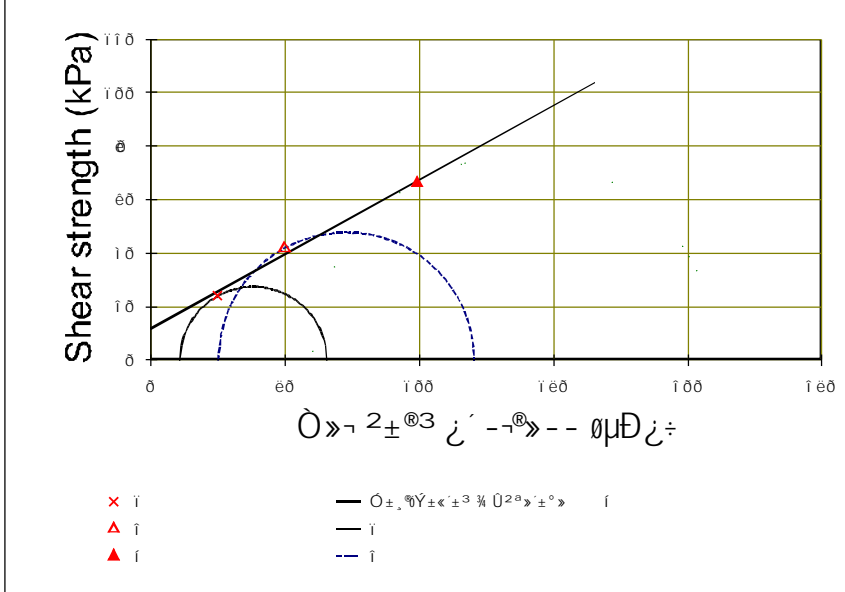
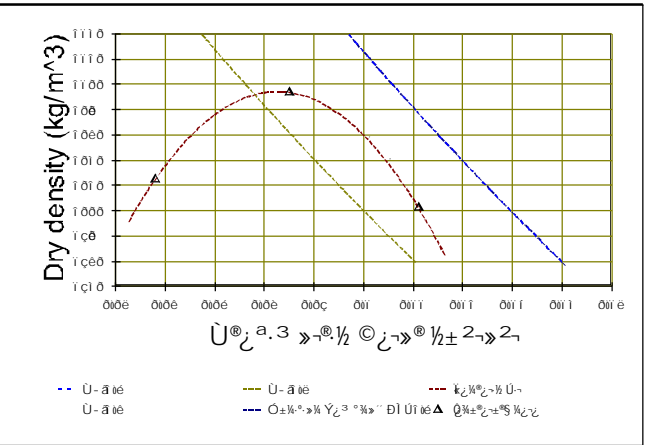
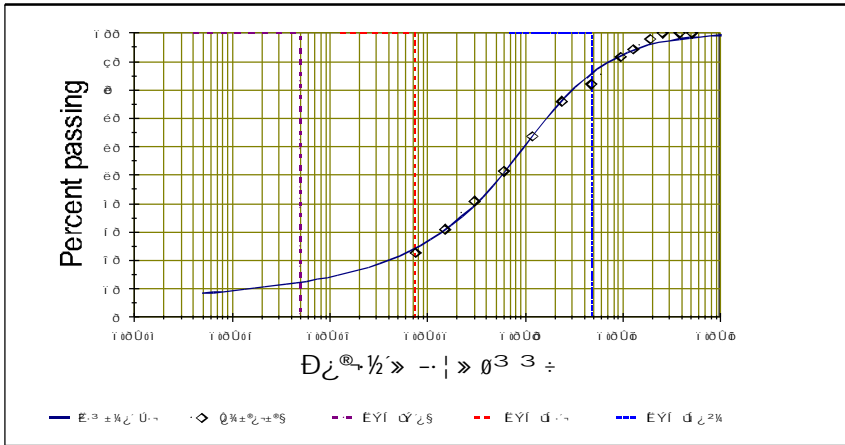
0 ± i ç è 0² >> ç P 0 i ÷

E I Y I | » « » E
x 2 . > ç ' í ç » E P « μ Ü . - « » ¼
í ± ' Ü » ½ ° » ± 2 E í x 0 l Ç í B O Ü E P ± © 2 0 ° . 2 » ± ½ ç » 1 ° . 2 » ¼ © . > 1 ° a »
0 ± » - E Y 0 0 E x 2 ' ç ½ » ¼ » 2 . - . 2 P 0 i ä í í í 0 ± . - « » . 2 P 0 i ä í í 0 0

E I Y I D » ½ » 2 - Y ç §	í í í é ú
E I Y I D » ½ » 2 - í . >	í í í ç í ú
E I Y I D » ½ » 2 - í ç ¼	é í í é ú
E I Y I D » ½ » 2 - Y ç »	í í í é ú
Ü í ð E	ò ú ð í é í
Ü í ð E	ò ú í ç í í
Ü í ð E	ò ú í í é
Ü é ð E	ò ú é é é é
Ü é ð E	ò ú ç é é é í

í ç » ç ½ » 2	í í í é ú
E ± ¼ í ç » ±	ò ú í é í
D ± » - . § E	í é ð è ú
E ç » Y ± 2 » 2 E	í ú í ú
E ± « 3 » ½ E ç » Y ± 2 » 2 -	ò ú ð é
Ü § Ü » 2 - . § E	í í í ð ° ½ °
í ç » Ü » 2 - . § E	í í é é ° ½ °
í ° ½ ° ½ Ü ç » . § E	í í é
O ç » « 3 Ü § Ü » 2 - . §	í í ð é ° ½ °
N ° » 3 « 3 0 ± . - « »	è ú í ú

í ç » ç P ± ' Y ç » 2 -	í ° ± 2 -
í » ± ¼ » ¼ í ç »	ç è ú
B » ç 1 » E ç » Y ± 2 » 2 - P » ± »	í é ú ç ú
B » ç 1 » E ç » Y ± 2 » 2 - B » »	í é ú ú
B » ç 1 » í ç » Ü § Ü » 2 - . §	í í ð í ° ½ °
Ü » ½ » 2 B 2 1 »	í ç ú ð
Ü » ½ » 2 Y ç » - ± 2	í í é ° - °



Ü » ± 0 ç - l » - > 2 1 0 ¾ » ç ç » - 0 x 2 ½ 0

2»»»®.21 Đ®±°»®.»-

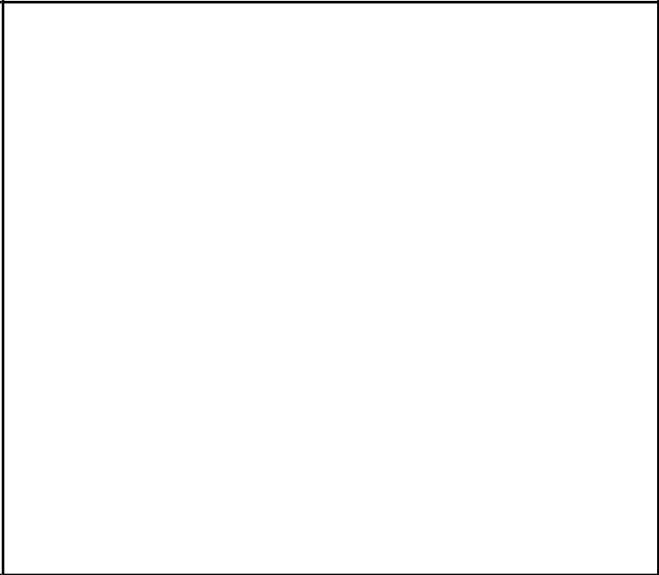
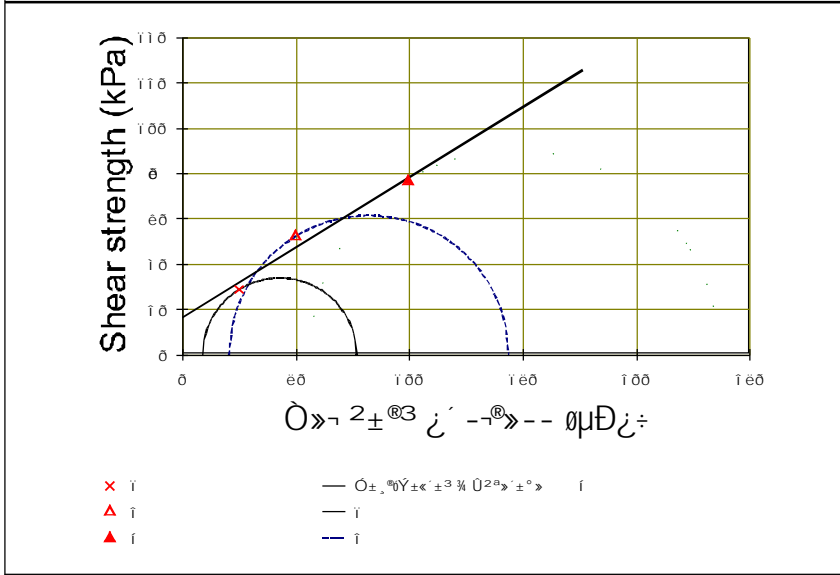
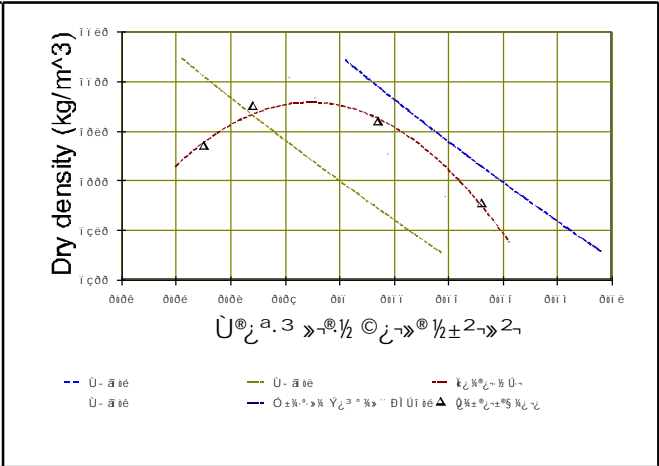
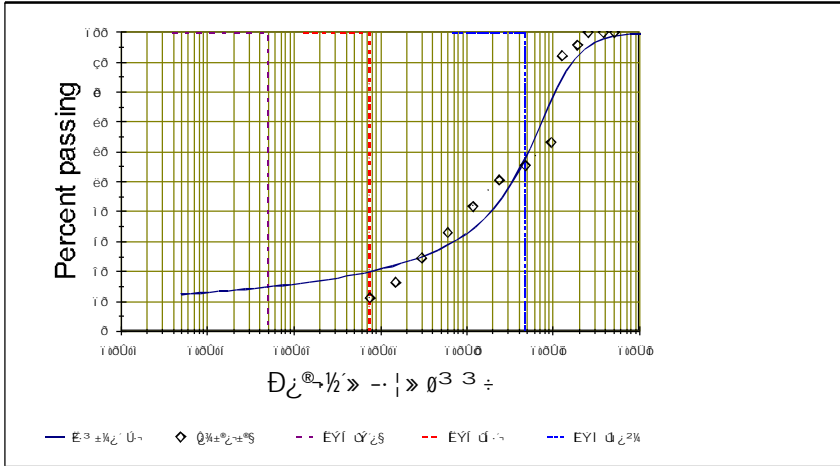
Ô±»ièèø²»¿®Pôitï÷

EÍYÍ l »«®» Đ±±®§ Û®¼»¼ [¿²¼ ©.», [·.¿²¼ Û®¼»
 ×².¿¿¿¿» P«µ Û.®»¼
 [±.Û»½®.±±± Đ±±®§ Û®¼» [¿²¼ ©.», [·.¿²¼ Û®¼» P®±©²º.±±½¿®» 1®.²»¼
 Ô±»-» ÝØØ» ×².¿¿» ¼®§ ¼»².®.² Pôitïã títití Ô±.®.² PôitïáitòÙ

EIYI Đ»½»².Ý¿§	títitòÙ
EÍYÍ Đ»½»².¿	èòitíÙ
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EIYI Đ»½»².Ý±¿®»	títitèèÙ
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[¿®¿²±²	títitèÙ
È±¼ [¿±	òòèití
Đ±®±.®»	títitíçÙ
É¿®Ý±²»²»	títitèèÙ
E±«³»®½ E¿®Ý±²»²»	òòò
Û®§ Û»².®»	títitòº½º
[±¿ Û»².®»	títitíº½º
[º½.º½ Û®¼.®»	títitè
Ó¿.³«³ Û®§ Û»².®»	títitèº½º
Nº.³«³ Ó±.®»	çèèÙ

[¿¿®P±.Ý±«²»	títit±²»
[¿±¼»¼ [¿¿®	çèèÙ
ß³»¿¹» E¿®Ý±²»²»P»±®»	títitèçÙ
ß³»¿¹» E¿®Ý±²»²»ß³»®»	títitèÙ
ß³»¿¹» [¿¿®Û®§ Û»².®»	títitòº½º
Û®½±² ß²¹»	títitèp
Û®»½.ª» Ý±¿»±²	títitèººº



Û»±Ó¿-l »-²¹ Ø¼±¿¿®»-ò ×²½ò

$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$

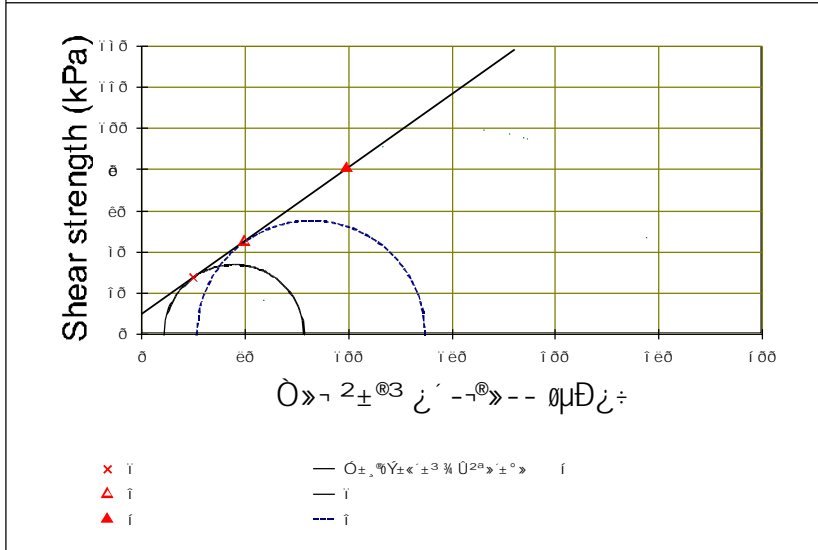
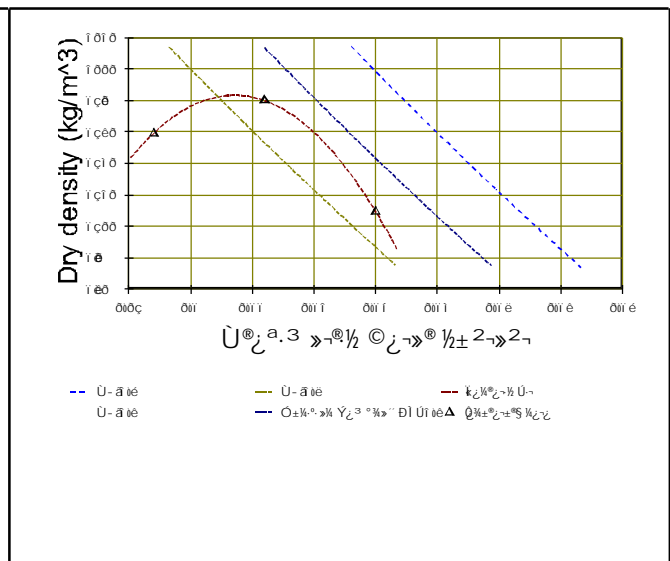
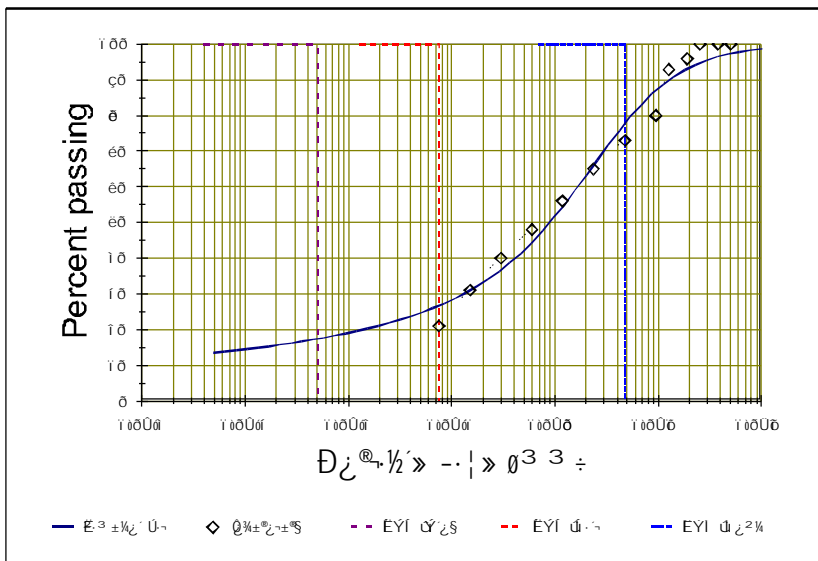
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$

$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$
 $\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$
 $\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$
 $\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$

EIYI	$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í éí éú
EIYI	$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	ç éú
EIYI	$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	é í ú
EIYI	$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í í ú
Üíðæ	$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	òòòòò
Üíðæ	$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	òòííò
Üíðæ	$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	òíííç
Üèðæ	$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	òèçèçí
Üèðæ	$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	íòèèèí

$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í ðèèú
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	òíçç
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í í ú
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í ú
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	òòò
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í í èò °½°
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í í çú °½°
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í è
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í í è °½°
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í ðèú

$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í °±²
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	çèú
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í èú
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í èú
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í èú °½°
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í èúèþ
$\sigma_{p} \approx 1.2 \sigma_{t} \approx 1.2 \times 10^6 \text{ Pa}$	í ðí è °



$U \approx 1.2 U \approx 1.2 \times 10^6 \text{ Pa}$

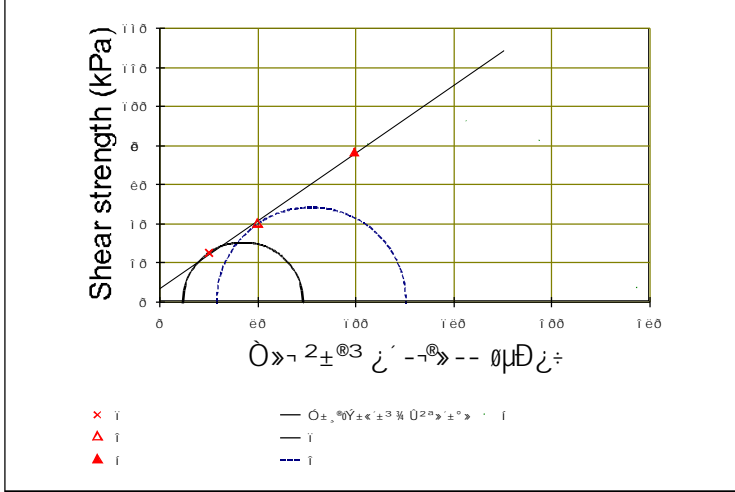
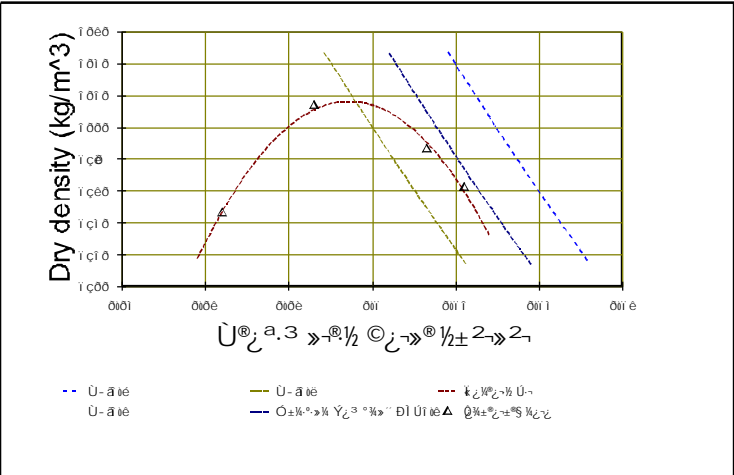
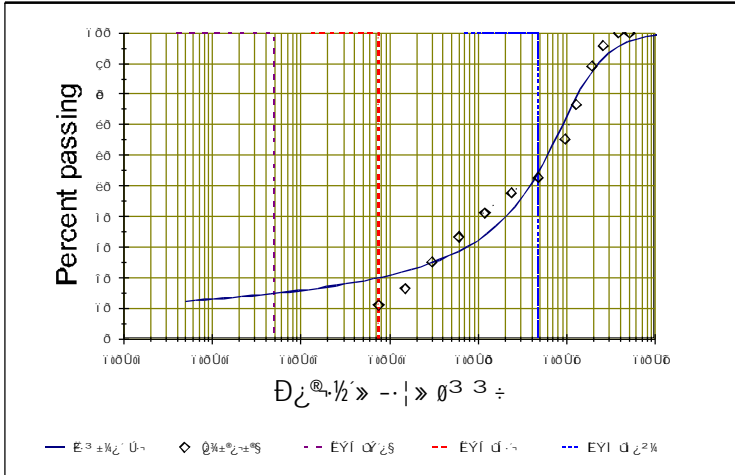
$\hat{1} \pm \dots - P_{\hat{z}} \dots \frac{1}{2} \hat{n} U^{21} . 2 \gg \gg \textcircled{R} . 2 1 \textcircled{D} \textcircled{R} \pm \textcircled{O} \gg \gg \textcircled{R} . \gg -$
 $\textcircled{D} \hat{z} \textcircled{z} \frac{1}{4} \dots \gg \textcircled{O} \dots \textcircled{O} \pm \dots \hat{e} \hat{e} \theta^2 \gg \hat{z} \textcircled{O}$ Póí í ÷

Éí ÝÍ Í » «® » Đ±±® § Û® ¼ »¼ í ¼²¼ ©.º, í .º ¼²¼ Đ »²-§ ±® Û® «ª»
 »².º ¼ í » »® P « µ Û .º «® »¼
 Í ± . Û » ½® ® ± ± ± Đ±±® § Û® ¼ »¼ í ¼²¼ ©.º, í .º ¼²¼ Đ »²-§ ±® Û® «ª» ® P® ± © 2¹ . 2 » ± ½ ± ¼ » 1® . 2 »¼
 Ô± » - ® ÝØÙ » ×² ® ¼ » ¼ » § ¼ »²- »-§ .² Póí í ã í ð ç ï Ö ± - «® .² Póí í ã í ð ç

EIYI Đ»½»²-γ¿§	í ï è è Ù
Eí ÝÍ Đ»½»²-í .º	è ï ï Ù
EIYI Đ»½»²-í ¼²¼	í ï è ð Ù
EIYI Đ»½»²-γ±¿»	ì è ï è Ù
Ûí ð »	ð ï ð ð ð è
Ûí ð »	ð ï ð è ï è ç
Ûí ð »	ð ï è í è í è
Û è ð »	í ï è ð è è ï
Û è ð »	è ÷ ç è í í

Í ¼ »® ¼ - ±²	í ï è ï Ù
È ± ¼ í ¼ - ±	ð ï ï ç ð
Đ ±® ± - »-§ »	í ï è ç Ù
É ¿ »® γ ±² »²- »	ì ï è è Ù
È ± «³ »-® ½ È ¿ »® γ ±² »²- »	ð ï ð è
Û ® § Û »² - »-§ »	í ï ð ç ð ® ¼®
Í ± ¿ Û »² - »-§ »	í ï ï ï ® ¼®
Í ® »½ . ½ Û ® «ª» - »-§ »	í ð è
Ö ¿ .º »³ Û ® § Û »² - »-§ »	í ï è ç ® ¼®
Ñ .º »³ »³ Ö ± - »-«® »	ç ï Ù

Í ¿ »® P ± .º γ ± «² - »	í ° ± ² - »
Í »³ ± ¼ »¼ í ¿ »®	ç è Ù
Bª »¿ ¹ » È ¿ »® γ ±² »²- » P »® ± »	í í è ï Ù
Bª »¿ ¹ » È ¿ »® γ ±² »²- » Bª »®	í ï è Ù
Bª »¿ ¹ » Í ¿ »® Û ® § Û »² - »-§ »	í ï ç è ® ¼®
Û »½ ±² B²¹ »	í ï è ç
Û »³ ¼ »² » γ ± » »-±²	í ï è è ® - °



$\hat{U} \gg \pm \hat{O} \hat{z} \hat{1} \gg \dots \textcircled{R} \hat{1} \textcircled{R} \frac{1}{4} \textcircled{z} \textcircled{z} \textcircled{R} \dots \hat{0} \times \frac{1}{2} \hat{0}$

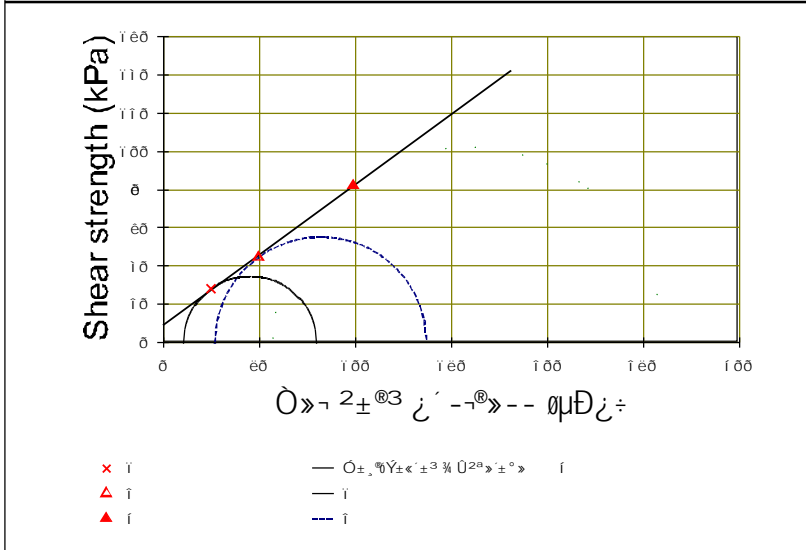
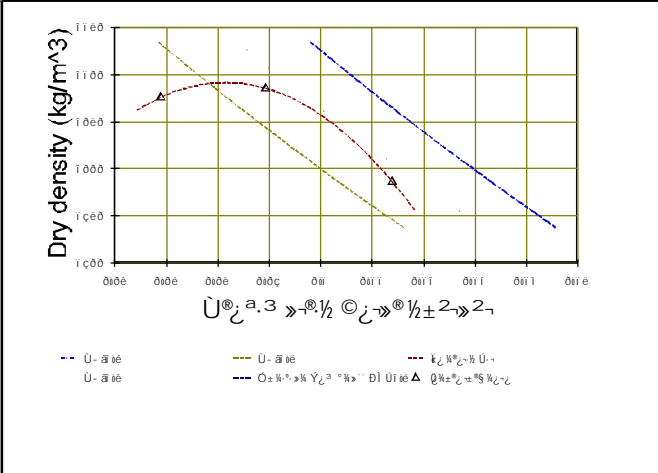
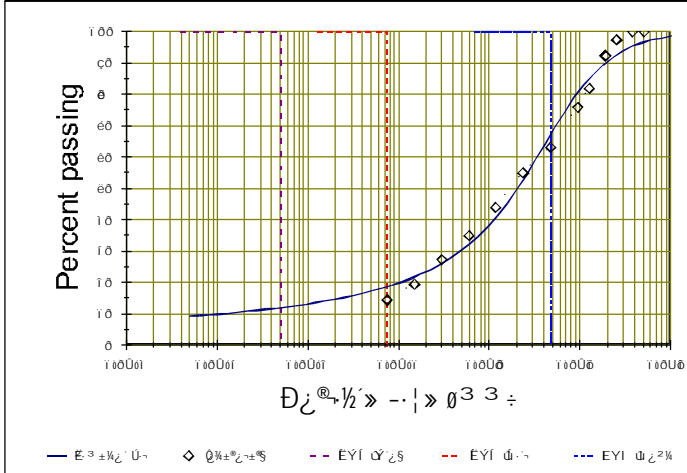
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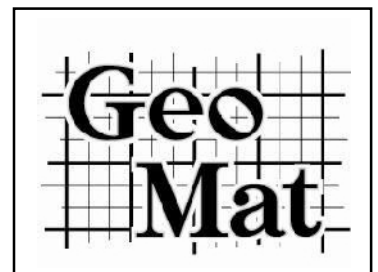
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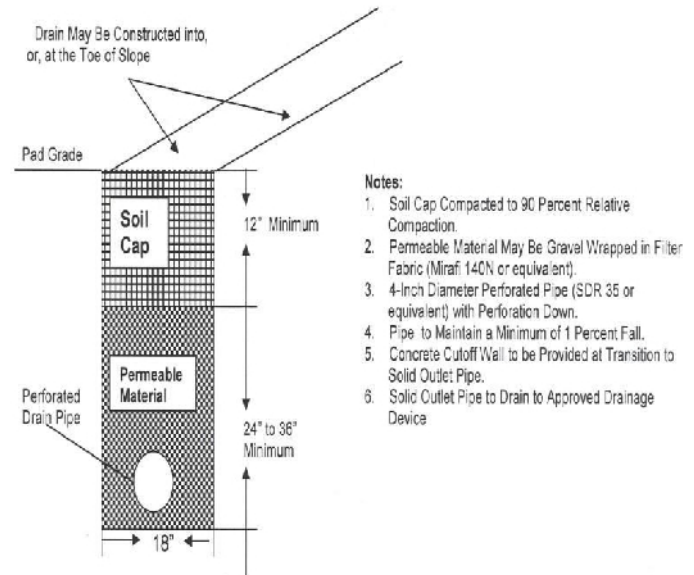
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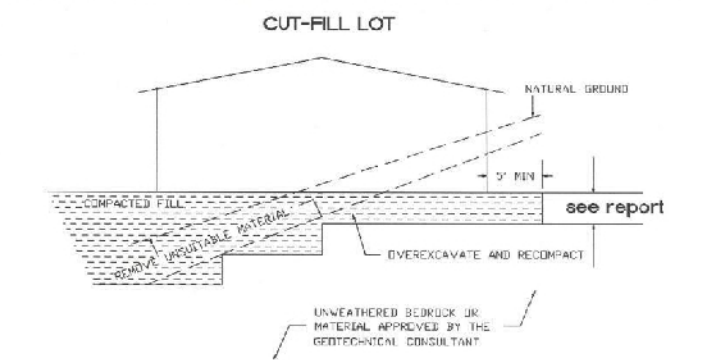
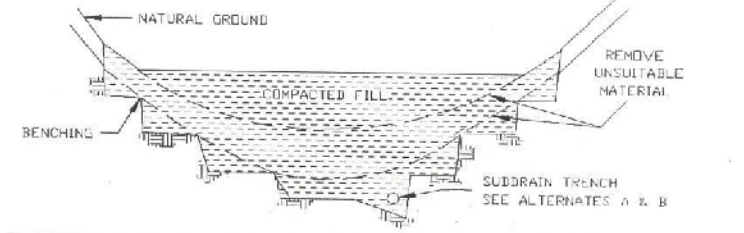
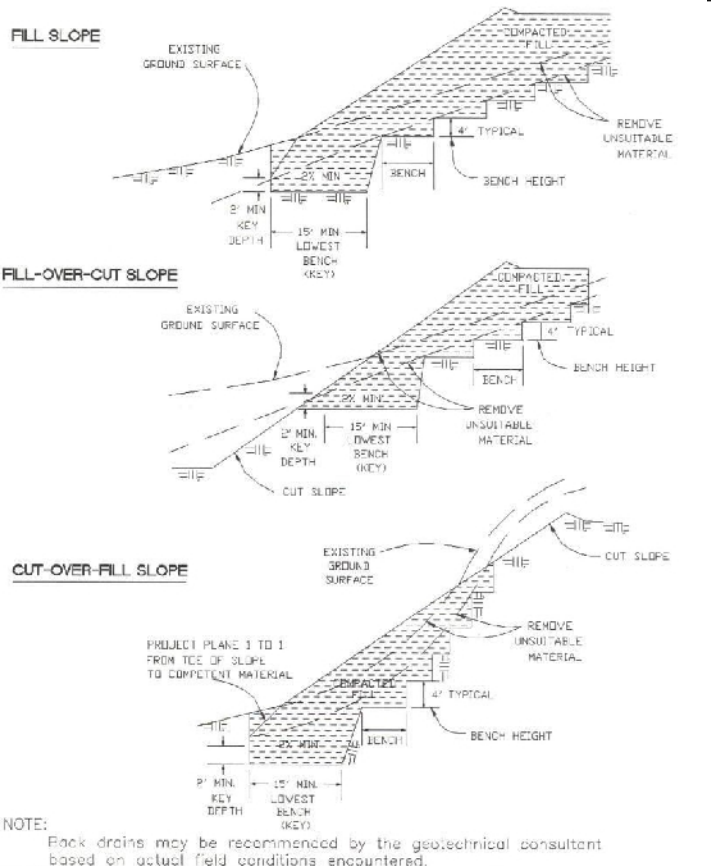
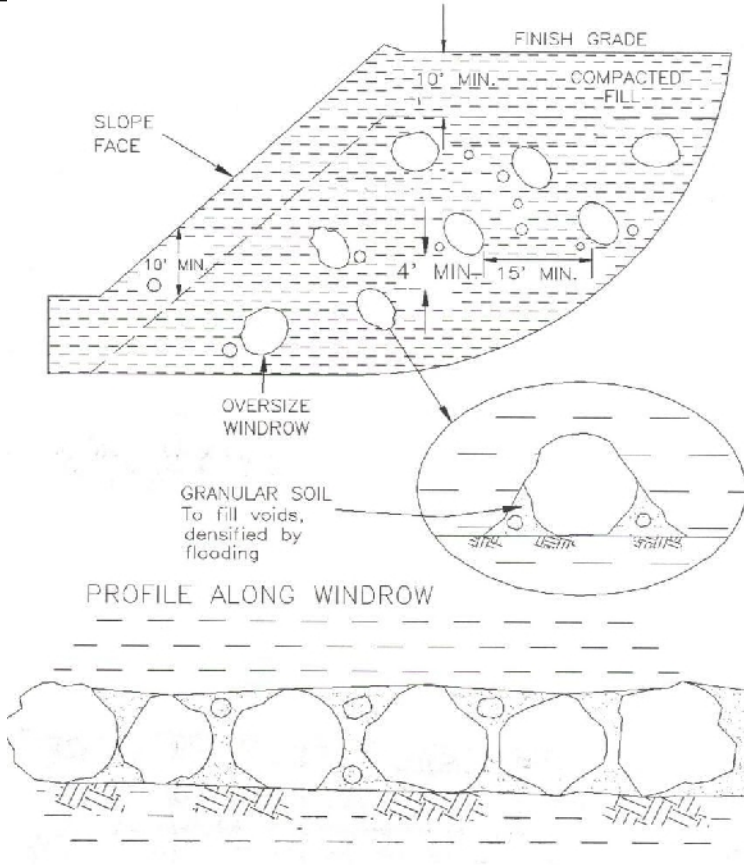
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- Notes: 1. Soil Cap Compacted to 90 Percent Relative Compaction. 2. Permeable Material May Be Gravel Wrapped in Filter Fabric (Mirafix 14CN or equivalent). 3. 4-Inch Diameter Perforated Pipe (SDR 35 or equivalent) with Perforation Down. 4. Pipe to Maintain a Minimum of 1 Percent Fall. 5. Concrete Cutoff Wall to be Provided at Transition to Solid Outlet Pipe. 6. Solid Outlet Pipe to Drain to Approved Drainage Device

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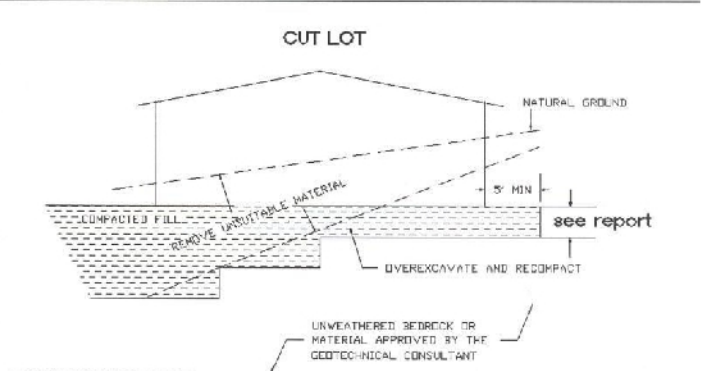
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SUBDRAIN ALTERNATE A-1 Perforated Pipe Surrounded With Filter Material

FILTER MATERIAL
 Filter material shall be Class 2 permeable material per State of California Standard Specifications, or approved alternate.
 Class 2 grading as follows:

SIEVE SIZE	PERCENT PASSING
1"	100
¾"	50 - 100
⅝"	40 - 100
No. 4	25 - 40
No. 8	10 - 33
No. 30	5 - 15
No. 50	0 - 7
No. 200	0 - 3



SUBDRAIN ALTERNATE A-2 1 1/2" Gravel Wrapped in Filter Fabric 6" MIN. OVERLAP

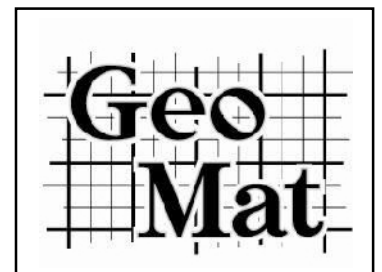
DETAIL OF CANYON SUBDRAIN TERMINAL

* BELOW BOTTOM OF FOOTING.
 NOTES:
 DEEPER OVEREXCAVATION AND RECOMPACTION SHALL BE PERFORMED IF DETERMINED TO BE NECESSARY BY THE GEOTECHNICAL CONSULTANT

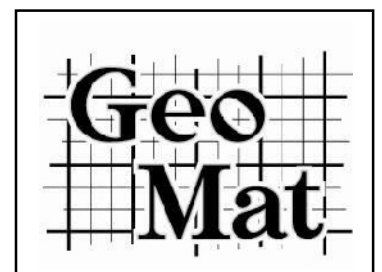
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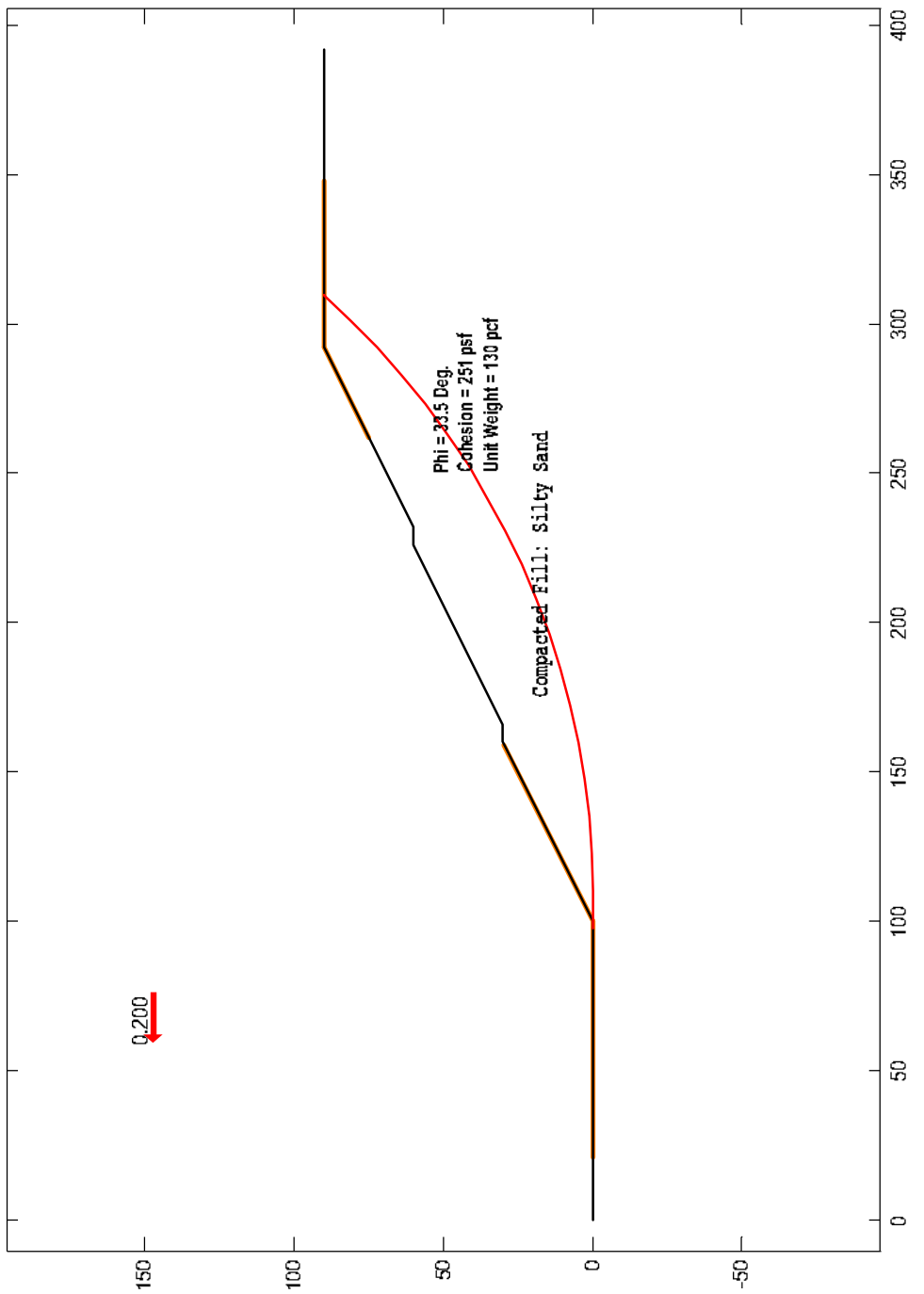


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GALENA Version 5.01

Compacted Fill



Analysis: 1

Multiple Stability Analysis

Method: Bishop Simplified

Surface: Circular

Results

Critical (minimum)

Factor of Safety: 1.22

Edited: 3 Dec 2007 Processed: 3 Dec 2007



Project: University Hills, San Bernardino, California
 85 Feet Compacted Fill Slope

File: C:\Documents and Settings\HP_Administrator\My Documents\GALENA\6003.Fill Slopes.gmf

Licensed to: GeoMat Testing Laboratories, Inc.

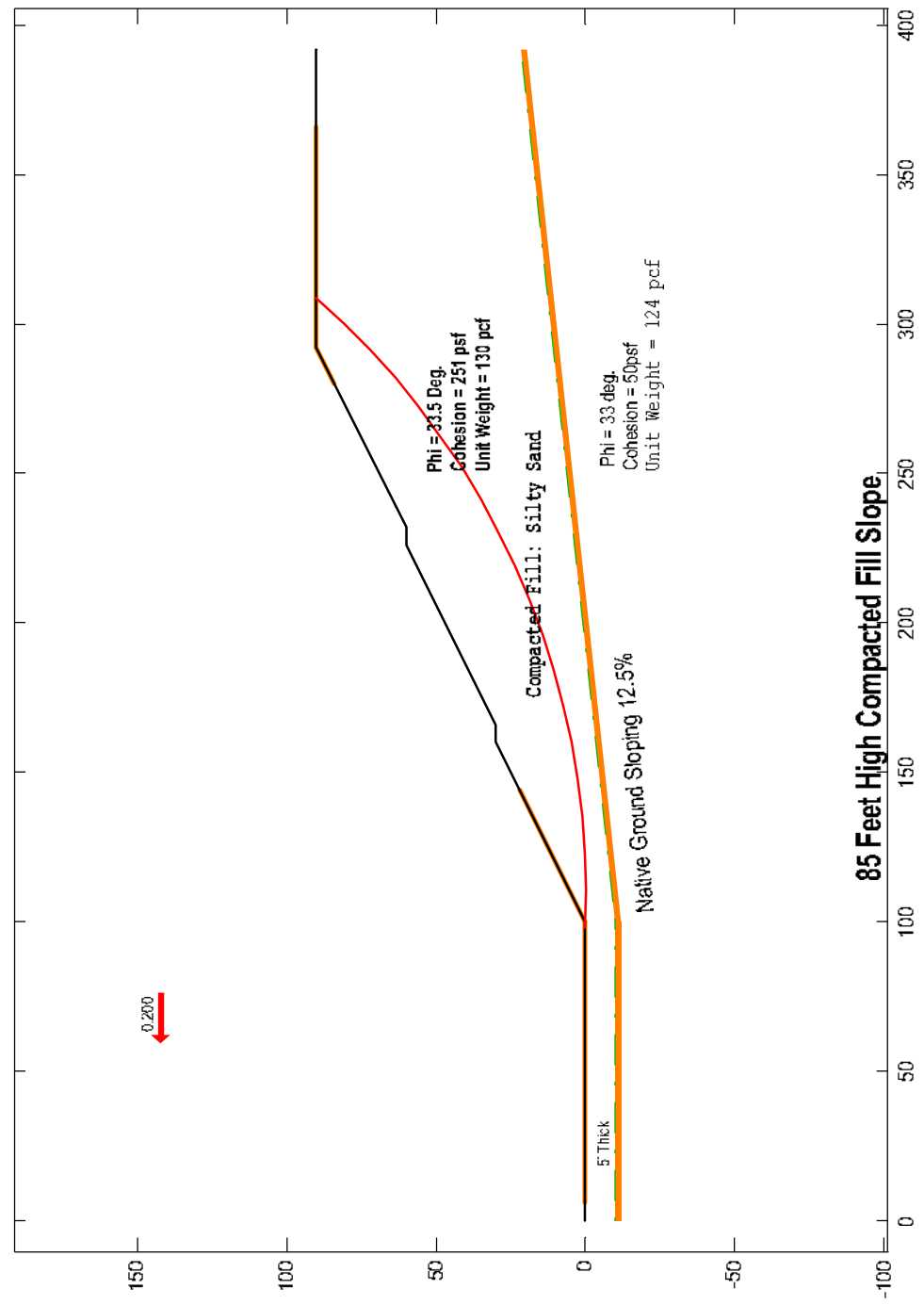
GALENA Version 5.01



Analysis: 2
Multiple Stability Analysis
 Method: Bishop Simplified
 Surface: Circular

Results
 Critical (minimum) Factor of Safety: 1.22

Edited: 3 Dec 2007 Processed: 3 Dec 2007



Project: University Hills, San Bernardino, California
 85 Feet Compacted Fill Slope with Sloping ground

File: C:\Documents and Settings\HP_Administrator\My Documents\GALENA\6003_Fill Slopes.gmf

Licensed to: GeoMat Testing Laboratories, Inc.

Galena 5.01 Analysis Results

Licensee: GeoMat Testing Laboratories, Inc.

Project: University Hills, San Bernardino, California
File: C:\Documents and Settings\HP_Administrator\My Documents\GALENA\6003.Fill Slopes.gmf
Processed: 03 Dec 2007 15:33:05

DATA: Analysis 1 - 85 Feet Compacted Fill Slope

Material Properties (1 material)

Material: 1 (Mohr-Coulomb Isotropic) - Compacted Fill
Cohesion Phi UnitWeight Ru
251.00 33.5 130.00 0.00

Material Profiles (1 profile)

Profile: 1 (2 points) Material beneath: 1 - Compacted Fill
0.00 100.00 395.00 100.00

Slope Surface (8 points)

0.00	0.00	100.00	0.00	160.00	30.00	166.00	30.00	226.00	60.00
232.00	60.00	292.00	90.00	392.00	90.00				

Failure Surface

Initial circular surface for critical search defined by: XL,XR,R

Intersects: XL:	90.00	YL:	0.00	XR:	305.00	YR:	90.00
Centre: XC:	118.26	YC:	234.30	Radius: R:			236.00

Earthquake Force

Pseudo-static earthquake (seismic) coefficient: 0.200

Variable Restraints

Parameter descriptor:	XL	XR	R
Range of variation:	138.00	86.00	69.00
Trial positions within range:	10	10	10

RESULTS: Analysis 1 - 85 Feet Compacted Fill Slope

Bishop Simplified Method of Analysis - Circular Failure Surface

Critical Failure Circle Search using Multiple Circle Generation Techniques

Factor of Safety for initial failure circle approximation: 1.24

There were: 903 successful analyses from a total of 1001 trial circles
98 analyses terminated due to unacceptable geometry

Critical (minimum) Factor of Safety: 1.22

Circle and Results Summary (Lowest 99 Factor of Safety circles)

Circle	X-Centre	Y-Centre	X-Left	Y-Left	X-Right	Y-Right	Radius	FoS
1	108.13	270.30	97.67	0.00	309.78	90.00	270.50	1.221
2	105.62	255.04	97.67	0.00	300.22	90.00	255.17	1.223
3	111.45	262.47	97.67	0.00	309.78	90.00	262.83	1.224
4	109.09	247.24	97.67	0.00	300.22	90.00	247.50	1.225
5	114.79	254.59	97.67	0.00	309.78	90.00	255.17	1.228
6	112.58	239.37	97.67	0.00	300.22	90.00	239.83	1.229
7	114.32	277.00	113.00	6.50	309.78	90.00	270.50	1.232
8	118.16	246.65	97.67	0.00	309.78	90.00	247.50	1.233
9	116.11	231.43	97.67	0.00	300.22	90.00	232.17	1.234
10	117.59	269.29	113.00	6.50	309.78	90.00	262.83	1.234
11	107.28	269.35	82.33	0.00	309.78	90.00	270.50	1.234
12	108.03	269.29	113.00	6.50	300.22	90.00	262.83	1.236
13	98.33	270.03	82.33	0.00	300.22	90.00	270.50	1.236
14	120.88	261.54	113.00	6.50	309.78	90.00	255.17	1.236
15	111.43	261.66	113.00	6.50	300.22	90.00	255.17	1.236
16	104.65	276.87	113.00	6.50	300.22	90.00	270.50	1.236
17	101.59	262.13	82.33	0.00	300.22	90.00	262.83	1.236
18	114.85	253.99	113.00	6.50	300.22	90.00	247.50	1.237
19	110.46	261.32	82.33	0.00	309.78	90.00	262.83	1.237
20	117.23	269.79	97.67	0.00	319.33	90.00	270.50	1.237
21	104.88	254.17	82.33	0.00	300.22	90.00	255.17	1.238
22	118.29	246.27	113.00	6.50	300.22	90.00	239.83	1.239
23	121.56	238.64	97.67	0.00	309.78	90.00	239.83	1.239
24	124.19	253.75	113.00	6.50	309.78	90.00	247.50	1.239
25	119.67	223.42	97.67	0.00	300.22	90.00	224.50	1.239
26	103.87	239.75	97.67	0.00	290.67	89.33	239.83	1.240
27	108.19	246.15	82.33	0.00	300.22	90.00	247.50	1.240
28	118.26	234.30	90.00	0.00	305.00	90.00	236.00	1.241
29	121.76	238.50	113.00	6.50	300.22	90.00	232.17	1.241
30	113.66	253.24	82.33	0.00	309.78	90.00	255.17	1.241

7	128.96	94.45	4.4	6.24	6.26	1	251.00	33.5	12278.02	0.00	1871.92	0.96
8	135.20	109.47	7.1	6.22	6.26	1	251.00	33.5	14231.42	0.00	2121.53	0.94
9	141.42	124.00	7.1	6.22	6.26	1	251.00	33.5	16119.56	0.00	2406.17	0.94
10	147.63	136.63	9.7	6.17	6.26	1	251.00	33.5	17761.34	0.00	2600.42	0.93
11	153.80	149.15	9.7	6.17	6.26	1	251.00	33.5	19389.35	0.00	2841.73	0.93
12	159.98	147.69	12.4	6.02	6.17	1	251.00	33.5	19199.64	0.00	2809.04	0.91
13	166.00	153.69	12.4	6.21	6.36	1	251.00	33.5	19979.78	0.00	2833.53	0.91
14	172.21	159.13	15.0	6.05	6.26	1	251.00	33.5	20687.01	0.00	2937.26	0.90
15	178.26	167.60	15.0	6.05	6.26	1	251.00	33.5	21788.01	0.00	3096.15	0.90
16	184.31	172.74	17.7	5.97	6.26	1	251.00	33.5	22456.04	0.00	3152.83	0.89
17	190.28	179.19	17.7	5.97	6.26	1	251.00	33.5	23294.56	0.00	3272.65	0.89
18	196.25	181.76	20.3	5.87	6.26	1	251.00	33.5	23628.26	0.00	3286.84	0.89
19	202.12	186.22	20.3	5.87	6.26	1	251.00	33.5	24208.16	0.00	3369.06	0.89
20	207.99	186.27	23.0	5.77	6.26	1	251.00	33.5	24214.91	0.00	3343.66	0.88
21	213.76	188.78	23.0	5.77	6.26	1	251.00	33.5	24542.02	0.00	3389.79	0.88
22	219.52	213.96	25.6	6.48	7.19	1	251.00	33.5	27814.49	0.00	3328.52	0.88
23	226.00	153.73	25.6	4.81	5.34	1	251.00	33.5	19984.94	0.00	3215.97	0.88
24	230.81	36.13	28.3	1.19	1.35	1	251.00	33.5	4696.97	0.00	2979.57	0.88
25	232.00	147.88	28.3	4.92	5.59	1	251.00	33.5	19223.76	0.00	2937.92	0.88
26	236.92	146.94	28.3	4.92	5.59	1	251.00	33.5	19102.85	0.00	2918.89	0.88
27	241.84	158.42	31.0	5.37	6.26	1	251.00	33.5	20595.10	0.00	2800.62	0.88
28	247.21	155.55	31.0	5.37	6.26	1	251.00	33.5	20221.01	0.00	2748.07	0.88
29	252.59	147.43	33.6	5.22	6.26	1	251.00	33.5	19165.30	0.00	2600.68	0.88
30	257.80	142.95	33.6	5.22	6.26	1	251.00	33.5	18583.27	0.00	2518.65	0.88
31	263.02	133.25	36.3	5.05	6.26	1	251.00	33.5	17322.79	0.00	2346.42	0.89
32	268.07	127.30	36.3	5.05	6.26	1	251.00	33.5	16548.65	0.00	2236.74	0.89
33	273.12	116.32	38.9	4.87	6.26	1	251.00	33.5	15121.12	0.00	2042.94	0.89
34	277.99	109.02	38.9	4.87	6.26	1	251.00	33.5	14172.45	0.00	1907.52	0.89
35	282.87	94.72	41.6	4.57	6.10	1	251.00	33.5	12313.24	0.00	1697.67	0.90
36	287.43	86.65	41.6	4.57	6.10	1	251.00	33.5	11264.44	0.00	1542.57	0.90
37	292.00	73.11	44.1	4.61	6.41	1	251.00	33.5	9503.86	0.00	1222.00	0.91
38	296.61	52.45	44.2	4.61	6.43	1	251.00	33.5	6818.42	0.00	837.89	0.91
39	301.21	29.36	46.9	4.28	6.26	1	251.00	33.5	3816.34	0.00	425.60	0.93
40	305.50	9.79	46.9	4.28	6.26	1	251.00	33.5	1272.10	0.00	49.19	0.93

 X-S Area: 4679.84 Path Length: 238.00 X-S Weight: 608379.50

DATA: Analysis 2 - 85 Feet Compacted Fill Slope with Sloping ground

Material Properties (2 materials)

Material: 1 (Mohr-Coulomb Isotropic) - Compacted Fill
Cohesion Phi UnitWeight Ru
251.00 33.5 130.00 0.00
Material: 2 (Mohr-Coulomb Isotropic) - Native Ground
Cohesion Phi UnitWeight Ru
50.00 33.0 124.00 0.00

Material Profiles (2 profiles)

Profile: 1 (2 points) Material beneath: 1 - Compacted Fill
0.00 100.00 395.00 100.00
Profile: 2 (3 points) Material beneath: 2 - Native Ground
0.00 -10.00 100.00 -10.00 392.00 21.50

Slope Surface (3 points)

0.00 0.00 100.00 0.00 160.00 30.00 166.00 30.00 226.00 60.00
232.00 60.00 292.00 90.00 392.00 90.00

Failure Surface

 Initial circular surface for critical search defined by: XL, XR, R
 Intersects: XL: 75.00 YL: 0.00 XR: 323.00 YR: 90.00
 Centre: XC: 134.31 YC: 223.26 Radius: R: 231.00

Earthquake Force

 Pseudo-static earthquake (seismic) coefficient: 0.200

Variable Restraints

Parameter descriptor:	XL	XR	R
Range of variation:	138.00	86.00	69.00
Trial positions within range:	10	10	10

RESULTS: Analysis 2 - 85 Feet Compacted Fill Slope with Sloping ground

Bishop Simplified Method of Analysis - Circular Failure Surface

 Critical Failure Circle Search using Multiple Circle Generation Techniques

Factor of Safety for initial failure circle approximation: 1.27

There were: 987 successful analyses from a total of 1001 trial circles
 14 analyses terminated due to unacceptable geometry

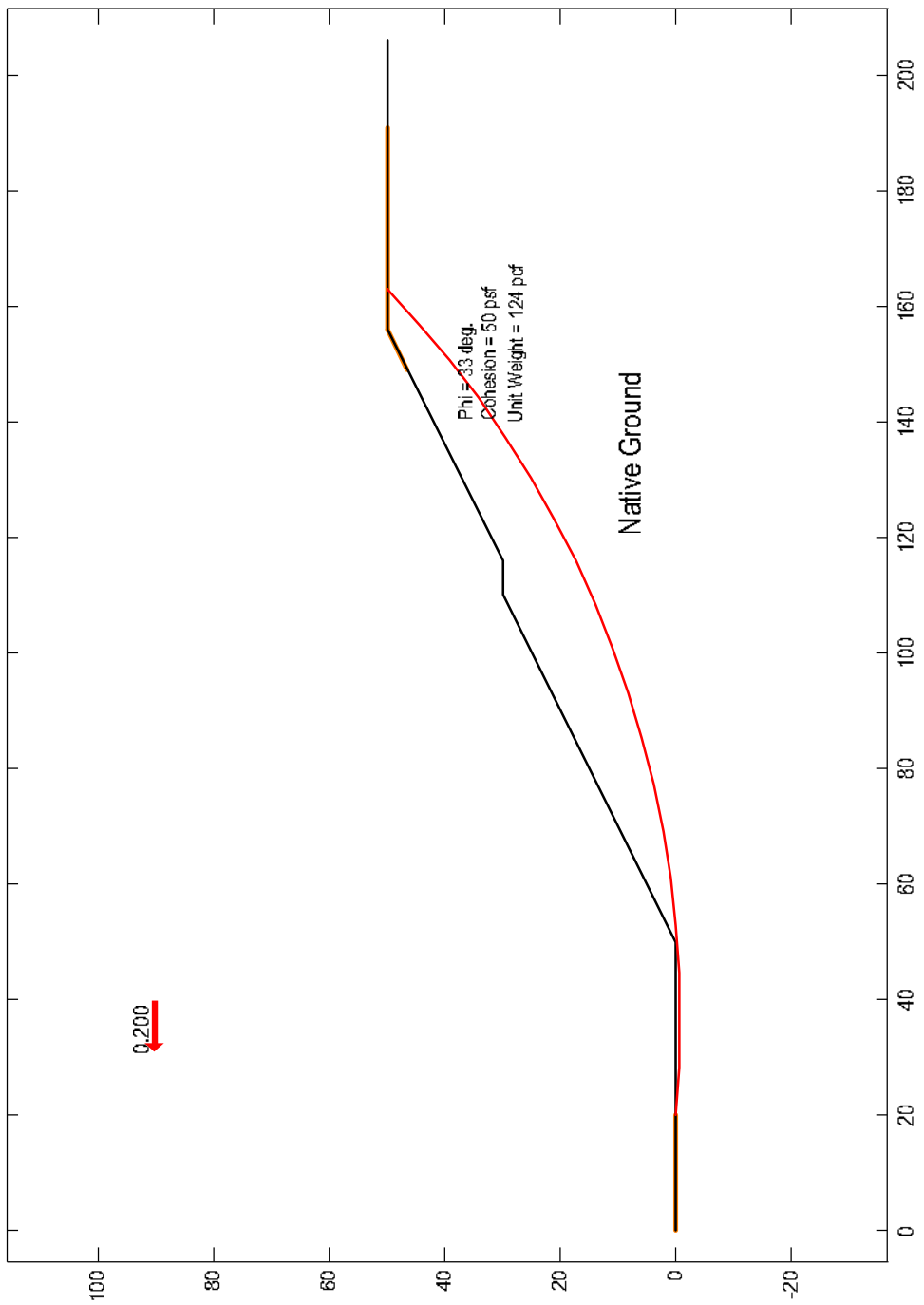
GALENA Version 5.01

Native Material

Analysis: 1
Multiple Stability Analysis
 Method: Bishop Simplified
 Surface: Circular

Results
 Critical (minimum)
 Factor of Safety: 1.11

Edited: 3 Dec 2007 Processed: 3 Dec 2007



Project: 50 Feet Cut Slope
 50 Feet Cut Slope

File: C:\Documents and Settings\HP_Administrator\My Documents\GALENA\6003.50 Cut Slope.gmf

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Galena 5.01 Analysis Results

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Project: 50 Feet Cut Slope
 File: C:\Documents and Settings\HP_Administrator\My Documents\GALENA\6003.50 Cut Slope.gmf
 Processed: 03 Dec 2007 13:53:56

DATA: Analysis 1 - 50 Feet Cut Slope

Material Properties (1 material)

Material: 1 (Mohr-Coulomb Isotropic) - Native Material
 Cohesion Phi UnitWeight Ru
 60.00 33.0 124.00 0.00

Material Profiles (1 profile)

Profile: 1 (2 points) Material beneath: 1 - Native Material
 0.00 80.00 206.00 80.00

Slope Surface (6 points)

0.00	0.00	50.00	0.00	110.00	30.00	116.00	30.00	156.00	50.00
206.00	50.00								

Failure Surface

Initial circular surface for critical search defined by: XL, XR, R
 Intersects: XL: 20.00 YL: 0.00 XR: 163.00 YR: 50.00
 Centre: XC: 36.42 YC: 182.54 Radius: R: 183.28

Earthquake Force

Pseudo-static earthquake (seismic) coefficient: 0.200

Variable Restraints

Parameter descriptor:	XL	XR	R
Range of variation:	20.00	42.00	29.00
Trial positions within range:	10	10	10

RESULTS: Analysis 1 - 50 Feet Cut Slope

Bishop Simplified Method of Analysis - Circular Failure Surface

Critical Failure Circle Search using Multiple Circle Generation Techniques

Factor of Safety for initial failure circle approximation: 1.18

There were: 90% successful analyses from a total of 1001 trial circles
 95 analyses terminated due to unacceptable geometry

Critical (minimum) Factor of Safety: 1.11

Circle and Results Summary (Lowest 99 Factor of Safety circles)

Circle	X-Centre	Y-Centre	X-Left	Y-Left	X-Right	Y-Right	Radius	FoS
1	36.42	182.54	20.00	0.00	163.00	50.00	183.28	1.112
2	37.59	179.19	20.00	0.00	163.00	50.00	180.06	1.114
3	35.06	185.70	17.78	0.00	163.00	50.00	186.50	1.115
4	38.76	175.84	20.00	0.00	163.00	50.00	176.83	1.116
5	36.21	182.35	17.78	0.00	163.00	50.00	183.28	1.118
6	35.71	172.90	20.00	0.00	158.33	50.00	173.61	1.118
7	39.94	172.46	20.00	0.00	163.00	50.00	173.61	1.119
8	37.37	178.99	17.78	0.00	163.00	50.00	180.06	1.120
9	36.92	169.55	20.00	0.00	158.33	50.00	170.39	1.120
10	39.50	185.48	20.00	0.00	167.67	50.00	186.50	1.120
11	41.12	169.07	20.00	0.00	163.00	50.00	170.39	1.121
12	34.85	185.50	15.56	0.00	163.00	50.00	186.50	1.122
13	38.14	166.18	20.00	0.00	158.33	50.00	167.17	1.122
14	38.53	175.61	17.78	0.00	163.00	50.00	176.83	1.122
15	40.63	182.11	20.00	0.00	167.67	50.00	183.28	1.123
16	34.32	176.06	17.78	0.00	158.33	50.00	176.83	1.123
17	35.99	182.13	15.56	0.00	163.00	50.00	183.28	1.124
18	39.36	162.80	20.00	0.00	158.33	50.00	163.94	1.125
19	42.31	165.67	20.00	0.00	163.00	50.00	167.17	1.125
20	35.51	172.70	17.78	0.00	158.33	50.00	173.61	1.125
21	39.70	172.22	17.78	0.00	163.00	50.00	173.61	1.125
22	41.78	178.73	20.00	0.00	167.67	50.00	180.06	1.125
23	39.26	185.26	17.78	0.00	167.67	50.00	186.50	1.126
24	37.14	178.76	15.56	0.00	163.00	50.00	180.06	1.127
25	36.71	169.33	17.78	0.00	158.33	50.00	170.39	1.127
26	40.59	159.40	20.00	0.00	158.33	50.00	160.72	1.127
27	43.51	162.25	20.00	0.00	163.00	50.00	163.94	1.128
28	42.93	175.34	20.00	0.00	167.67	50.00	176.83	1.128
29	40.39	181.88	17.78	0.00	167.67	50.00	183.28	1.128
30	40.87	168.82	17.78	0.00	163.00	50.00	170.39	1.128

7	44.63	1.24	3.9	2.68	2.69	1	60.00	33.0	153.67	0.00	51.61	0.96
8	47.32	0.75	3.9	2.68	2.69	1	60.00	33.0	93.52	0.00	30.04	0.96
9	50.00	2.28	3.9	2.83	2.84	1	60.00	33.0	282.47	0.00	92.39	0.96
10	52.83	9.02	6.4	4.08	4.11	1	60.00	33.0	1117.97	0.00	251.17	0.94
11	56.92	15.48	6.4	4.08	4.11	1	60.00	33.0	1919.05	0.00	435.23	0.94
12	61.00	21.41	9.0	4.06	4.11	1	60.00	33.0	2654.59	0.00	590.84	0.93
13	65.06	27.04	9.0	4.06	4.11	1	60.00	33.0	3352.69	0.00	748.27	0.93
14	69.12	32.00	11.6	4.03	4.11	1	60.00	33.0	3968.60	0.00	870.62	0.91
15	73.15	36.79	11.6	4.03	4.11	1	60.00	33.0	4562.31	0.00	1002.35	0.91
16	77.17	40.76	14.1	3.99	4.11	1	60.00	33.0	5054.09	0.00	1093.77	0.90
17	81.16	44.70	14.1	3.99	4.11	1	60.00	33.0	5542.84	0.00	1200.69	0.90
18	85.14	47.65	16.7	3.94	4.11	1	60.00	33.0	5908.12	0.00	1263.36	0.89
19	89.08	50.74	16.7	3.94	4.11	1	60.00	33.0	6292.21	0.00	1346.39	0.89
20	93.01	52.67	19.3	3.88	4.11	1	60.00	33.0	6530.78	0.00	1382.32	0.88
21	96.89	54.93	19.3	3.88	4.11	1	60.00	33.0	6811.32	0.00	1442.37	0.88
22	100.77	55.85	21.8	3.81	4.11	1	60.00	33.0	6925.09	0.00	1453.50	0.87
23	104.59	57.29	21.8	3.81	4.11	1	60.00	33.0	7104.03	0.00	1491.51	0.87
24	108.40	24.38	24.4	1.60	1.76	1	60.00	33.0	3023.64	0.00	1474.88	0.87
25	110.00	43.00	24.4	2.94	3.23	1	60.00	33.0	5332.17	0.00	1413.05	0.87
26	112.94	39.07	24.4	2.94	3.23	1	60.00	33.0	4844.94	0.00	1282.16	0.87
27	115.88	45.91	27.0	3.66	4.11	1	60.00	33.0	5693.24	0.00	1177.05	0.86
28	119.55	45.79	27.0	3.66	4.11	1	60.00	33.0	5678.10	0.00	1173.86	0.86
29	123.21	44.21	29.6	3.57	4.11	1	60.00	33.0	5482.36	0.00	1129.03	0.86
30	126.78	43.36	29.6	3.57	4.11	1	60.00	33.0	5376.29	0.00	1106.74	0.86
31	130.36	41.02	32.1	3.48	4.11	1	60.00	33.0	5086.63	0.00	1044.52	0.86
32	133.84	39.47	32.1	3.48	4.11	1	60.00	33.0	4894.68	0.00	1004.17	0.86
33	137.32	36.47	34.7	3.38	4.11	1	60.00	33.0	4522.79	0.00	926.50	0.87
34	140.70	34.28	34.7	3.38	4.11	1	60.00	33.0	4250.71	0.00	869.17	0.87
35	144.08	30.73	37.3	3.27	4.11	1	60.00	33.0	3809.98	0.00	778.05	0.87
36	147.35	27.94	37.3	3.27	4.11	1	60.00	33.0	3464.21	0.00	704.86	0.87
37	150.62	20.63	39.8	2.69	3.50	1	60.00	33.0	2557.57	0.00	608.88	0.88
38	153.31	18.21	39.8	2.69	3.50	1	60.00	33.0	2257.74	0.00	533.95	0.88
39	156.00	5.52	39.8	0.93	1.21	1	60.00	33.0	684.34	0.00	464.13	0.88
40	156.93	12.61	42.4	3.03	4.11	1	60.00	33.0	1563.99	0.00	303.95	0.88
41	159.97	4.20	42.4	3.03	4.11	1	60.00	33.0	521.33	0.00	79.89	0.88

X-S Area: 1120.26 Path Length: 156.16 X-S Weight: 138912.27

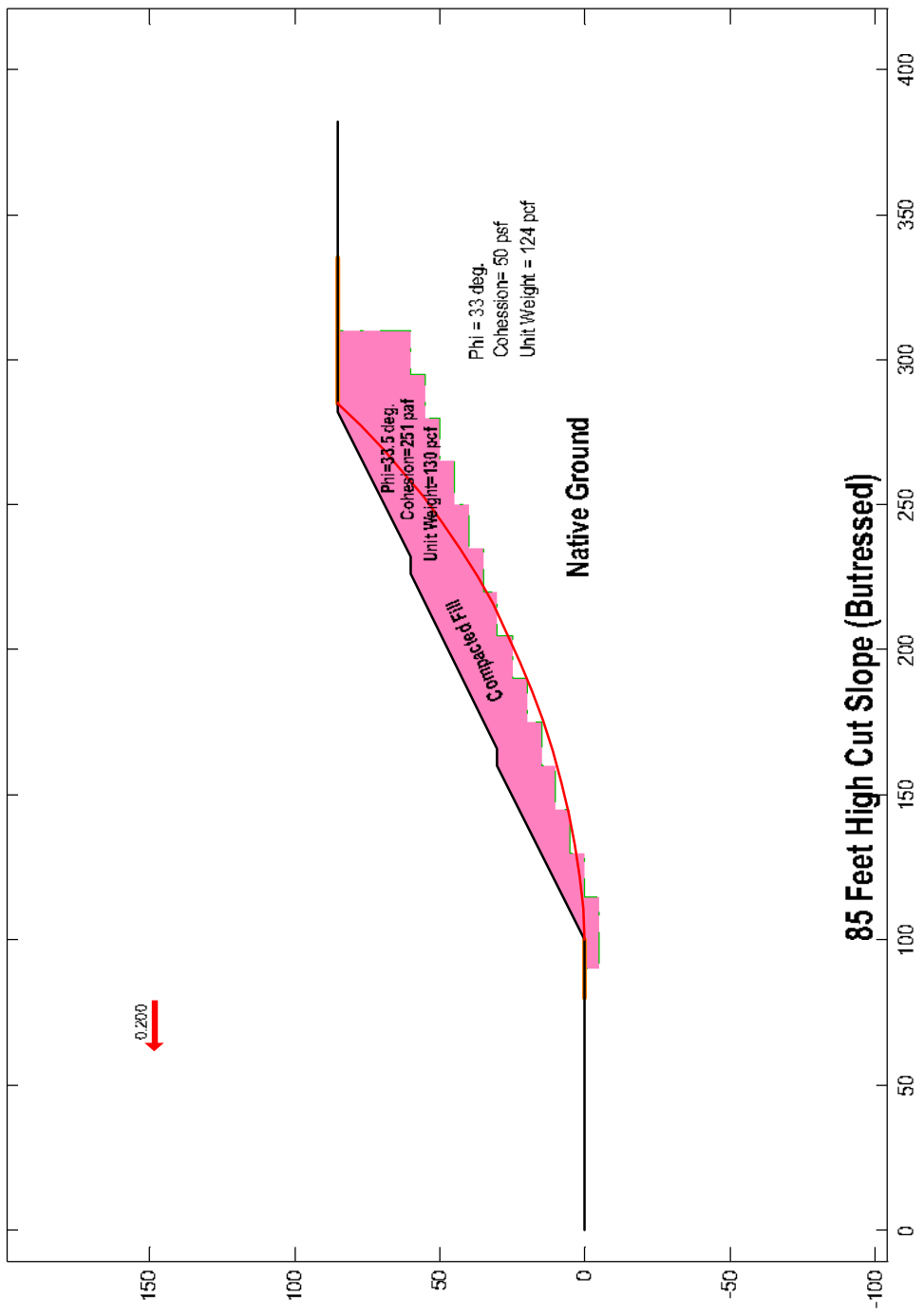
GALENA Version 5.01



Analysis: 1
Multiple Stability Analysis
 Method: Bishop Simplified
 Surface: Circular

Results
 Critical (minimum)
 Factor of Safety: 1.12

Edited: 3 Dec 2007 Processed: 3 Dec 2007



85 Feet High Cut Slope (Butressed)

Project: 85 Feet High Cut Slope (Overexcavated)
 85 Feet High Cut Slope (Overexcavated)

File: C:\Documents and Settings\HP_Administrator\My Documents\GALENA\6003.85 feet Cut Slope.gmf

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Galena 5.01 Analysis Results

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Project: 85 Feet High Cut Slope (Overexcavated)
 File: C:\Documents and Settings\HP_Administrator\My Documents\GALENA\6003.85 feet Cut Slope.gmf
 Processed: 03 Dec 2007 15:43:34

DATA: Analysis 1 - 85 Feet High Cut Slope (Overexcavated)

Material Properties (2 materials)

Material: 1 (Mohr-Coulomb Isotropic) - Compacted Fill
 Cohesion Phi UnitWeight Ru
 251.00 33.5 130.00 0.00
 Material: 2 (Mohr-Coulomb Isotropic) - Native Ground
 Cohesion Phi UnitWeight Ru
 50.00 33.0 124.00 0.00

Material Profiles (2 profiles)

Profile: 1 (2 points) Material beneath: 1 - Compacted Fill
 0.00 100.00 410.00 100.00
 Profile: 2 (37 points) Material within: 2 - Native Ground

90.00	0.00	90.00	-5.00	115.00	-5.00	115.00	0.00	130.00	0.00
130.00	5.00	145.00	5.00	145.00	10.00	160.00	10.00	160.00	15.00
175.00	15.00	175.00	20.00	190.00	20.00	190.00	25.00	205.00	25.00
205.00	30.00	220.00	30.00	220.00	35.00	235.00	35.00	235.00	40.00
250.00	40.00	250.00	45.00	265.00	45.00	265.00	50.00	280.00	50.00
280.00	55.00	295.00	55.00	295.00	60.00	310.00	60.00	310.00	85.00
282.00	85.00	232.00	60.00	226.00	60.00	166.00	30.00	160.00	30.00
100.00	0.00	90.00	0.00						

Slope Surface (8 points)

0.00	0.00	100.00	0.00	160.00	30.00	166.00	30.00	226.00	60.00
232.00	60.00	282.00	85.00	382.00	85.00				

Failure Surface

Initial circular surface for critical search defined by: XL, XR, R
 Intersects: XL: 100.00 YL: 0.00 XR: 285.00 YR: 85.00
 Centre: XC: 88.09 YC: 269.74 Radius: R: 270.00

Earthquake Force

Pseudo-static earthquake (seismic) coefficient: 0.200

Variable Restraints

Parameter descriptor:	XL	XR	R
Range of variation:	20.00	50.00	45.00
Trial positions within range:	10	10	1

RESULTS: Analysis 1 - 85 Feet High Cut Slope (Overexcavated)

Bishop Simplified Method of Analysis - Circular Failure Surface

Critical Failure Circle Search using Multiple Circle Generation Techniques

Factor of Safety for initial failure circle approximation: 1.21

There were: 85 successful analyses from a total of 101 trial circles
 16 analyses terminated due to unacceptable geometry

Critical (minimum) Factor of Safety: 1.12

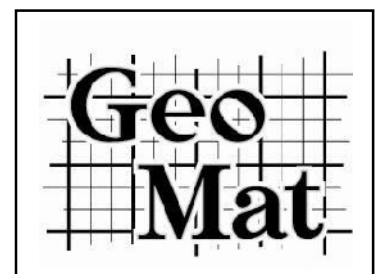
Circle and Results Summary (Lowest 85 Factor of Safety circles)

Circle	X-Centre	Y-Centre	X-Left	Y-Left	X-Right	Y-Right	Radius	FoS
1	88.09	269.74	100.00	0.00	285.00	85.00	270.00	1.124
2	93.83	269.93	100.00	0.00	290.56	85.00	270.00	1.139
3	93.81	269.91	86.67	0.00	290.56	85.00	270.00	1.146
4	93.75	269.84	84.44	0.00	290.56	85.00	270.00	1.150
5	93.67	269.76	82.22	0.00	290.56	85.00	270.00	1.153
6	99.45	270.00	100.00	0.00	296.11	85.00	270.00	1.154
7	99.33	269.87	91.11	0.00	296.11	85.00	270.00	1.155
8	99.39	269.93	93.33	0.00	296.11	85.00	270.00	1.156
9	93.58	269.66	80.00	0.00	290.56	85.00	270.00	1.157
10	99.26	269.80	88.89	0.00	296.11	85.00	270.00	1.158
11	99.18	269.71	86.67	0.00	296.11	85.00	270.00	1.160
12	99.08	269.60	84.44	0.00	296.11	85.00	270.00	1.163
13	98.96	269.48	82.22	0.00	296.11	85.00	270.00	1.166
14	98.83	269.34	80.00	0.00	296.11	85.00	270.00	1.171
15	104.96	269.95	100.00	0.00	301.67	85.00	270.00	1.172
16	104.92	269.91	97.78	0.00	301.67	85.00	270.00	1.172
17	104.86	269.84	95.56	0.00	301.67	85.00	270.00	1.172
18	104.78	269.76	93.33	0.00	301.67	85.00	270.00	1.173

9	136.85	60.61	10.7	4.09	4.16	1	251.00	33.5	7524.77	0.00	1619.08	0.92
10	140.93	41.63	10.7	2.62	2.67	2	50.00	33.0	5161.56	0.00	1767.23	0.92
11	143.55	23.82	13.0	1.45	1.48	2	50.00	33.0	2953.17	0.00	1793.16	0.91
12	145.00	80.05	13.0	4.63	4.75	1	251.00	33.5	10027.59	0.00	1861.00	0.90
13	149.63	85.81	13.0	4.63	4.75	1	251.00	33.5	10712.07	0.00	1991.13	0.90
14	154.26	113.72	15.4	5.74	5.95	1	251.00	33.5	14144.16	0.00	2067.74	0.89
15	160.00	96.02	15.4	4.85	5.03	1	251.00	33.5	12046.39	0.00	2084.05	0.89
16	164.85	21.73	17.7	1.15	1.20	1	251.00	33.5	2721.52	0.00	1937.04	0.88
17	166.00	86.24	17.7	4.50	4.72	1	251.00	33.5	10775.39	0.00	1955.96	0.88
18	170.50	89.91	17.7	4.50	4.72	1	251.00	33.5	11191.65	0.00	2033.84	0.88
19	175.00	110.49	19.9	5.32	5.66	1	251.00	33.5	13857.67	0.00	2080.34	0.88
20	180.32	114.33	20.0	5.32	5.66	1	251.00	33.5	14272.46	0.00	2141.25	0.88
21	185.64	96.03	22.3	4.36	4.71	1	251.00	33.5	11937.64	0.00	2131.69	0.87
22	190.00	130.54	22.3	5.80	6.28	1	251.00	33.5	16328.25	0.00	2190.87	0.87
23	195.80	70.70	24.7	3.10	3.41	1	251.00	33.5	8806.59	0.00	2155.52	0.87
24	198.90	71.09	24.7	3.10	3.41	1	251.00	33.5	8828.44	0.00	2161.05	0.87
25	202.00	69.13	24.7	3.00	3.30	2	50.00	33.0	8572.07	0.00	2243.45	0.87
26	205.00	18.21	24.7	0.79	0.87	1	251.00	33.5	2274.19	0.00	2193.49	0.87
27	205.79	74.02	27.0	3.20	3.59	1	251.00	33.5	9225.78	0.00	2130.36	0.86
28	208.99	73.92	27.0	3.20	3.59	1	251.00	33.5	9182.16	0.00	2119.87	0.86
29	212.19	78.23	27.0	3.39	3.81	2	50.00	33.0	9700.42	0.00	2192.74	0.87
30	215.58	101.43	29.3	4.42	5.08	2	50.00	33.0	12577.17	0.00	2126.47	0.87
31	220.00	31.75	29.3	1.40	1.60	1	251.00	33.5	3940.78	0.00	2025.89	0.86
32	221.40	84.81	29.3	3.76	4.31	2	50.00	33.0	10516.83	0.00	2094.59	0.87
33	225.15	19.00	31.7	0.85	1.00	2	50.00	33.0	2356.58	0.00	2028.66	0.87
34	226.00	123.09	31.7	6.00	7.05	2	50.00	33.0	15263.19	0.00	1854.96	0.87
35	232.00	46.34	31.7	2.50	2.94	2	50.00	33.0	5745.86	0.00	1672.42	0.87
36	234.50	81.85	34.0	4.55	5.49	2	50.00	33.0	10149.54	0.00	1581.95	0.87
37	239.06	78.23	34.0	4.55	5.49	2	50.00	33.0	9700.58	0.00	1511.03	0.87
38	243.61	71.96	36.3	4.43	5.49	2	50.00	33.0	8922.44	0.00	1391.87	0.87
39	248.04	67.34	36.3	4.43	5.49	2	50.00	33.0	8350.60	0.00	1301.19	0.87
40	252.46	60.28	38.7	4.29	5.49	2	50.00	33.0	7474.36	0.00	1167.21	0.88
41	256.75	54.75	38.7	4.29	5.49	2	50.00	33.0	6789.61	0.00	1058.05	0.88
42	261.04	47.09	41.0	4.15	5.49	2	50.00	33.0	5838.58	0.00	911.60	0.88
43	265.18	40.74	41.0	4.15	5.49	2	50.00	33.0	5051.63	0.00	785.27	0.88
44	269.33	32.67	43.3	4.00	5.49	2	50.00	33.0	4050.70	0.00	628.88	0.89
45	273.33	25.59	43.3	4.00	5.49	2	50.00	33.0	3173.04	0.00	486.73	0.89
46	277.32	20.09	45.7	4.68	6.69	2	50.00	33.0	2491.08	0.00	305.96	0.90
47	282.00	4.60	45.7	3.00	4.29	2	50.00	33.0	571.02	0.00	90.98	0.90

X-S Area: 2874.74 Path Length: 208.74 X-S Weight: 357598.00

$\beta^{\circ} \circ \gg 2\frac{1}{4} \cdot \ddot{\cdot} \quad \ddot{\cdot} \quad \ddot{\cdot}$



November 13, 2007

Haytham Nabils
Geomat Testing Laboratories, Inc.
9980 Indiana Avenue, Suite 14
Riverside, California 92503

SUBJECT: ENGINEERING GEOLOGIC STUDY AND SITE PLAN REVIEW
University Hills Development, Badger Canyon Area
San Bernardino, California
Project No. 1397-01

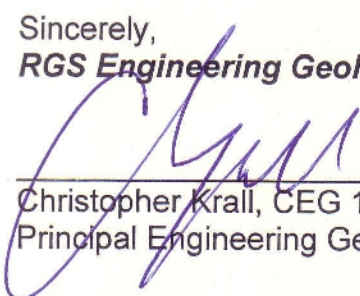
Mr. Nabils:

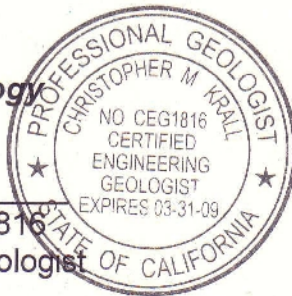
At your request, we have conducted an engineering geologic study and site plan review for the subject development. As you are aware the property has been extensively studied in terms of geotechnical factors and geologic/fault impacts by CHJ, Inc. However, since these reports were completed, the project development plans have changed. Accordingly, the purpose of this study was to evaluate the engineering geologic conditions identified at the site relative to the current development plan and provide appropriate engineering geologic recommendations for future site planning, design and development.

We understand this report will be used as part of an Environmental Impact Report (EIR) submittal for the development. This report is limited in scope to the engineering geologic aspects of the property and is intended to accompany the submittal of a soil or geotechnical report to provide a comprehensive evaluation of the geotechnical factors associated with the planned development.

We appreciate this opportunity to provide services for this project. Should you have any questions, or require additional information, please contact our office.

Sincerely,
RGS Engineering Geology


Christopher Krall, CEG 1816
Principal Engineering Geologist



Dist: (4) Addressee (hardcopy)
(1) Addressee (electronic)

Β½½±³ ° ç²§.²¹ Ó çº -ò ×'' «-ç ç-±²-ò ç²¼ Βº° »²¼.½»-

Ú.¹ «®» ï ó Í ç-» Ö±½ ç-±² Ó çº
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Ð ç-» ï ó Û »±±¹.½ Ó çº

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Í ½±º » ±º É ±®µ

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±½z' ±º »¹.±²z'º z«-ò Í » -º»²¹³ ±º » z³-«zµ»º.²¼¼¼¼ 1º±«²¼ - zµ.²¹ -
½±³ ³ ±²ß ³ z-«»¼ z- ³ z'.³ «³ ±ºº»zµ 1º±«²¼ z½½»»ºz±²ò B½½»»ºz±² - ¼ªº.²»¼
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Í ÙÝÑÒÜBÎ Ç Í Û×Í ÓxÝ ØBÆBÎ Û

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Í » ³ ±-ª - .¹².º.½z² ¹ »±±½ -».-³.½ z¼z¼ z-»±½z-ª¼ ©.³.³ »º±º»²¼ - z-º±²¹
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-».-³.½ z¼z¼.²¼¼¼¼¼¼ª²¹ºº±¼- ±º -º±²¹ 1º±«²¼ ³ ±±²- ½z«-»¼ ¼š ³ z¼±º
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-»-ª³ »²-ò z²¼º±½µºz'ò Üz.«º» ±º z¹» ©zª»º - z z¹»º z-¼ª²¹ z² » z³-«zµ»
½z² z-±.³º z½ºº»²- ±½z±²¼ z-±º»º»»ªz±²-ò Üz½ ±º ³ » - z »ºª²z' z¼z¼-
-¼.-½«-»¼.²¼ª.ª¼z'š¼ª±º

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z-±½z-ª¼ ©.³.ª»ººz±²º»²±³ »²±²ò ©.½.ª -¼.-½«-»¼¼ª±º

É².ª»®.-§ Ø.-
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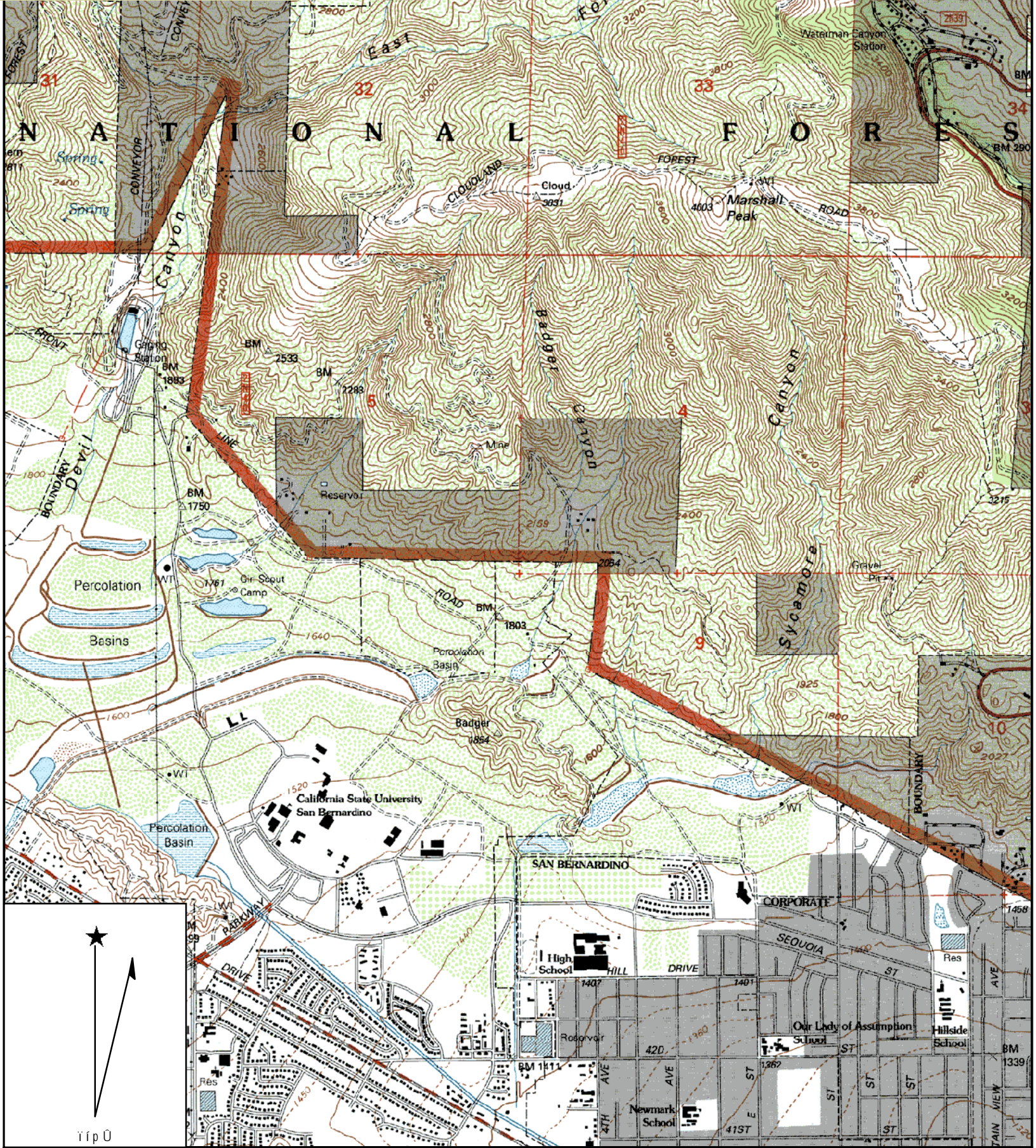
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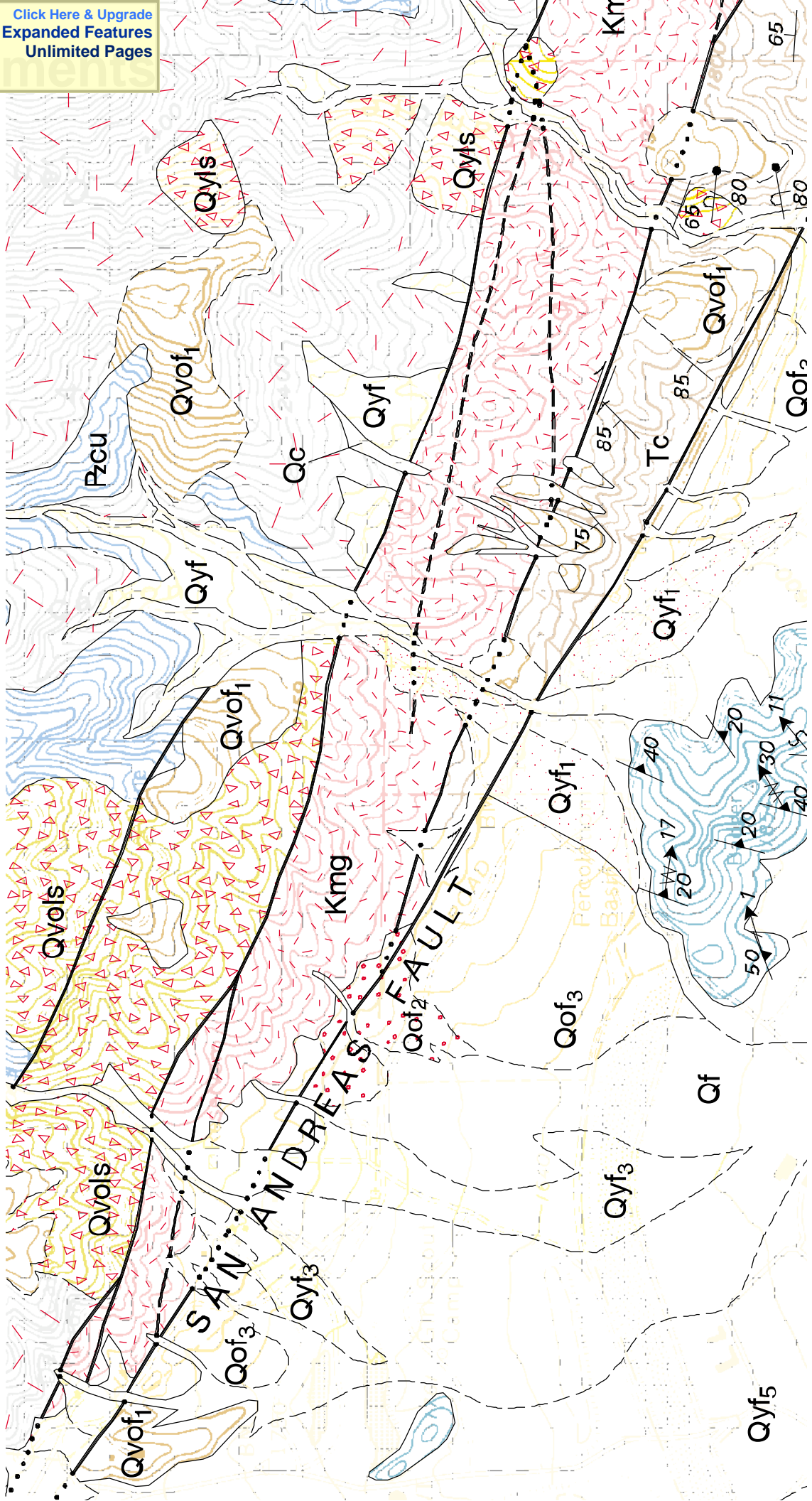
Ý´±-«º»

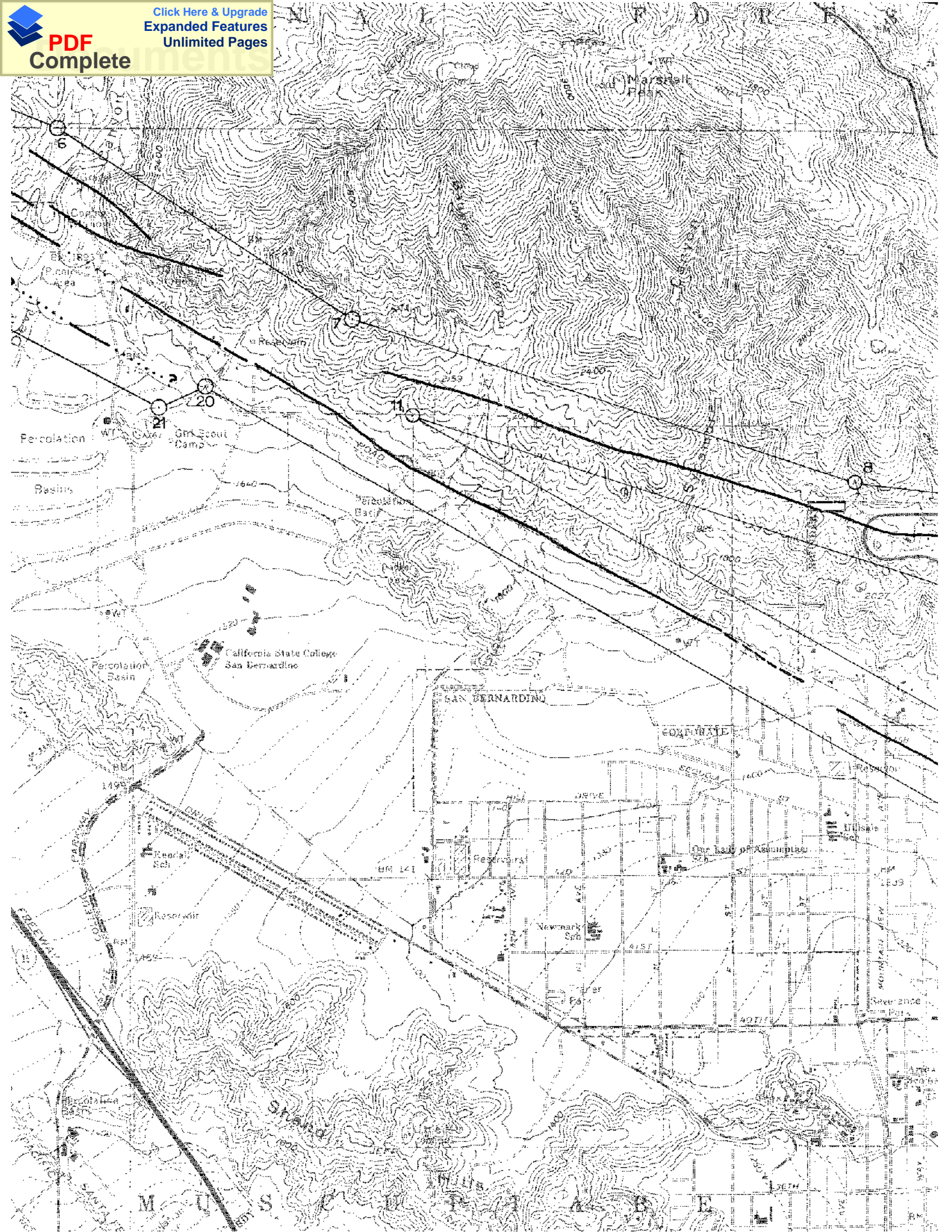
Ñ«º.2ª»-→¹ j-±² © j- °º±º³ »¼ «-.-²¹ ¼ »¼»¹º» ±º ½ jº» j²¼ -µ.´ ±º¼.² jº.‘§ »´»º½.-»¼0
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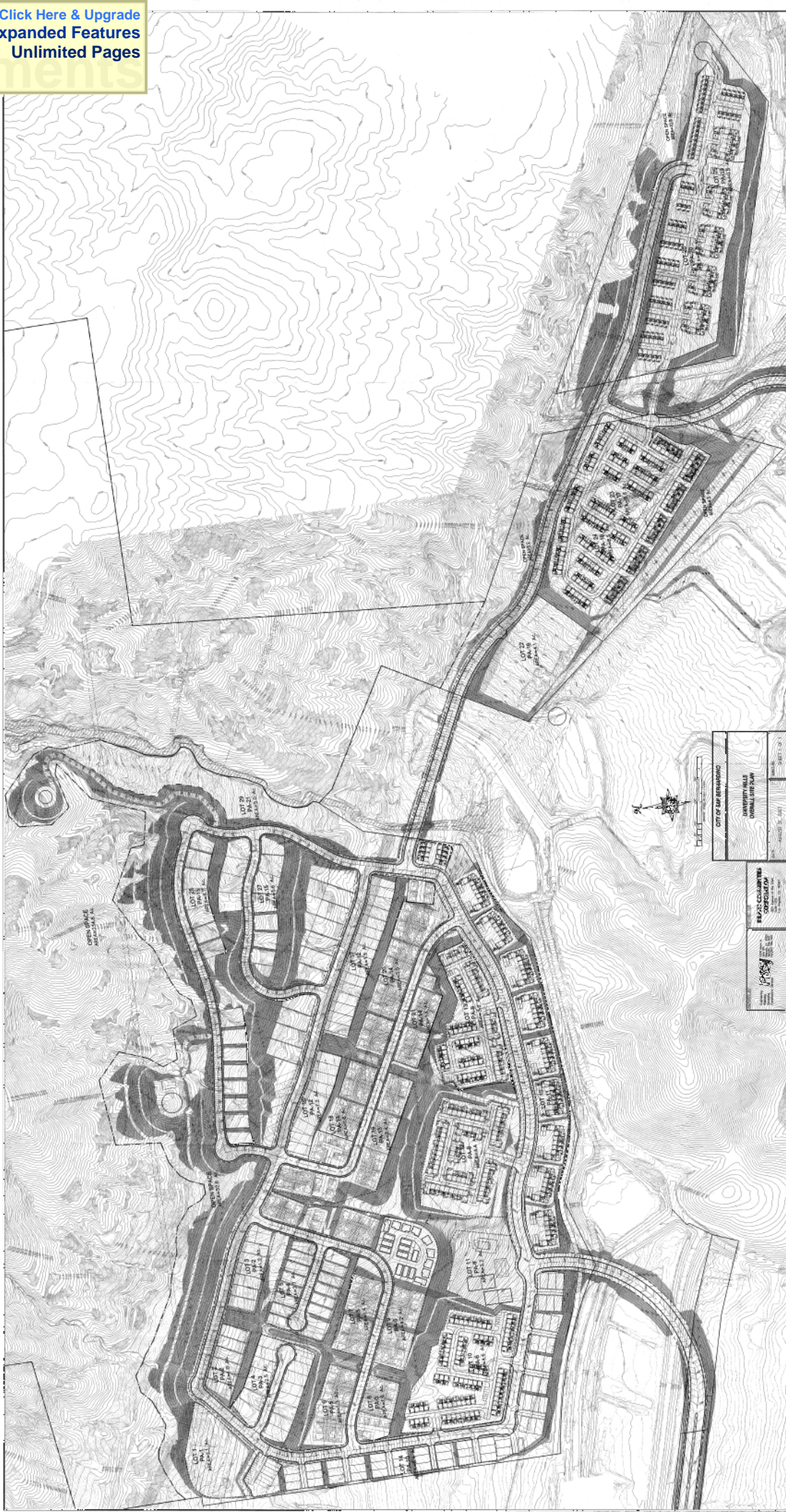


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LEGEND

CITY OF SAN BERNARDINO

UNIVERSITY HILLS

SMALL LOT PLAN

SCALE

DATE

PROJECT NO.

DESIGNED BY

DRAWN BY

CHECKED BY

APPROVED BY

$\beta^{\circ} \circ \gg 2\frac{1}{4} \cdot \cdot \beta$

**Geo
Mat**



Î ÒÙÙÎ ÒÒÛÛÎ

Ý¸:°±².¸ Ù.ª.¸±² ±° Ó.²»- ¸²¼ Ù»±±¹§ ïççèè •Ù«¼»²»- °±² Ùª¸¸¸²¹ ³» Ø¸¸¼ ±°
Í «²¼» Ù¸¸¸¹ «°-«²»èè ß¼±°-¼¼ ¼§ ³» Í-¸» Ó.².²¹ ¸²¼ Ù»±±¹§ Þ±¸¼ ±² Ó¸§ çò ïççèè

Ý¸:°±².¸ Ù.ª.¸±² ±° Ó.²»- ¸²¼ Ù»±±¹§ ïðððð •Ù.¹.¸´ x³ ¸¹»- ±° Ñº.½.¸´ Ó¸° - ±° ß´«-òð±±
Ù¸¼³ - «¸µ» Ù¸¸¸¹ ±²²- ±° Ý¸:°±².¸èè Í ±«³»² Í »¹.±²ò ÙÓÙ ÝÙ ïððððððð

ÝØØò x²½ò ïððè¸ò Í «¼-«²¼» x²ª»-¹¸±² ±° Ù¸¸¸¹ð ð¸¼.¸» Ø´- ð±²¼½ò Þ¼¹»º Ý¸²§±²
ß»¸¸ò Ý.¸ ±° Í ¸² Þ»²¼.²±ò Ý¸:°±².¸ò Ò±¼ Ò±ò ðèèçì òèè Ò¸²«¸§ í ò ïððèè

ÝØØò x²½ò ïððè¸ò Ù»±±¹½.².½¸´ x²ª»-¹¸±²ò ð¸¼.¸» Ø´- ð±²¼½ò Þ¼¹»º Ý¸²§±² ß»¸¸ò
Í »²-¸ª» Ì¸¼¸ Ó¸° Ò±ò ïèì òðò Ý.¸ ±° Í ¸² Þ»²¼.²±ò Ý¸:°±².¸ò Ò±¼ Ò±ò ðèèçì òí ò Ó¸§ í èò
ïððèè

ÝØØò x²½ò ïððè¸ò Ù»±±¹½.².½¸´ x²ª»-¹¸±²ò Ñºº-¸» x³ °±²ª»³ »²-ò ð¸¼.¸» Ø´- ð±²¼½ò
Þ¼¹»º Ý¸²§±² ß»¸¸ò Ì »²-¸ª» Ì¸¼¸ Ó¸° Ò±ò ïèì òðò Ý.¸ ±° Í ¸² Þ»²¼.²±ò Ý¸:°±².¸ò Ò±¼
Ò±ò ðèè ï ò í ò Ò«²» èò ïððèè

Ò»²².²¹-ò Ý¸¸»-ò Éò ïççìò •ð»³.².¸§ Ù¸¸¸¹ ß¼ªª.¸ Ó¸° ±° Ý¸:°±².¸èè Ý¸:°±².¸ Ù.ª.¸±² ±°
Ó.²»- ¸²¼ Ù»±±¹§ Ñº»² Ù.¸ Í »°±² çì òððð

Ý¸º-±²ò Í òÙò ¸²¼ Ó¸¸ò ÒòÝòò ïçèèò Ý±²±«º Ó¸° Í ±©.²¹ Ó.².³ «³ Ù»º ± Ù±«²¼©¸»º
Éº»º Í ¸²-¸ ß²¸ Í.ªº È¸»»§ò Ý¸:°±².¸ò ïçèè òí çèçò È².ª¼ Í-¸»- Ù»±±¹.½¸´ Í «ª»§ò
Ó.-½¸´ ¸²±«- Ù.¸¼ Í-«¼»- Ó¸° ÒÙò òððð

Ó¸¸ò ÒòÝò ¸²¼ Ý¸º-±²ò Í òÙòò ïçèèò Ò´«»º¸±² Í «-½»º-¼.¸-¸.² ³» Í ¸² Þ»²¼.²± È¸´»§ ¸²¼
È.½.².¸ò Í ±«³»² Ý¸:°±².¸èè ß ð»³.².¸§ Ùª¸¸¸²ò È².ª¼ Í-¸»- Ù»±±¹.½ Í «ª»§ò Ñº»²
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Ó¸¸ò ÒòÝò Ó±²±²ò ÙòÓòò ¸²¼ Ý±²ò ÞòÙòò ïçèèò Ù-¸¼ªª¸±² ¸²¼ Ù»±±¹.½ Í »¸±²- ±° Ù¸¸¸¹
Í §-¸»³ - .² ³»ª.½.².¸ ±° ³» Ý»²-¸¸ Ì¸²-ª»º- Í ¸²¹»-ò Í ±«³»² Ý¸:°±².¸ò È².ª¼ Í-¸»-
Ù»±±¹.½¸´ Í «ª»§ò Ñº»² Ù.¸ Í »°±² èèèèèè

Ó¸¸ò ÒòÝò Ó±²±²ò ÙòÓòò ¸²¼ Ý±²ò ÞòÙòò ïççìò Ì » Í ¸² ß²¼ª»¸- Ù¸¸¸¹ Í §-¸»³ .² ³» È.½.².¸ ±°
³» Ý»²-¸¸ Ì¸²-ª»º- Í ¸²¹»- ð±².²½òò Í ±«³»² Ý¸:°±².¸ò È².ª¼ Í-¸»- Ù»±±¹.½ Í «ª»§ò
Ñº»² Ù.¸ Í »°±² çì òí èì ò

Ó´»º ÙòÓòò Ó¸¸ò ÒòÝòò ¸²¼ Ý¸º-±²ò Í òÙòò ïðððò Ù»±±¹.½ Ó¸° ±° ³» Í ¸² Þ»²¼.²± Ò±² èèè
Í «¼ª²¹»ò Í ¸² Þ»²¼.²± Ý±«²-§ò Ý¸:°±².¸ò È².ª¼ Í-¸»- Ù»±±¹.½ Í «ª»§ò Ñº»² Ù.¸
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ð»»º-»² »ò ¸òò ïççèè •ð±¼¼.¸-¸½ Í »-³.½ Ø¸¸¼ ß--»--³ »²-°±² ³» Í-¸» ±° Ý¸:°±².¸èè
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β»®.ζ´ Đ. ±±±¹®ζ´° - Î »ª.»©»¼

Í ±«®½»	Üζ-»	Ú´¹ζ´	Đ. ±±± Ö±±	Í ½ζ´»
Í ζ² Þ»®²º Ý±± Ü´±±¼	İ İ öí ðöèè	Úóí ì	éóí î ò í í ò í ì	İ ĩāĩ ĩ ððĩ
Í ζ² Þ»®²º Ý±± Ü´±±¼	ðéóđĩ óçĩ	Ýòĩ èì	ĩ çĩ ò ĩ çè	İ ĩāĩ ððĩ
Í ζ² Þ»®²º Ý±± Ü´±±¼	đĩ öĩ çóðè	Ýöèèĩ	ĩ èóí çò ì ðò ì ĩ	İ ĩāĩ ððĩ